

775 Fiero Lane, Suite 200 San Luis Obispo, CA 93401 Email: contact@snapnrack.com Phone Number: (877) 732-2860

SnapNrack Series 100 Roof Mount System COVER LETTER

The loading criteria used in this report is from ASCE 7-10. For codes that reference ASCE 7-05, Appendix A is provided to convert the wind speeds in ASCE 7-05 to the wind speeds used in this report. Instructions for this conversion are provided in Appendix A. This report covers wind speeds (V_{ult}) to 190 MPH, ground snow to 120 PSF, building heights to 60 feet, and tilt angles to 60 degrees.

The following codes are covered in this report:

- IBC 2015
- IBC 2012
- IBC 2009
- IBC 2006

The mounting system structural submittal package shall consist of the following:

- Pages 1-17 of the report (this includes this cover letter).
- Applicable page from the following:
 - o C1 C15 for 0 to 30 ft. Mean Roof Height and 6063 alloy rail
 - o C17 C32 for 31 to 60 ft. Mean Roof Height and 6063 alloy rail
 - o C33 C48 for 0 to 30 ft. Mean Roof Height and 6005 alloy rail
 - o C49 C64 for 31 to 60 ft. Mean Roof Height and 6005 alloy rail
- Appendix A (if applicable).
- The applicable installation details (listed on page 17 of this report).

This report provides structural engineering calculations and installation criteria for the mounting system only. It does not certify the capacity of the supporting members. The capacity of the supporting structure is to be certified by the licensed professional responsible for the building's structural certification.

Please contact SnapNrack at (877) 732-2860, or Contact@snapnrack.com, for questions regarding this report.

Norman Scheel, PE, SE
Fellow ASCE
Fellow SEAOC
LEED AP BD+C, LEED AP HOMES
E-mail: info@nsse.com





Structural Report and Calculations

Series 100 Roof Mount

For

SnapNrack

775 Fiero Lane, Suite 200 San Luis Obispo, CA 93401

Prepared By

Norman Scheel Structural Engineer

5022 Sunrise Boulevard Fair Oaks, CA 95628 (916) 536-9585

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Structural Report and Calculations

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Structural Report and Calculations

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Building Department Support Calculations

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Appendix: ASCE-2010 to 2005 Conversion Sheet A1

Structural Report and Calculations



Introduction

This report describes, illustrates, and explains the Structural Calculation Packet for SnapNrack's Series 100 Mounting System, dated 7/6/2016. The calculations have been performed in accordance with the codes referenced in the cover letter. The racking system has been designed to withstand code-prescribed forces due to its own weight, the weight of the solar panels, the snow loads, and both the wind and seismic forces.

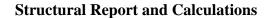
Rail Spans

This report covers two different material options for the system rails. Although they are both aluminum, one rail option uses a 6063 alloy (25 ksi yield) and the other uses a 6005 alloy (35 ksi yield).

Despite having different yield strengths, both types of rails support the PV panels. As for the rails themselves, they are supported by mounting hardware which attaches them to the roof structure with spans that are expressed in inches. Refer to the tables below for rail spans under varying conditions of rail alloy and roof height. Shaded cells require an edge zone adjustment (see details following charts).

Notes for Tables 1A thru 2H

- 1. Determine the mean roof height, tilt angle, and rail alloy (if you are unsure, use the 6063 alloy values). For mean roof heights less than 30 feet, use Table 1A/2A for tilt angles less than 19 degrees, Table 1B/2B for tilt angles between 20 and 36 degrees, Table 1C/2C for tilt angles between 37 and 45 degrees, and Table 1D/2D for tilt angles between 46 and 60 degrees. For mean roof heights between 31 and 60 feet use Table 1E/2E for tilt angles less than 19 degrees, Table 1F/2F for tilt angles between 20 and 36 degrees, Table 1G/2G for tilt angles between 37 and 45 degrees, and Table 1H/2H for tilt angles between 46 and 60 degrees.
- 2. Determine the wind and snow load for the project site from the building department. Make certain to use 2015 IBC wind loads. Locate the wind load in the table across top rows and the snow load down the left columns to find corresponding maximum rail span.
- 3. For snow loads, column Pg equals the ground snow.
- 4. Shaded cells require application of an edge zone adjustment (details to follow).





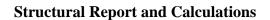
6063 Alloy Rail Tables

0-30 ft. Roof Height

	Table 1A: Rail Spans (in) for Roof Slopes and Tilt Angles 0° to 19° 6063 Alloy															
	Wind Load Vult 110 115 120 125 130 135 140 145 150 155 160 170 180 190															
	Vu	lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	q_{l}	ı	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	Pg	Ps	-10.7	-11.7	-12.7	-13.8	-14.9	-16.1	-17.3	-18.6	-19.9	-21.2	-22.6	-25.5	-28.6	-31.9
(C)	0	0	116	110	104	99	95	91	87	83	80	77	75	70	65	62
(psf)	10	8	114	110	104	99	95	91	87	83	80	77	75	70	65	62
oad	20	15	89	89	89	89	89	89	87	83	80	77	75	70	65	62
\ \ \	30	23	75	75	75	75	75	75	75	75	75	75	75	70	65	62
Snow Load	40	31	66	66	66	66	66	66	66	66	66	66	66	66	65	62
	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	60
Ground	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

