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GPD\# 2012801.10
April 24, 2012

## RIGORCUS STRUCTURAL ANALYSIS REPORT

| AT\&T DESIGNAIION: | Site USID: | 4340 |
| :---: | :---: | :---: |
|  | Site FA: | 110096382 |
|  | Site Name: | NORTH PORTLAND |
|  | AT\&T Project: | MOD LTE W3 012312 |
| ANALYSIS CRITERIA: | Codes: | TIA-222-G, 2009 IBC \& ASCE 7-05 |
|  |  | 100-mph 3-second gust with 0 " ice |
|  |  | 40 (1-mph 3 -second gust with $1^{\prime \prime}$ ice |
| SITE DATA: |  | 1340 Riverside Street, Portland, ME 04103, Cumberland County |
|  |  | Latitude $43^{\circ} 42{ }^{\prime} 59.831 " \mathrm{~N}$, Longitude $70^{\circ} 18{ }^{\prime} 18.936 " \mathrm{~W}$ |
|  |  | Market: New England |
|  |  | 1/7.5' PiROD Monopole |

Mr. Mark Roberts,

GPD is pleased to submit this Structural Analy:sis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

## Analysis Results

| Tower Stress Level with Proposed Equipment: | $82.1 \%$ | Pass |
| :--- | :--- | :--- |
| Foundation Ratio with Proposed Equipment: | $58.1 \%$ | Pass |

We at GPD appreciate the opportunity of providing our continuing professional services to you and NexLink. If you have any questions or need further assistance on this or any other projects please do not hesitate to call.


## SUMMARY \& RESULTS

The purpose of this analysis was to verify whether the existing structure is capable of carrying the proposed loading configuration as specified by AT\&T to N exLink. This report was commissioned by Mr. Mark Roberts of NexLink.

The proposed coax shall be installed internal to the monopole for the results of this analysis to be valid.
TO WER SUMMARY AND RESULTS

| Member | Capacity | Results |
| :--- | :---: | :---: |
| Monopole | $82.1 \%$ | Pass |
| Anchor Rods | $48.2 \%$ | Pass |
| Base Plate | $67.3 \%$ | Pass |
| Flange Bolts | $79.1 \%$ | Pass |
| Flange Plates | $75.7 \%$ | Pass |
| Foundation | $58.1 \%$ | Pass |

## AN ALYSIS METHO D

tnxTower (Version 6.0.4.0), a commercially available software program, was used to create a three-dimensional model of the tower and calculate primary member stresses for various dead, live, wind, and ice load cases. Selected output from the analysis is included in Appendix B. The following table details the information provided to complete this structural analysis. This analysis is solely based on this information and is being completed without the benefit of a detailed site visit.

DOCUMENTS PROVIDED

| Document | Remarks | Source |
| :--- | :--- | :---: |
| Equipment M odification Form | AT\&T Internal Loading Document, uploaded 4/5/2012 | Siterra |
| RF Data Sheet | Not Provided | $\mathrm{N} / \mathrm{A}$ |
| Construction Drawings | Not Provided | $\mathrm{N} / \mathrm{A}$ |
| Tower Design | PiROD File \#. A-113355, dated 3/5/97 | Siterra |
| Foundation Design | PiROD File \#. A-113355, dated 3/5/97 | Siterra |
| Geotechnical Report | Halaey \& Aldrich File \#. 80593-001, dated 2/28/97 | Siterra |
| Previous Structural Analysis | GPD Project \#. 2008147.07, dated 8/15/08 | Siterra |

## ASSU M PTIO NS

This structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. GPD has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The antenna configuration is as supplied and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Some assumptions are made regarding antennas and mount sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type and industry practice.
4. All mounts, if applicable, are considered adequate to support the loading. No actual analysis of the mount(s) is performed. This analysis is limited to analyzing the tower only.
5. The soil parameters are as per data supplied or as assumed and stated in the calculations.
6. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
7. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
8. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
9. Loading interpreted from photos is accurate to $\pm 5^{\prime} \mathrm{AGL}$, antenna size accurate to $\pm 3.3 \mathrm{sf}$, and coax equal to the number of existing antennas without reserve.
10. All existing loading was obtained from GPD (Project \#: 2008147.07, dated 8/15/08), site photos, the provided Equipment M odification Form and is assumed to be accurate.
11. All proposed coax shall be installed inside internal to the monopole.
12. The proposed RRU's were assumed to be installed 2' below the proposed antenna centerline elevation.
13. The existing/proposed Ioading elevations listed within the Equipment Modification Form were found to vary from the loading elevations listed in the previous analysis as well as site photos. The existing/proposed loading has been modeled based on the elevations observed in site photos.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and GPD Group should be allowed to review any new information to determine its effect on the structural integrity of the tower.

## DISCLAIMER OF W ARRANTIES

GPD GROUP has not performed a recent site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD GROUP in connection with this Rigorous Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. All tower components have been assumed to only resist dead loads when no other loads are applied. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

GPD GROUP does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD GROUP provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the feasibility of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation in excess of the specified code recommended amount, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD GROUP, but are beyond the scope of this report.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

GPD GROUP makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD GROUP will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD GROUP pursuant to this report will be limited to the total fee received for preparation of this report.