0-30 ft. Roof Height

	Table 1B: Rail Spans (in) for Roof Slopes and Tilt Angles 20° to 36° 6063 Alloy															
	Wind Load Vult 110 115 120 125 130 135 140 145 150 155 160 170 180 190															
	Vu	lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	q_{l}	1	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_{g}	$\mathbf{P}_{\mathbf{s}}$	-7.0	-7.6	-8.3	-9.0	-9.7	-10.5	-11.3	-12.1	-13.0	-13.8	-14.7	-16.6	-18.7	-20.8
	0	0	120	120	120	120	120	118	112	108	103	99	95	89	83	78
Snow Load (psf)	10	8	112	111	110	109	108	107	105	104	103	99	95	89	83	78
pac	20	15	89	89	89	89	89	89	88	88	87	87	86	85	83	78
w L	30	23	75	75	75	75	75	75	75	75	75	75	75	75	74	73
Sno	40	31	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	60
Ground	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40



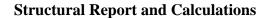


0-30 ft. Roof Height

	Table 1C: Rail Spans (in) for Roof Slopes and Tilt Angles 37° to 45° 6063 Alloy															
	Wind Load Vult 110 115 120 125 130 135 140 145 150 155 160 170 180 190															
	Vu	lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	q_h	l	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_g	P_{s}	-6.7	-7.3	-7.9	-8.6	-9.3	-10.0	-10.8	-11.6	-12.4	-13.2	-14.1	-15.9	-17.8	-19.9
(J	0	0	120	120	120	120	120	120	116	111	106	102	98	91	85	80
(bsd)	10	8	112	111	110	109	108	107	105	104	103	102	98	91	85	80
pac	20	15	89	89	89	89	89	89	88	88	87	87	86	85	83	80
» L	30	23	75	75	75	75	75	75	75	75	75	75	75	75	74	73
Snow Load	40	31	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	60
Ground	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
9	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

0-30 ft. Roof Height

	Table 1D: Rail Spans (in) for Roof Slopes and Tilt Angles 46° to 60° 6063 Alloy															
	Wind Load Vult 110 115 120 125 130 135 140 145 150 155 160 170 180 190															
	qı	h	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	Pg	Ps	-6.3	-6.9	-7.6	-8.2	-8.9	-9.6	-10.3	-11.0	-11.8	-12.6	-13.4	-15.2	-17.0	-18.9
Œ.	0	0	120	120	120	120	118	115	113	110	107	105	101	94	88	82
sd)	10	8	106	105	104	102	101	100	98	97	96	94	93	90	88	82
Snow Load (psf)	20	15	89	88	87	87	86	85	84	83	82	82	81	79	77	76
w L	30	23	75	75	75	75	75	75	75	74	74	73	72	71	70	69
Sno	40	31	66	66	66	66	66	66	66	66	66	66	66	65	64	63
	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	59
Ground	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
0	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40



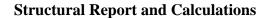


31-60 ft. Roof Height

	Table 1E: Rail Spans (in) for Roof Slopes and Tilt Angles 0° to 19° 6063 Alloy															
	Wind Load Wilt 110 115 120 125 120 125 140 145 150 155 160 170 180 100															
	Vult 110 115 120 125 130 135 140 145 150 155 160 170 180 190															
	q_h	ì	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	Pg	Ps	-12.3	-13.5	-14.7	-15.9	-17.2	-18.6	-20.0	-21.4	-22.9	-24.5	-26.1	-29.4	-33.0	-36.7
	0	0	106	101	96	91	87	83	80	77	74	71	69	64	61	57
(psf)	10	8	106	101	96	91	87	83	80	77	74	71	69	64	61	57
Load	20	15	89	89	89	89	87	83	80	77	74	71	69	64	61	57
× L	30	23	75	75	75	75	75	75	75	75	74	71	69	64	61	57
Snow	40	31	66	66	66	66	66	66	66	66	66	66	66	64	61	57
	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	57
Ground	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
9	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

31-60 ft. Roof Height

	Table 1F: Rail Spans (in) for Roof Slopes and Tilt Angles 20° to 36° 6063 Alloy															
	Wind Load Vult 110 115 120 125 130 135 140 145 150 155 160 170 180 190															
	Vu	ılt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	qı	n	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_g	$\mathbf{P}_{\mathbf{s}}$	-8.0	-8.8	-9.6	-10.4	-11.2	-12.1	-13.0	-14.0	-14.9	-16.0	-17.0	-19.2	-21.5	-24.0
	0	0	120	120	120	119	113	108	103	99	95	91	88	82	77	72
Jsd)	10	8	110	109	108	107	106	104	103	99	95	91	88	82	77	72
oad	20	15	89	89	89	89	89	88	87	86	86	85	84	82	77	72
\ V_L	30	23	75	75	75	75	75	75	75	75	75	75	75	74	73	72
Snow Load (psf)	40	31	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	60
Ground	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40



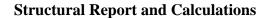


31-60 ft. Roof Height

	Table 1G: Rail Spans (in) for Roof Slopes and Tilt Angles 37° to 45° 6063 Alloy															
	Wind Load															
	Vu	lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	qh	ı	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_g	\mathbf{P}_{s}	-7.7	-8.4	-9.1	-9.9	-10.7	-11.6	-12.4	-13.3	-14.3	-15.2	-16.2	-18.3	-20.6	-22.9
	0	0	120	120	120	120	116	111	106	101	97	93	90	84	79	74
(bst)	10	8	110	109	108	107	106	104	103	101	97	93	90	84	79	74
bad	20	15	89	89	89	89	89	88	87	86	86	85	84	83	79	74
» Ľ	30	23	75	75	75	75	75	75	75	75	75	75	75	74	73	72
Snow Load	40	31	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	60
Ground	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