## APPENDIX A

Tower Analysis Summary Form

Tower Analysis Summary Form

| General Info |
| :--- |
| Site Name NORTH PORTLAND <br> Site Number ME5015 (3340) <br> FA Number 10096382 <br> Date of Analysis $4 / 24 / 2012$ <br> Company Performing Analysis GPD |

The information contained in this summary report is not to be used
independently from the PE stamped tower analysis.

| Tower Info | Description | Date |
| :---: | :---: | :---: |
| Tower Type (G, SST, MP) | MP |  |
| Tower Height (top of steel AGL) | 177.5' |  |
| Tower Manufacturer | PiROD |  |
| Tower Model | n/a |  |
| Tower Design | PIROD File \#: A-113355 | 3/5/1997 |
| Foundation Investigation | PIROD File \#: A-113355 | 3/5/1997 |
| Geotech Investigation | Haley \& Aldrich File \#: 80593-001 | 2/28/1997 |
| Tower Mapping | n/a |  |
| Modification Drawings | n/a |  |
| Previous Structural Analysis | GPD Project \#: 2008147.07 | 8/15/2008 |
| Foundation Mapping | n/a |  |

Design Parameters

| Design Code Used | TIA-222-G \& 2009 IBC |
| :--- | :---: |
| Location of Tower (County, State) | Cumberland, Maine |
| Basic Wind Speed (mph) | 100 |
| Ice Thickness (in) | 1 |
| Structure Classification (I, II, III) | II |
| Exposure Category (, C, D) | C |
| Topographic Category (1 to 5) | 1 |

Analysis Results (\% Maximum Usage)

| Existing/Reserved + Future + Proposed Condition |  |
| :--- | :---: |
| Tower (\%) | $82.1 \%$ |
| Tower Base $(\%)$ | $67.3 \%$ |
| Foundation $(\%)$ | $58.1 \%$ |
| Foundation Adequate? | Yes |



Existing / Reserved Loading

| Antenna |  |  |  |  |  |  |  | Mount |  |  | Transmission Line |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna Owner | Mount Height (ft) | Antenna CL (tt) | Quantity | Type | Manufacturer | Model | Azimuth | Quantity | Manufacturer | Type | Quantity | Model | Size | Attachment Leg/Face |
| AT\&T Mobility | 179 | 180 | 6 | Panel | Powerwave | 7770.00 | 50/160/280 | 1 | Unknown | 13' LP Platiorm | 12 | Unknown | 1-5/8" | Internal |
| AT\&T Mobility | 179 | 180 | 6 | TMA | Powerwave | LGP21401 |  |  |  | behind the antennas |  |  |  |  |
| AT\&T Mobility | 179 | 180 | 6 | Diplexer | Powerwave | LGP21903 |  |  |  | behind the antennas |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Nextel | 160 | 160 | 12 | Panel | Decibel | DB846G90A-XY |  | 1 | Unknown | 15' LP Platform | 15 | Unknown | 1-5/8" | Internal |
| Nextel | 160 | 160 | 3 | Panel | Decibel | 932DG65T2E-M |  |  |  | on the same mount |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Unknown | 125 | 125 | 2 | Dish | Unknown | 4' Dish |  |  |  | pipe mounted | 2 | Unknown | EW90 | Internal |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Antenna |  |  |  |  |  |  |  | Mount |  |  | Transmission Line |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna Owner | Mount Height (ft) | Antenna CL (ft) | Quantity | Type | Manufacturer | Model | Azimuth | Quantity | Manufacturer | Type | Quantity | Model | Size | Attachment Leg/Face |
| AT\&T Mobility | 179 | 180 | 1 | Panel | Powerwave | P65-17-XLH-RR |  |  |  | on existing mount | 3 | DC/Fiber | ${ }^{1 / 2^{\prime \prime}}$ | Internal |
| AT\&T Mobility | 179 | 180 | 1 | Panel | Andrew | SBNH-1D6565C |  |  |  | on existing mount |  |  |  |  |
| AT\&T Mobility | 179 | 180 | 1 | Panel | KMW | AM-X-CD-14-65-00T |  |  |  | on existing mount |  |  |  |  |
| AT\&T Mobility | 179 | 178 | 6 | RRH | Ericsson | RBS6601 |  |  |  | on existing mount |  |  |  |  |
| AT\&T Mobility | 179 | 178 | 1 | Surge | Raycap | DC6-48-60-18-8F |  |  |  | on existing mount |  |  |  |  |

Note: Proposed loading is in addition to the existing loading at the same elevation.