31-60 ft. Roof Height

		Tabl	e 1H:	Rail S	pans ((in) fo	r Roof	Slope	s and	Tilt An	gles 4	6° to 6	60° 60	063 All	oy	
								Wind	Load							
	Vu	ılt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	qı	h	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	Pg	Ps	-7.3	-8.0	-8.7	-9.5	-10.2	-11.0	-11.9	-12.7	-13.6	-14.5	-15.5	-17.5	-19.6	-21.8
	0	0	120	120	119	116	113	110	107	104	100	96	93	86	81	76
Snow Load (psf)	10	8	104	103	101	100	98	97	96	94	93	91	90	86	81	76
ad	20	15	88	87	86	85	84	83	82	81	81	80	79	77	75	73
~ Ľ	30	23	75	75	75	75	75	74	73	73	72	72	71	70	68	67
Snov	40	31	66	66	66	66	66	66	66	66	66	65	65	64	63	62
	50	39	60	60	60	60	60	60	60	60	60	60	60	60	59	58
Ground	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	54
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40





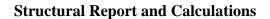
6005 Alloy Rail Tables

0-30 ft. Roof Height

		Ta	ıble 2	A: Rail	Spans	(in) fo	r Roo	f Slope	es and	Tilt Aı	ngles ()° to 1	9° <i>600</i>	05 Allo	у	
								Wind	Load							
	Vu	lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	qh	l	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	Pg	$\mathbf{P}_{\mathbf{s}}$	-10.7	-11.7	-12.7	-13.8	-14.9	-16.1	-17.3	-18.6	-19.9	-21.2	-22.6	-25.5	-28.6	-31.9
	0	0	140	132	125	119	114	109	104	100	96	93	89	84	79	74
(bst)	10	8	137	132	125	119	114	109	104	100	96	93	89	84	79	74
	20	15	106	106	106	106	106	106	104	100	96	93	89	84	79	74
¥ Ľ	30	23	90	90	90	90	90	90	90	90	90	90	89	84	79	74
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	79	79	79	74
	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	72
Ground	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

0-30 ft. Roof Height

	٦	Γable	2B: R	ail Spa	ans (in	ı) for F	Roof S	lopes	and Ti	lt Ang	les 20	° to 36	5° 60	05 Allo	рy	
							,	Wind L	oad							
	Vu	ılt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	qı	h	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_g	Ps	-7.0	-7.6	-8.3	-9.0	-9.7	-10.5	-11.3	-12.1	-13.0	-13.8	-14.7	-16.6	-18.7	-20.8
(J	0	0	144	144	144	144	144	141	135	129	124	119	114	107	100	94
(psf)	10	8	134	133	132	130	129	128	127	125	124	119	114	107	100	94
Load	20	15	106	106	106	106	106	106	106	105	105	104	103	101	100	94
w L	30	23	90	90	90	90	90	90	90	90	90	90	90	90	89	88
Snow	40	31	79	79	79	79	79	79	79	79	79	79	79	79	79	79
pu ?	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	72
Ground	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
9	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48



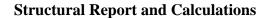


0-30 ft. Roof Height

		Tak	ole 2C	: Rail S	Spans	(in) fo	r Roof	Slope	s and	Tilt An	gles 3	7° to 4	5° 60	005 All	оу	
								Wind	l Load							
	Vu	lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	q_h		15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	$\mathbf{P}_{\mathbf{g}}$	P_{s}	-6.7	-7.3	-7.9	-8.6	-9.3	-10.0	-10.8	-11.6	-12.4	-13.2	-14.1	-15.9	-17.8	-19.9
(J	0	0	144	144	144	144	144	144	139	133	127	122	118	109	102	96
(bst)	10	8	134	133	132	130	129	128	127	125	124	122	118	109	102	96
pac	20	15	106	106	106	106	106	106	106	105	105	104	103	101	100	96
νL	30	23	90	90	90	90	90	90	90	90	90	90	90	90	89	88
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	79	79	79	79
	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	72
Ground	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
O	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

0-30 ft. Roof Height

	7	Γable	2D: R	Rail Sp	ans (ir	n) for I	Roof S	lopes	and T	ilt Ang	les 46	° to 60	o° 60	05 All	оу	
								Wind L	oad							
	Vu	lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	qı	ı	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	Pg	P_s	-6.3	-6.9	-7.6	-8.2	-8.9	-9.6	-10.3	-11.0	-11.8	-12.6	-13.4	-15.2	-17.0	-18.9
<u>_</u>	0	0	144	144	144	144	142	139	135	132	129	126	121	113	105	99
(psf)	10	8	128	126	124	123	121	120	118	116	115	113	112	109	105	99
oad	20	15	106	106	105	104	103	102	101	100	99	98	97	95	93	91
ĭ. Ľ	30	23	90	90	90	90	90	90	90	89	88	88	87	85	84	82
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	79	78	77	76
	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	71
Ground	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48



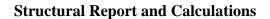


31-60 ft. Roof Height

		Ta	able 2	E: Rail	Spans	(in) fo	or Roo	f Slope	es and	Tilt A	ngles ()° to 1	9° <i>60</i>	05 All	ру	
								Wind	Load							
	Vu	lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	q _h	ı	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	Pg	$\mathbf{P}_{\mathbf{s}}$	-12.3	-13.5	-14.7	-15.9	-17.2	-18.6	-20.0	-21.4	-22.9	-24.5	-26.1	-29.4	-33.0	-36.7
	0	0	128	121	115	109	105	100	96	92	89	86	83	77	73	69
(Jsd)	10	8	128	121	115	109	105	100	96	92	89	86	83	77	73	69
Load	20	15	106	106	106	106	105	100	96	92	89	86	83	77	73	69
» L	30	23	90	90	90	90	90	90	90	90	89	86	83	77	73	69
Snow	40	31	79	79	79	79	79	79	79	79	79	79	79	77	73	69
ud 5	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	69
Ground	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

31-60 ft. Roof Height

		Table	e 2F: F	Rail Sp	ans (iı	n) for	Roof S	lopes	and T	ilt Ang	les 20	° to 3	6° <i>60</i>	05 All	оу	
								Wind I	Load							
	Vu	ılt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	q_l	h	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_g	$\mathbf{P}_{\mathbf{s}}$	-8.0	-8.8	-9.6	-10.4	-11.2	-12.1	-13.0	-14.0	-14.9	-16.0	-17.0	-19.2	-21.5	-24.0
(1)	0	0	144	144	144	142	135	129	123	118	114	109	105	98	92	87
(psf)	10	8	132	131	129	128	127	125	123	118	114	109	105	98	92	87
Load	20	15	106	106	106	106	106	105	105	104	103	102	101	98	92	87
w Ľ	30	23	90	90	90	90	90	90	90	90	90	90	90	89	87	86
Snow	40	31	79	79	79	79	79	79	79	79	79	79	79	79	79	79
	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	72
Ground	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
9	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48





31-60 ft. Roof Height

	-	Tabl	e 2G:	Rail S	pans (in) fo	r Roof	Slope	s and	Tilt An	gles 3	7° to 4	5° 60	005 All	oy	
								Wind	Load							
	Vu	ılt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	qı	h	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	Pg	Ps	-7.7	-8.4	-9.1	-9.9	-10.7	-11.6	-12.4	-13.3	-14.3	-15.2	-16.2	-18.3	-20.6	-22.9
۵	0	0	144	144	144	144	139	133	127	122	117	112	108	101	94	89
(psf)	10	8	132	131	129	128	127	125	124	122	117	112	108	101	94	89
oad	20	15	106	106	106	106	106	105	105	104	103	102	101	99	94	89
w L	30	23	90	90	90	90	90	90	90	90	90	90	90	89	87	86
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	79	79	79	79
	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	72
Ground	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

31-60 ft. Roof Height

		Tak	ole 2H	: Rail S	Spans	(in) fo	r Roof	Slope	s and	Tilt An	gles 4	6° to 6	60° 60	005 All	oy	
								Wind	Load							
	Vu	lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	qh		17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_g	P_{s}	-7.3	-8.0	-8.7	-9.5	-10.2	-11.0	-11.9	-12.7	-13.6	-14.5	-15.5	-17.5	-19.6	-21.8
<u></u>	0	0	144	144	143	139	136	132	129	125	120	115	111	104	97	91
(Jsd)	10	8	125	123	122	120	118	116	115	113	111	110	108	104	97	91
	20	15	105	104	103	102	101	100	99	98	97	96	95	92	90	88
ž Ľ	30	23	90	90	90	90	90	89	88	87	87	86	85	83	82	80
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	78	77	76	74
	50	39	72	72	72	72	72	72	72	72	72	72	72	71	70	69
Ground	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	65
9	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

Structural Report and Calculations



Rail Testing

The aluminum rails have been designed in accordance with the 2015 Aluminum Design Manual (ADM) as referenced in the IBC. Testing was conducted per the standards set forth by the IBC Section 1715; Preconstruction Load Test. The results of this testing procedure were used in comparison with the calculated values to establish the maximum uplift load allowed for the rails.

Racking Connections to the Existing Roof

Contained within the calculation packet are calculations for the connection of the rails to the roof framing. Using the sizes provided by SnapNrack, we have calculated the maximum forces that will be resisted based on the withdrawal value of the lag screws, and the strength of the aluminum components which are involved in transferring these forces from the rail to the roof framing. These components consist of the flashed L-foot (SnapNrack Drawing PEN-D01), Standoff (PEN-D02, D03), Seam Clamp (PEN-D04), Corrugated Block (PEN-D05), Metal Roof Base (PEN-D09, D10, D11, D12) and Hanger Bolt (PEN-D06). All (6) options are acceptable under the parameters shown in SnapNrack's plans. The results from our analysis have been integrated into the summary charts.

The connection of the PV racking system to the roof will use a 5/16" diameter Lag Bolt installed with a minimum 2 ½" embedment into the framing member. Bolts shall be installed to a rafter or blocking capable of supporting both wind and seismic loads along with the weight of the PV system.

When PEN-D07 is involved, use minimum quantity 2 ¼-20 lag bolts with minimum 1.25" embedment. In addition, SnapNrack's Tile Roof Hooks (Drawing PEN-D13, D14) are also acceptable attachment components when the following limitations are followed:

- 1. tile roof hooks have been reviewed up to 120 mph, Design Wind Speed
- 2. rail span is limited to 6 feet with tile roof hooks





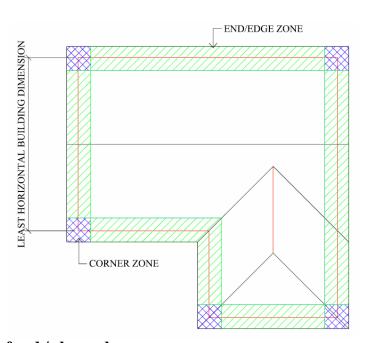
Summary Charts and Topographic Factors

The attached pages of this summary contain some of the most common building configurations with varying wind speeds. These charts serve as quick references for looking up maximum rail spans based on the building and site conditions. However, it must be noted that for any building where a topographic factor is applied (e.g. hills, mesas, seashore), the rail span lengths given might exceed what is allowed for the given site condition. In that case, a registered structural engineer shall evaluate the exact topographic conditions for the specific site.