| Antenna |  |  |  |  |  |  |  | Mount |  |  | Transmission Line |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna Owner | $\begin{gathered} \text { Mount } \\ \text { Height (ft) } \end{gathered}$ | Antenna CL (t) | Quantity | Type | Manufacturer | Model | Azimuth | Quantity | Manufacturer | Type | Quantity | Model | Size | Attachment Leg/Face |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## APPENDIX B

tnxTower O utput File

| tnxTower | ME5015 (4340) NORTH PORTLAND |  | $\text { Page } 1 \text { of } 4$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 S. Main St., Suite 2531 | Project | 2012801.10 | Date 14:17:48 04/24/12 |
| Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Client | Nexlink Global Communications | Designed by cburton |

## Tower Input Data

There is a pole section.
This tower is designed using the TIA-222-G standard.
The following design criteria apply:
Tower is located in Cumberland County, Maine.
Basic wind speed of 100 mph .
Structure Class II.
Exposure Category C.
Topographic Category 1.
Crest Height 0.00 ft .
Nominal ice thickness of 1.0000 in.
Ice thickness is considered to increase with height.
Ice density of 56 pcf .
A wind speed of 40 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 60 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1 .
Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs
Consider Moments - Horizontals Consider Moments - Diagonals
Use Moment Magnification
$\sqrt{ }$ Use Code Stress Ratios
$\sqrt{ }$ Use Code Safety Factors - Guys Escalate Ice
Always Use Max Kz
Use Special Wind Profile
$\checkmark$ Include Bolts In Member Capacity
$\sqrt{ }$ Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg
Use Diamond Inner Bracing (4 Sided) Add IBC .6D+W Combination

Distribute Leg Loads As Uniform
Assume Legs Pinned
$\sqrt{ }$ Assume Rigid Index Plate
$\sqrt{ }$ Use Clear Spans For Wind Area
$\sqrt{ }$ Use Clear Spans For KL/r Retension Guys To Initial Tension
$\sqrt{ }$ Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends Sort Capacity Reports By Component Triangulate Diamond Inner Bracing

Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules
$\sqrt{ }$ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression
$\sqrt{ }$ All Leg Panels Have Same Allowable Offset Girt At Foundation
$\sqrt{ }$ Consider Feedline Torque
Include Angle Block Shear Check Poles
$\sqrt{ }$ Include Shear-Torsion Interaction
Always Use Sub-Critical Flow Use Top Mounted Sockets

| tnxTower <br> GPD Group <br> 520 S. Main St., Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Job ME5015 (4340) NORTH PORTLAND |  | Page  <br>  2 of 4 <br> Date  <br> 14:17:48 04/24/12  |
| :---: | :---: | :---: | :---: |
|  | Project | 2012801.10 |  |
|  | Client | Nexlink Global Communications | Designed by cburton |

## Feed Line/Linear Appurtenances - Entered As Area

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& Allow Shield \& Component Type \& \begin{tabular}{l}
Placement \\
ft
\end{tabular} \& Total Number \& \& \(C_{A} A_{A}\)

$f t^{2} / f t$ \& Weight plf <br>
\hline LDF7-50A(1-5/8") \& C \& No \& Inside Pole \& 177.50-8.00 \& 12 \& No Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& $1{ }^{1 \prime}$ Ice \& 0.00 \& 0.82 <br>
\hline 1/2" DC/Fiber \& C \& No \& Inside Pole \& 177.50-8.00 \& 3 \& No Ice \& 0.00 \& 0.15 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.15 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 0.15 <br>
\hline LDF7-50A(1-5/8") \& C \& No \& Inside Pole \& 160.00-8.00 \& 15 \& No Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 0.82 <br>
\hline EW90 \& C \& No \& Inside Pole \& 125.00-8.00 \& 2 \& No Ice \& 0.00 \& 0.32 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.32 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.00 \& 0.32 <br>
\hline
\end{tabular}

## Discrete Tower Loads

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | $\begin{aligned} & \text { Offset } \\ & \text { Type } \end{aligned}$ | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ <br> ft <br> ft | Azimuth Adjustment | Placement |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $C_{A} A_{A}$ <br> Side <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 13' Rotatable Platform | C | None |  | 0.0000 | 179.00 | No Ice | 32.79 | 32.79 | 2.04 |
|  |  |  |  |  |  | 1/2" Ice | 44.63 | 44.63 | 2.48 |
|  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 56.47 | 56.47 | 2.91 |
| (2) $7770.00 \mathrm{w} / 6$ ' Mount Pipe | A | From | 4.00 | 0.0000 | 179.00 | No Ice | 6.22 | 4.35 | 0.06 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 6.77 | 5.20 | 0.11 |
|  |  | Leg | 1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 7.30 | 5.92 | 0.16 |
| (2) $7770.00 \mathrm{w} / 6$ ' Mount Pipe | B | From | 4.00 | 0.0000 | 179.00 | No Ice | 6.22 | 4.35 | 0.06 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 6.77 | 5.20 | 0.11 |
|  |  | Leg | 1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 7.30 | 5.92 | 0.16 |
| (2) $7770.00 \mathrm{w} / 6$ ' Mount Pipe | C | From | 4.00 | 0.0000 | 179.00 | No Ice | 6.22 | 4.35 | 0.06 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 6.77 | 5.20 | 0.11 |
|  |  | Leg | 1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 7.30 | 5.92 | 0.16 |
| (2) LGP21903 Diplexer | A | From | 4.00 | 0.0000 | 179.00 | No Ice | 0.27 | 0.18 | 0.01 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 0.34 | 0.25 | 0.01 |
|  |  | Leg | 1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 0.43 | 0.32 | 0.02 |
| (2) LGP21903 Diplexer | B | From | 4.00 | 0.0000 | 179.00 | No Ice | 0.27 | 0.18 | 0.01 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 0.34 | 0.25 | 0.01 |
|  |  | Leg | 1.00 |  |  | 1 " Ice | 0.43 | 0.32 | 0.02 |
| (2) LGP21903 Diplexer | C | From | 4.00 | 0.0000 | 179.00 | No Ice | 0.27 | 0.18 | 0.01 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 0.34 | 0.25 | 0.01 |
|  |  | Leg | 1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 0.43 | 0.32 | 0.02 |
| (2) LGP21401 | A | From | 4.00 | 0.0000 | 179.00 | No Ice | 1.29 | 0.23 | 0.01 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 1.45 | 0.31 | 0.02 |
|  |  | Leg | 1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 1.61 | 0.40 | 0.03 |
| (2) LGP21401 | B | From | 4.00 | 0.0000 | 179.00 | No Ice | 1.29 | 0.23 | 0.01 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 1.45 | 0.31 | 0.02 |
|  |  | Leg | 1.00 |  |  | $1^{\prime \prime}$ Ice | 1.61 | 0.40 | 0.03 |
| (2) LGP21401 | C | From | 4.00 | 0.0000 | 179.00 | No Ice | 1.29 | 0.23 | 0.01 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 1.45 | 0.31 | 0.02 |
|  |  | Leg | 1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 1.61 | 0.40 | 0.03 |
| P65-17-XLH-RR w/ Mount Pipe | A | From | 4.00 | 0.0000 | 179.00 | No Ice | 11.47 | 8.70 | 0.10 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 12.08 | 10.11 | 0.18 |
|  |  | Leg | 1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 12.71 | 11.38 | 0.27 |


| tnxTower | Job ME5015 (4340) NORTH PORTLAND |  | $\begin{aligned} & \text { Page } \\ & \\ & \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 S. Main St., Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2012801.10 | Date 14:17:48 04/24/12 |
|  | Client | Nexlink Global Communications | Designed by cburton |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ <br> $f t$ <br> ft | Azimuth Adjustment | Placement |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $C_{A} A_{A}$ <br> Side <br> $f t^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SBNH-1D6565C w/ 5' Mount Pipe | B | From | 4.00 | 0.0000 | 179.00 | No Ice | 11.45 | 8.88 | 0.08 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 12.06 | 9.78 | 0.16 |
|  |  | Leg | 1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 12.69 | 10.70 | 0.25 |
| AM-X-CD-14-65-00T w/ Mount Pipe | C | From | 4.00 | 0.0000 | 179.00 | No Ice | 6.91 | 5.63 | 0.09 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 7.60 | 6.54 | 0.15 |
|  |  | Leg | 1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 8.25 | 7.36 | 0.22 |
| (2) RBS 6601 | A | From | 4.00 | 0.0000 | 179.00 | No Ice | 0.55 | 0.40 | 0.02 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 0.70 | 0.52 | 0.03 |
|  |  | Leg | -1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 0.86 | 0.64 | 0.05 |
| (2) RBS 6601 | B | From | 4.00 | 0.0000 | 179.00 | No Ice | 0.55 | 0.40 | 0.02 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 0.70 | 0.52 | 0.03 |
|  |  | Leg | -1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 0.86 | 0.64 | 0.05 |
| (2) RBS 6601 | C | From | 4.00 | 0.0000 | 179.00 | No Ice | 0.55 | 0.40 | 0.02 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 0.70 | 0.52 | 0.03 |
|  |  | Leg | -1.00 |  |  | 1 " Ice | 0.86 | 0.64 | 0.05 |
| DC6-48-60-18-8F | C | From Leg | 1.00 | 0.0000 | 179.00 | No Ice | 2.22 | 2.22 | 0.02 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 2.44 | 2.44 | 0.04 |
|  |  |  | -1.00 |  |  | $1{ }^{\prime \prime}$ Ice | 2.66 | 2.66 | 0.06 |
| 15' LP Platform | C | None |  | 0.0000 | 160.00 | No Ice | 18.85 | 18.85 | 1.50 |
|  |  |  |  |  |  | 1/2" Ice | 24.30 | 24.30 | 1.80 |
|  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 29.75 | 29.75 | 2.09 |
| (4) DB846G90A-XY w/ Mount Pipe | A | From | 4.00 | 0.0000 | 160.00 | No Ice | 5.23 | 7.53 | 0.04 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 5.78 | 8.72 | 0.09 |
|  |  | Leg | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 6.30 | 9.62 | 0.16 |
| (4) DB846G90A-XY w/ Mount Pipe | B | From | 4.00 | 0.0000 | 160.00 | No Ice | 5.23 | 7.53 | 0.04 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 5.78 | 8.72 | 0.09 |
|  |  | Leg | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 6.30 | 9.62 | 0.16 |
| (4) DB846G90A-XY w/ Mount Pipe | C | From | 4.00 | 0.0000 | 160.00 | No Ice | 5.23 | 7.53 | 0.04 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 5.78 | 8.72 | 0.09 |
|  |  | Leg | 0.00 |  |  | 1 " Ice | 6.30 | 9.62 | 0.16 |
| 932DG65T2E-M w/Mount Pipe | A | From | 4.00 | 0.0000 | 160.00 | No Ice | 4.15 | 3.50 | 0.04 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 4.79 | 4.54 | 0.07 |
|  |  | Leg | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 5.35 | 5.30 | 0.11 |
| 932DG65T2E-M w/Mount Pipe | B | From | 4.00 | 0.0000 | 160.00 | No Ice | 4.15 | 3.50 | 0.04 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 4.79 | 4.54 | 0.07 |
|  |  | Leg | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 5.35 | 5.30 | 0.11 |
| 932DG65T2E-M w/Mount Pipe | C | From | 4.00 | 0.0000 | 160.00 | No Ice | 4.15 | 3.50 | 0.04 |
|  |  | Centroid- | 0.00 |  |  | 1/2" Ice | 4.79 | 4.54 | 0.07 |
|  |  | Leg | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 5.35 | 5.30 | 0.11 |
| 3" x 5' Mount Pipe | A | From Face | 0.50 | 0.0000 | 125.00 | No Ice | 1.36 | 1.36 | 0.03 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 1.67 | 1.67 | 0.04 |
|  |  |  | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 1.98 | 1.98 | 0.05 |
| 3" x 5' Mount Pipe | B | From Leg | 0.50 | 0.0000 | 125.00 | No Ice | 1.36 | 1.36 | 0.03 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 1.67 | 1.67 | 0.04 |
|  |  |  | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 1.98 | 1.98 | 0.05 |