End Zone and Edge Distances

The edge zones and/or end zones of the roof area shall be determined based on the building's least horizontal dimension (LDH). The edge zone, "a", is equal to 10% of the LDH where a = .1 * LDH. It should be noted that if the solar panels installed cross two different roof sections, the smaller LDH shall be used.

Rail spans in the corner zone shall be a maximum of 24 inches and this restriction will only apply to the rail attachments located in the end and edge zones (does not apply to modulus or rails that overhang into the zone). Furthermore, all edge zones requiring an adjustment (shaded cells in chart) shall be reduced by 24 inches to a minimum of 32 inches.



Detail 1 roof end /edge and corner zones

Structural Report and Calculations



Site – Specific Analysis

A site-specific analysis is required if the location of the solar panel installation corresponds to any of the following criteria:

- The total pitch of the solar panel (solar panel pitch & roof pitch) is greater than 60 degrees above the horizontal.
- A topographic factor applied to a location. Generally, topographic factors are applied when the structure is on a hill, mesa or bluff, or is adjacent to a large body of water. For complete descriptions of topographic factors, please refer to ASCE 7-10 section 26.8
- The mean roof height of the structure that the solar panels will be installed on is greater than 60 ft. above grade.
- A combination of loads and/or site conditions applied that is not addressed in the attached rail span charts.

If one or more of these factors corresponds to the project location, please contact NSSE, and we will analyze the site conditions and recommend standoff spacing for each specific site.

Existing Building Limitations

This summary letter addresses the structural adequacy of the solar racking system only and does <u>not</u> investigate or validate the adequacy of the structure the racking system is being placed upon. It does <u>not</u> address the ability of the existing roofing or roof framing to support the new loads imposed upon them by the new system, <u>nor</u> does it address the new localized forces between the roofing and the roof framing which might be imposed by the new standoff connections. It also does <u>not</u> address the additional lateral forces imposed upon the building due to the seismic and wind forces that the new system will add to the existing roof. These various building-specific issues need to be evaluated by the appropriate registered professional(s) prior to the addition of the photovoltaic and racking systems. NSSE may be consulted for building-specific structural evaluation. NSSE assumes the systems will be installed to the specifications presented here and the installer will use good structural judgment.



Structural Report and Calculations

Please note that all sizes, materials specifications, and weights have been provided by SnapNrack. Installation must be in accordance with SnapNrack drawings as noted:

Drawing Title	Revision
S100-D01	F
S100-D02	F
S100-D03	F
S100-D03	F
S100-D04	F
S100-D05	F
S100-D06	F
S100-D07	F
S100-D08	F
S100-D09	F
S100-D10	F
S100-D11	F
PEN-D01	F
PEN-D02	F
PEN-D03	F
PEN-D04	F
PEN-D05	F
PEN-D06	F
PEN-DO7	F
PEN-D08	F
PEN-D09	F
PEN-D10	F
PEN-D11	F
PEN-D12	F
PEN D13	F
PEN D14	F

Please see SnapNrack plans for limits on the bolt parameters. Torque all 5/16" diameter hardware as specified in SnapNrack's plans (10-16 ft-lbs for Silver Stainless Steel and 7-9ft –lbs for black Stainless Steel, unless otherwise noted). All waterproofing, roofing and drainage issues are the responsibility of SnapNrack's customer(s) otherwise known as the contractor(s) or the professional solar installer(s).

Please let us know if you have any questions.

Norman Scheel PE, SE LEED-AP BD+C, LEED-AP Homes Fellow SEAOC Fellow A.S.C.E.

Wind Design ASCE 7-10 Main Force Resisting System 6063 Alloy Rail



Mean Roof Height

0 1

to 30

ft

1110011 1100----

Risk Category: II (Table 1.5-2)

Wind Exposure Category

 \mathbf{C}

Velocity Pressure 28.3.2 ASCE 7-10

 $q_z = q_h = 0.00256 k_z k_{zt} k_d V^2$

 $k_z = 0.98$ Velocity Pressure Exposure Coefficients (Table 26.8-1)

 $K_{zt} = 1.00$ Topographic Factor (Fig. 26.8-1)

 $K_d = 0.85$ Wind Directionality Factor (Table 26.6-1)

				Ve	locity	Pressur	es							
Wind Speed	110	115	120	125	130	135	140	145	150	155	160	170	180	190
q_{h}	25.80	28.20	30.71	33.32	36.04	38.86	41.80	44.84	47.98	51.23	54.59	61.63	69.09	76.98
ASD (0.6W)	15.48	16.92	18.42	19.99	21.62	23.32	25.08	26.90	28.79	30.74	32.75	36.98	41.46	46.19

$$P = q_h [GC_{pf} - GC_{pi}]$$

 q_h = Velocity Pressure (psf)

 GC_{pi} = +/- Internal Pressure Coefficient GC_{pf} = External Pressure Coefficient