| tnxTower | Job ME5015 (4340) NORTH PORTLAND |  | $\text { Page } 4 \text { of } 4$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 S. Main St., Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2012801.10 | $\begin{aligned} & \text { Date } \\ & \text { 14:17:48 04/24/12 } \end{aligned}$ |
|  | Client | Nexlink Global Communications | Designed by cburton |


| Dishes |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | $\begin{aligned} & \text { Dish } \\ & \text { Type } \end{aligned}$ | Offset Type | Offsets: <br> Horz <br> Lateral Vert $f t$ | Azimuth Adjustment | $3 d B$ <br> Beam <br> Width <br> 。 | Elevation | Outside <br> Diameter <br> ft |  | Aperture Area <br> $f t^{2}$ | Weight |
| 4' Dish | A | Paraboloid | From | 1.00 | 0.0000 |  | 125.00 | 4.00 | No Ice | 12.57 | 0.08 |
|  |  | w/Radome | Face | 0.00 |  |  |  |  | 1/2" Ice | 13.10 | 0.09 |
|  |  |  |  | 0.00 |  |  |  |  | $1^{\prime \prime}$ Ice | 13.62 | 0.10 |
| 4' Dish | B | Paraboloid | From | 1.00 | 0.0000 |  | 125.00 | 4.00 | No Ice | 12.57 | 0.08 |
|  |  | w/Radome | Leg | 0.00 |  |  |  |  | 1/2" Ice | 13.10 | 0.09 |
|  |  |  |  | 0.00 |  |  |  |  | $1^{\prime \prime}$ Ice | 13.62 | 0.10 |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation | Appurtenance | Gov. <br> Load | Deflection | Tilt | Twist | Radius of <br> Curvature |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  | Comb. | in | $\circ$ | o | 。 |
| 179.00 |  | 49 | 15.315 | 0.7831 | 0.0010 | 58663 |
| 160.00 | 13' Rotatable Platform | 49 | 12.496 | 0.7448 | 0.0006 | 17265 |
| 125.00 | 15' LP Platform | 49 | 7.547 | 0.5865 | 0.0003 | 11168 |

## Section Capacity Table

| Section | Elevation | Component |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Type |  |  |

Program Version 6.0.4.0-1/27/2012 File:O:/2012/2012801/10/tnx/4340 North Portland.eri

## APPENDIX C

Tower Elevation Drawing


DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
| :---: | :---: | :---: | :---: |
| 13' Rotatable Platform | 179 | (2) RBS 6601 | 179 |
| (2) $7770.00 \mathrm{w} / 6$ ' Mount Pipe | 179 | (2) RBS 6601 | 179 |
| (2) $7770.00 \mathrm{w} / 6^{\prime}$ Mount Pipe | 179 | DC6-48-60-18-8F | 179 |
| (2) $7770.00 \mathrm{w} / 6$ ' Mount Pipe | 179 | 15' LP Platform | 160 |
| (2) LGP21903 Diplexer | 179 | (4) DB846G90A-XY w/ Mount Pipe | 160 |
| (2) LGP21903 Diplexer | 179 | (4) DB846G90A-XY w/ Mount Pipe | 160 |
| (2) LGP21903 Diplexer | 179 | (4) DB846G90A-XY w/ Mount Pipe | 160 |
| (2) LGP21401 | 179 | 932DG65T2E-M w/Mount Pipe | 160 |
| (2) LGP21401 | 179 | 932DG65T2E-M w/Mount Pipe | 160 |
| (2) LGP21401 | 179 | 932DG65T2E-M w/Mount Pipe | 160 |
| P65-17-XLH-RR w/ Mount Pipe | 179 | 3" $\times 5$ ' Mount Pipe | 125 |
| SBNH-1D6565C w/ 5' Mount Pipe | 179 | 3" $\times$ 5' Mount Pipe | 125 |
| AM-X-CD-14-65-00T w/ Mount Pipe | 179 | 4' Dish | 125 |
| (2) RBS 6601 | 179 | 4' Dish | 125 |

## MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |  |
| :---: | :---: | :--- | :--- | :--- | :--- | :---: |
| A53-B-42 | 42 ksi | 63 ksi |  |  |  |  |

## TOWER DESIGN NOTES

1. Tower is located in Cumberland County, Maine.
2. Tower designed for Exposure C to the TIA-222-G Standard.
3. Tower designed for a 100 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 40 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: $82.1 \%$

|  | GPD Group | ${ }^{\text {Job: }}$ ME5015 (4340) NORTH PORTLAND |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | S. Main St., Suite 2531 | Project: 2012801.10 |  |  |
|  | Akron, OH 44311 |  |  |  |
|  | Phone: (330) 572-2100 | Code: TIA-222-G | Date: 04/24/12 | Scale: NTS |
|  | FAX: (330) 572-2101 | Path: O:12012120128011101tnx 43440 North Portland.eri |  | Dwg No. E-1 |



## APPENDIX D

Base Plate \& Anchor Rod Analysis
2012801.10
GPD GROUP

| Overturning Moment = Axial Force = Shear Force = | $3904.00 \mathrm{k}^{*} \mathrm{ft}$ |
| :---: | :---: |
|  | 54.00 k |
|  | 33.00 k |

Anchor Rod and Base Plate Stresses, TIA-222-G-1
ME5015 (4340) NORTH PORTLAND
Anchor Rods
(Section 4.9.9, TIA-222-G-1)
${ }^{*}$ This analysis assumes the clear distance from the top of the concrete to the bottom of the leveling nut is less than the diameter of the anchor rod. Notify GPD Group immediately if existing field conditions do not meet this assumbtion.

| Stiffeners |  |
| :---: | :---: |
| Configuration = Thickness = | Every Rod |
|  | 0.75 in |
| Width $=$Notch $=$Height $=$Stiffener Strength $\left(\mathrm{F}_{\mathrm{y}}\right)=$ | 4.5 in |
|  | 0.5 in |
|  | 8 in |
|  | 36 ksi |
| Weld Info. Known? = Vertical Weld Size = Horiz. Weld Type = | Yes |
|  | 0.375 in |
|  | Fillet |
| Fillet Size = Weld Strength = Stiffener Vertical Force = Vert. Weld Capacity = Horiz. Weld Capacity = Stiffener Capacity = | 0.375 in |
|  | 70 ksi |
|  | 37.54 kips |
|  | 39.9\% kips |
|  | 60.3\% kips |
|  | 67.3\% kips |
| Controlling Capacity = | 67.3\% OK |

## APPENDIXE

Flange Plate Analysis


Existing Flange Connection @ ME5015 (4340) NORTH PORTLAND

| Acceptable Stress |  |
| ---: | ---: |
| Ratio $=$ |  |
|  |  |
|  |  |




## Existing Flange Connection @ ME5015 (4340) NORTH PORTLAND 2012801.10

| Acceptable Stress |  |
| ---: | ---: |
| Ratio $=$ |  |
|  |  |
|  |  |


2012801.10
GPD GROUP

| Flange Bolts |  |
| :---: | :---: |
| \# Bolts = | 48 |
| Bolt Type = | A325 |
| Threads Included? = | Yes |
| Bolt Diameter = | 1 |
| Bolt Circle $=$ | 57 |
| $\phi_{\mathrm{t}}=$ | 0.75 |
| $\phi_{\mathrm{v}}=$ | 0.75 |


Prying Action Check
N/A, top flange thickness > tc

Existing Flange Connection @ ME5015 (4340) NORTH PORTLAND

| Acceptable Stress |  |
| ---: | ---: |
| Ratio $=$ |  |
|  | $105.0 \%$ |




| Flange Bolts |  |
| :---: | :---: |
| \# Bolts = | 36 |
| Bolt Type = | A325 |
| Threads Included? = | Yes |
| Bolt Diameter = | 1 |
| Bolt Circle $=$ | 51 |
| $\phi_{t}=$ | 0.75 |
| $\phi_{\mathrm{v}}=$ | 0.75 |