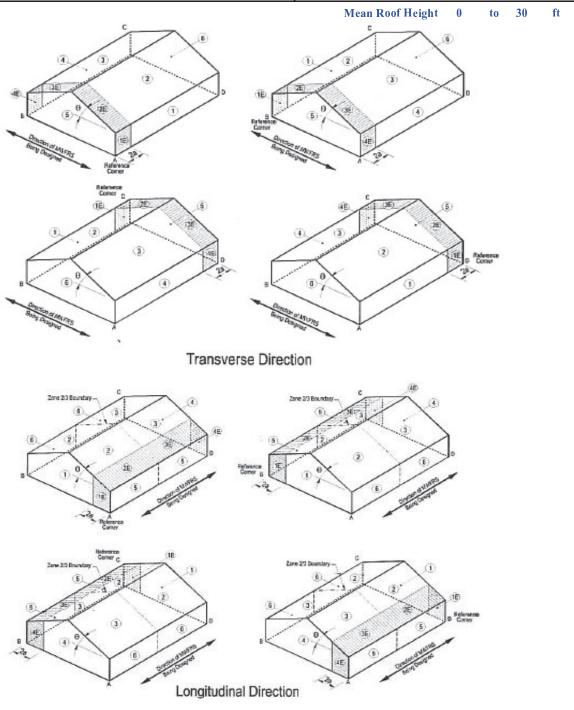
	$\mathrm{GC}_{\mathrm{pf}}$	Roof Zones	Fig 28.4-1 A	SCE 7-10	
Pitch	Slope	Zone 2	Zone 3	Zone 2E	Zone 3E
0/12	0.0	-0.69	-0.37	-1.07	-0.53
1/12	4.8	-0.69	-0.37	-1.07	-0.53
2/12	9.5	-0.69	-0.40	-1.07	-0.53
3/12	14.0	-0.69	-0.44	-1.07	-0.53
4/12	18.4	-0.69	-0.47	-1.07	-0.54
5/12	22.6	-0.45	-0.35	-0.72	-0.65
6/12	26.6	-0.10	-0.15	-0.19	-0.58
7/12	30.3	0.21	-0.43	0.27	-0.53
8/12	33.7	0.21	-0.43	0.27	-0.53
9/12	36.9	0.21	-0.43	0.27	-0.53
10/12	39.8	0.21	-0.43	0.27	-0.53
11/12	42.5	0.21	-0.43	0.27	-0.53
12/12	45.0	0.21	-0.43	0.27	-0.53
21/12	60.0	0.32	-0.41	0.40	-0.51

Notes

- 1) GCpi equal + 0.10 based on published data from the Solar America Board for Codes and Standards.
- 2) Wind Exposure B and C covered in this document.

Wind Design ASCE 7-10 Main Force Resisting System 6063 Alloy Rail





of

Zone Locations Main Force Resisting Systems ASCE 7-10

Wind Design ASCE 7-10 Components and Cladding Walls 6063 Alloy Rail



Mean Roof Height

0 t

30

ft

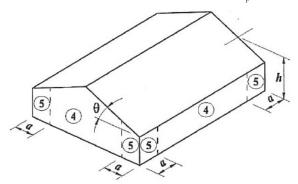
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

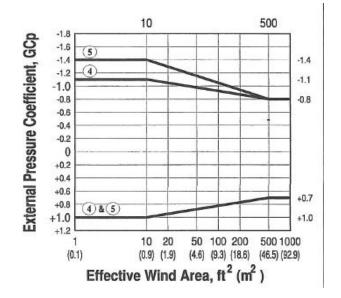
 q_h = Velocity Pressure (psf)

 $GC_{pi} = +/-$ Internal Pressure Coefficient

GC_p = External Pressure Coefficient



GC _p Walls (Fig. 30.4-1)					
Slope in Degrees Zone 4 Zone 5 Zone 4 & 5					
0 to 10	-1.00	-1.27	0.91		
10 to 45	-1.10	-1.39	-1.00		



Notes

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) $Edge\ distance\ a=0.1*LDH\ (Least\ Horizontal\ Dimension)$
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel

5022 Sunrise Boulevard Fair Oaks CA 95628 (916) 536-9585

Wind Design ASCE 7-10 Components and Cladding Roof 0 to 7 degrees for 6063 Alloy Rail



Mean Roof Height

30

ft

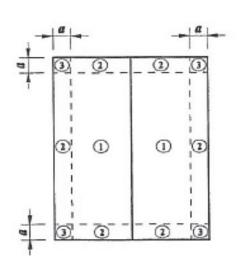
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

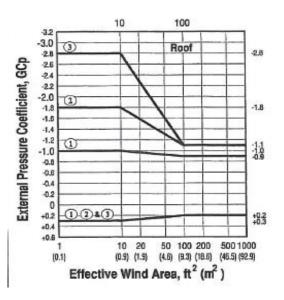
$$P = q_h [GC_p - GC_{pi}]$$

Velocity Pressure (psf)

 $GC_{\mathfrak{p}\mathrm{i}}$ +/- Internal Pressure Coefficient

 $GC_{\mathfrak{p}}$ External Pressure Coefficient





GC _p Roofs Fig. 30.4-2A					
Slope in Degrees Zone 1 Zone 2 Zone 3 Zone 1,2,3					
0 to 7	-0.99	-1.71	-2.59	0.29	

5022 Sunrise Boulevard Fair Oaks CA 95628 (916) 536-9585

Notes

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel

Wind Design ASCE 7-10 Components and Cladding Roof 7 to 27 degrees for 6063 Alloy Rail