Prying Action Check
N/A, top flange thickness > tc


| Acceptable Stress |  |
| ---: | ---: |
| Ratio $=$ |  |
|  |  |
|  |  |


**Stiffeners ineffective - check plate unstiffened**

Existing Flange Connection @

## ME5015 (4340) NORTH PORTLAND

 2012801.10GPD GROUP

| Acceptable Stress |  |
| ---: | ---: |
| Ratio $=$ |  |
|  | $105.0 \%$ |


Tension \& Shear (TIA-222-G-1, Section 4.9.6)

| $\mathrm{F}_{\mathrm{ub}}=$ | 120 | ksi |
| :---: | :---: | :---: |
| $A_{b}=$ | 0.785398 | $\mathrm{in}^{2}$ |
| $\mathrm{A}_{\mathrm{n}}=$ | 0.606 | in ${ }^{\text {c }}$ |
| $\phi \mathrm{R}_{\mathrm{nv}}=$ | 31.81 | kips |
| $\phi \mathrm{R}_{\mathrm{nt}}=$ | 54.54 | s |
| $\mathrm{V}_{\mathrm{ub}}=$ | 0.66 | s |
| $\mathrm{T}_{\mathrm{ub}}=$ | 38.00 | k |

Prying Action Check
N/A, top flange thickness > tc

**Stiffeners ineffective - check plate unstiffened**

**Stiffeners ineffective - check plate unstiffened**

## Existing Flange Connection @ <br> ME5015 (4340) NORTH PORTLAND 2012801.10

GPD GROUP

| Acceptable Stress |  |
| ---: | ---: |
| Ratio $=$ |  |
|  |  |


Prying Action Check
N/A, top flange thickness > tc

**Stiffeners ineffective - check plate unstiffened**

Existing Flange Connection @
ME5015 (4340) NORTH PORTLAND 2012801.10
GPD GROUP


| Acceptable Stress |  |
| ---: | ---: |
| Ratio $=$ |  |
|  |  |
|  |  |


Tension \& Shear (TIA-222-G-1, Section 4.9.6)

| = | 120 | ksi |
| :---: | :---: | :---: |
| $\mathrm{A}_{\mathrm{b}}=$ | 0.785398 | $\mathrm{in}^{2}$ |
| $\mathrm{A}_{\mathrm{n}}=$ | 0.606 | $\mathrm{in}^{\text {c }}$ |
| $\phi \mathrm{R}_{\mathrm{nv}}$ | 31.81 | ps |
| $\phi \mathrm{R}_{\mathrm{nt}}$ | 54.54 | s |
| $\mathrm{V}_{\mathrm{ub}}=$ | 0.64 |  |
| $\mathrm{T}_{\mathrm{ub}}=$ | 25.42 | kips |

Prying Action Check
N/A, top flange thickness > tc

| Upper Flange Plate |  |
| :---: | :---: |
| Location = | External |
| Plate Strength $\left(\mathrm{F}_{\mathrm{y}}\right)=$ | 36 ksi |
| Plate Tensile ( $\mathrm{F}_{\mathrm{u}}$ ) $=$ | 58 ksi |
| Plate Thickness | 1.25 in |
| Outer Diameter = | 36 in |
| $\phi_{\mathrm{f}}=$ | 0.9 |
| wcalc $=$ | 13.75 in |
| wmax $=$ | 21.04 in |
|  | 13.75 in |
| $\mathrm{Z}=$ | $5.37 \mathrm{in}^{3}$ |
| $\mathrm{M}_{\mathrm{u}}=$ | 87.20 k-in |
| $\phi \mathrm{M}_{\mathrm{n}}=$ | 173.9947 k-in |
| UP Capacity = | 50.1\% OK |


| UpperStiffeners |  |
| :---: | :---: |
| Configuration = | Every Other |
| Thickness = | 0.625 in |
| Width $=$ | 3 in |
| Notch $=$ | 0.5 in |
| Height $=$ | 5 in |
| Stiffener Strength ( $\mathrm{F}_{\mathrm{y}}$ ) $=$ | 36 ksi |
| Weld Info. Known? = | Yes |
| Vertical Weld Size $=$ | 0.375 in |
| Horiz. Weld Type = | Fillet |
| Fillet Size $=$ | 0.375 in |
| Weld Strength = | 70 ksi |

**Stiffeners ineffective - check plate unstiffened**

Existing Flange Connection @

## ME5015 (4340) NORTH PORTLAND

 2012801.10GPD GROUP

| Acceptable Stress |  |
| ---: | ---: |
| Ratio $=$ |  |
|  |  |
|  |  |


Tension \& Shear (TIA-222-G-1, Section 4.9.6)

| $\mathrm{F}_{\mathrm{ub}}=$ | 120 | ksi |
| :---: | :---: | :---: |
| $\mathrm{A}_{\mathrm{b}}$ | 0.785398 | $\mathrm{in}^{2}$ |
| $\mathrm{A}_{\mathrm{n}}=$ | 0.606 | $\mathrm{in}^{\text {c }}$ |
| $\phi \mathrm{R}_{\mathrm{nv}}=$ | 31.81 | kips |
| $\phi \mathrm{R}_{\mathrm{nt}}=$ | 54.54 | S |
| $=$ | 0.40 | s |
| $\mathrm{T}_{\mathrm{ub}}=$ | 12.14 | kips |

Prying Action Check
N/A, top flange thickness > tc

| Upper Flange Plate |  |
| :---: | :---: |
| Location = | External |
| Plate Strength ( $\mathrm{F}_{\mathrm{y}}$ ) $=$ | 36 ksi |
| Plate Tensile ( $\mathrm{F}_{\mathrm{u}}$ ) $=$ | 58 ksi |
| Plate Thickness | 1.25 in |
| Outer Diameter = | 30 in |
| $\phi_{\mathrm{f}}=$ | 0.9 |
| wcalc $=$ | 12.37 in |
| wmax $=$ | 20.84 in |
|  | 12.37 in |
| $\mathrm{Z}=$ | $4.83 \mathrm{in}^{3}$ |
| $\mathrm{M}_{\mathrm{u}}=$ | 39.22 k -in |
| $\phi \mathrm{M}_{\mathrm{n}}=$ | 156.5492 k-in |
| UP Capacity = | 25.1\% OK |


| UpperStiffeners |  |
| :---: | :---: |
| Configuration $=$ | Every Other |
| Thickness $=$ | 0.625 in |
| Width $=$ | 3 in |
| Notch = | 0.5 in |
| Height $=$ | 5 in |
| Stiffener Strength ( $\mathrm{F}_{\mathrm{y}}$ ) $=$ | 36 ksi |
| Weld Info. Known? = | Yes |
| Vertical Weld Size $=$ | 0.375 in |
| Horiz. Weld Type = | Fillet |
| Fillet Size $=$ | 0.375 in |
| Weld Strength $=$ | 70 ksi |

**Stiffeners ineffective - check plate unstiffened**

**Stiffeners ineffective - check plate unstiffened**

## APPENDIX F

Foundation Analysis

Mat Foundation Analysis ME5015 (4340) NORTH PORTLAND

| General Info |  |
| :---: | :---: |
| Code | TIA-222-G |
| Bearing On | Soil |
| Foundation Type | Mono Pad |
| Pier Type | Round |
| Reinforcing Known | Yes |
| Max Capacity | 1.05 |


| Tower Reactions |  |
| :---: | :---: |
| M oment, M | $3904 \mathrm{k}-\mathrm{ft}$ |
| Axial, P | 54 k |
| Shear, V | 33 k |


| Pad \& Pier Geometry |  |  |
| :---: | :---: | :---: |
| Pier Diameter, $\varnothing$ | 7 | ft |
| Pad Length, L | 24 | ft |
| Pad Width, W | 24 | ft |
| Pad Thickness, t | 3 | ft |
| Depth, D | 12 | ft |
| Height Above Grade, HG | 0.5 | ft |


| Pad \& Pier Reinforcing |  |  |
| :---: | :---: | :--- |
| Rebar Fy | 60 | ksi |
| Concrete Fc' | 4 | ksi |
| Clear Cover | 3 | in |
| Reinforced Top \& Bottom? | Yes |  |
| Pad Reinforcing Size | $\# 10$ |  |
| Pad Quantity Per Layer | 31 |  |
| Pier Rebar Size | $\# 11$ |  |
| Pier Quantity of Rebar | 38 |  |


| Soil Properties |  |
| :---: | :---: |
| Soil Type | Cohesive |
| Soil Unit Weight | 120 pcf |
| Cohesion, Cu | 0 ksf |
| Bearing Type | Gross |
| Ultimate Bearing | 9 ksf |
| Water Table Depth | 5 ft |
| Frost Depth | 5.833 ft |

GPD M at Foundation Analysis - V1.01

| Bearing Summary |  |  | Load Case |
| :---: | :---: | :---: | :---: |
| Qxmax | 2.57 | ksf | 0.9D+1.6W |
| Qymax | 2.57 | ksf | 0.9D+1.6W |
| Qmax @ 45 ${ }^{\circ}$ | 3.10 | ksf | 0.9D+1.6W |
| $\mathrm{Q}_{\text {(all) Gross }}$ | 6.75 | ksf |  |
| Controlling Capacity | 45.9\% | Pass |  |


| Overturning Summary (Required FS=1.0) |  | Load Case |  |
| :---: | :---: | :---: | :---: |
| FS(ot)x | 1.72 | $\geq 1.0$ | $0.9 \mathrm{D}+1.6 \mathrm{~W}$ |
| FS(ot)y | 1.72 | $\geq 1.0$ | $0.9 \mathrm{D}+1.6 \mathrm{~W}$ |
| Controlling Capacity | $\mathbf{5 8 . 1} \%$ | Pass |  |