Mean Roof Height

0

30

ft

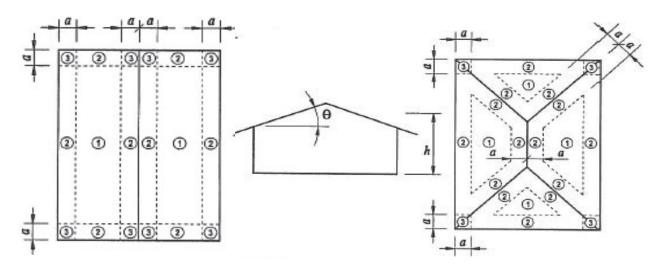
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

 q_h = Velocity Pressure (psf)

 $GC_{pi} = +/-$ Internal Pressure Coefficient

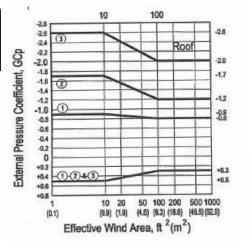
GC_p = External Pressure Coefficient



GC _p Roofs Fig. 30.4-2B					
Slope in Degrees	Zone 1	Zone 2	Zone 3	Zone 1,2,3	
7 to 27	-0.89	-1.64	-2.53	0.48	

Notes

- 1) Roof slopes from 0 $^{\circ}$ to 45 $^{\circ}$
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel



Page

Wind Design ASCE 7-10 Components and Cladding Roof 27 to 45 degrees for 6063 Alloy Rail



Mean Roof Height

0

30

ft

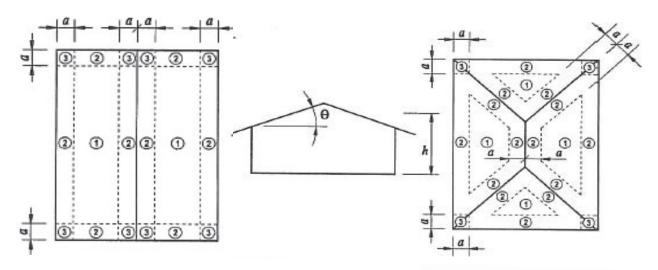
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

 q_h = Velocity Pressure (psf)

 $GC_{pi} = +/-$ Internal Pressure Coefficient

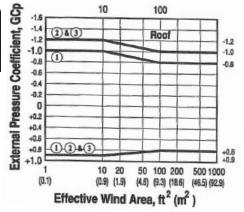
GC_p = External Pressure Coefficient



GC _p Roofs Fig. 30.4-2C					
Slope in Degrees	Zone 1	Zone 2	Zone 3	Zone 1,2,3	
27 to 45	-0.98	-1.18	-1.18	0.89	

Notes

- 1) Roof slopes from 0 $^{\circ}$ to 45 $^{\circ}$
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel



Seismic Design ASCE 7-10 Chapter 11 and 13 6063 Alloy Rail



Mean Roof Height

ASCE 7-10 Seismic Design Section 13.6.9

Site Class	ification	D	Default "D"			
Seismic U	se Group	II	Table 11.5-1			
R_p	=	2.5	Input from Table 1	3.6-1 ASCE 7-10		
A_p	=	1.0	Input from Table 1	3.6-1 ASCE 7-10		
I_p	=	1.0	Input from Table 1	1.5-1 ASCE 7-10		
S_s	=	3.0	Input from USGS	Program		
S_1	=	1.5	Input from USGS	Program		
F_a	=	1.0	Site Coefficient Ta	able 11.4-1		
F_{v}	=	1.5	Site Coefficient Ta	able 11.4-2		
S_{ms}	=	3.0	ASCE 7-10 Section	n 11.4.3		
S_{m1}	=	2.3	ASCE 7-10 Section	n 11.4.3		
S_{ds}	=	2.0	ASCE 7-10 Section	n 11.4.3		
S_{d1}	=	1.5	ASCE 7-10 Section	n 11.4.3		
Z	=	30.5	Height at point of	Attachment (ft.)		
h	=	30.0	Average Roof Heig	ght of Structure (ft.)		
F_p	=	0.97	Wp			
$F_{p \text{ max}}$	=	3.20	Wp	(Eq. 13.3.1)		
$F_{p \; min}$	=	0.60	Wp	$\mathbf{F}_{\mathbf{p}} = \frac{\mathbf{0.4 a}}{\mathbf{A}}$	$\frac{_{p} S_{DS} W_{p}}{2}$ (1+2 - z	-)
Use F _p	=	0.97	Wp	(-	$\frac{R_{p}}{I_{p}} \frac{S_{DS} W_{p}}{I_{p}} (1+2\frac{z}{h})$	
				(Eq. 13.3.2)	$F_p = 1.6 S_{DS} I_p W_p$	Max
				(Eq. 13.3.3)	$F_p = 0.3 S_{DS} I_p W_p$	Min

Vertical Accelerations

$$0.20$$
 (S_{ds}) W_p

Notes

1) Based on an average deal load of 4 psf the anticipated maximum seismic load is approximately 4 psf with a vertical accelerations of 1.6 psf wind loads govern the design of the PV system.

Page

Snow Loads ASCE 7-10 Chapter 7 6063 Alloy Rail



Mean Roof Height 0

to

30

ft

ASCE 7-10 Snow Loads Chapter 7

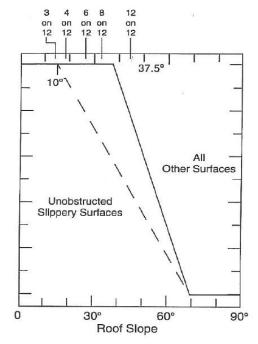
 $P_f = 0.7 C_e C_t I P_g$

 $P_s = C_s P_f$

Snow Load Chart					
Ground Snow Pg	Flat Roof P _f	Sloped Roof P _s	Sloped Roof P _s		
Ground Show 1 g	Tiat Root I f	Slope < 9/12	Slope 9/12 to 12/12		
10 psf	8	8	8		
20 psf	15	15	15		
30 psf	23	23	23		
40 psf	31	31	31		
50 psf	39	39	39		
60 psf	46	46	46		
70 psf	54	54	54		
80 psf	62	62	62		
100 psf	77	77	77		
120 psf	92	92	92		

Calculations for Snow Loads Chapter 7

 C_e = 1.00 Exposure Factor (Section 7.3.1) C_t = 1.10 Thermal Factor (Section 7.3.2) I = 1.00 Importance Factor (Section 7.3.3)



7-2b: Cold roofs with $C_t=1.1$

Page

Rail Properties for 6063 Alloy Rail



Mean Roof Height

30 to

ft

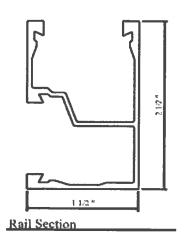
Rail Properties for Downward Loads

Section Properties

Α	=	0.63	1n-
S	=	0.34	in ³
I	=	0.46	in^4
	Stresses		
F_b	=	15.2	ksi
F_v	=	15.2	ksi
E	=	10000	ksi
$M_{\rm allow}$	=	5.17	k-in

6.38

k

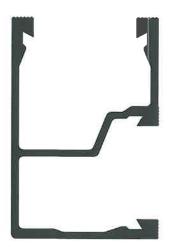


Rail Properties for Upward Loads

 V_{allow}

Section Properties

Α	=	0.41	in^2
S	=	0.25	in^3
I	=	0.11	in^4
	Stresses		
$\mathbf{F}_{\mathtt{b}}$	=	15.2	ksi
$\mathbf{F_v}$	=	15.2	ksi
E	=	10000	ksi
.5			
M_{allow}	=	3.84	k-in
V_{allow}	=	4.16	k



SnapNrack Standard Rail 6063 Alloy

Notes

- 1) Rail section properties determined from test data.
- 2) Rail test date performed per guidelines of chapter 17 of the 2015 IBC.
- 3) This report is using 6063 Alloy Rail

PV panel Calculations & Component and Cladding Forces 6063 Alloy Rail



Mean Roof Height

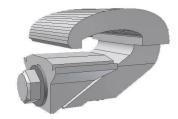
30

PV Panel Calculations for 39" x 65" Panel Connections

Panel Dimensions

65" Long Panels

Panel Width	=	39.0	in
Panel Length	=	65.0	in
Panel Weight	=	70.4	#
Panel Area	=	17.6	ft^2



Universal End Clamp

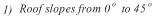
Wind Loading

ASCE 7-10 Component and Cladding

Wind Speed	110 to 190 mph
Exposure Cat.	C

Edge Distance (a) 4 Ft

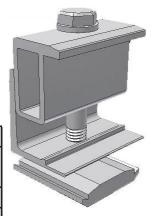
Component and Cladding					
Loading	Zone 1	Zone 2	Zone 3	Zones 1, 2, & 3	
Max	-22.96	-30.71	-30.71	68.51	
Min	-76.21	-128.56	-197.85	12.64	

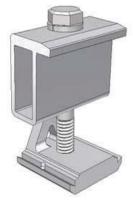


- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) $Edge\ distance\ a=0.1*LDH\ (Least\ Horizontal\ Dimension)$

Maria Baran						
	Maximum	Force at Mount	ing Bracket			
	Component and Cladding					
Loading Zone 1 Zone 2 Zone 3 Zones 1, 2, & 3						
End Clamp	-335	-566	-871	302		
Int. Clamp	-671	-1132	N/A	603		

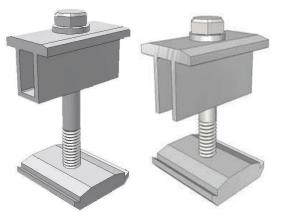
- 1) 4 brackets minimum per PV panel to rail connection
- 2) Only one corner of one PV panel may be located in zone 3
- 3) Zone 2 may have multiple panels located in this zone





Adjustable End Clamp

X-Clamp



Mid Clamp 1

Mid Clamp 2

PV panel Calculations & Component and Cladding Forces 6063 Alloy Rail



Mean Roof Height

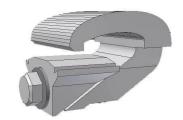
30

PV Panel Calculations for 39" x 78" Panel Connections

Panel Dimensions

78" Long Panels

Panel Width	=	39.0	in
Panel Length	=	78.0	in
Panel Weight	=	84.5	#
Panel Area	=	21.1	ft^2



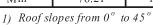
Universal End Clamp

Wind Loading

ASCE 7-10 Component and Cladding

Wind Speed	110 to 190 mph
Exposure Cat.	C
Edge Distance (a)	4 Ft

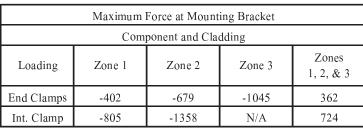
Component and Cladding											
Loading Zone 1 Zone 2 Zone 3 Zones 1, 2, & 3											
Max	-22.96	-30.71	-30.71	68.51							
Min	-76.21	-128.56	-197.85	12.64							



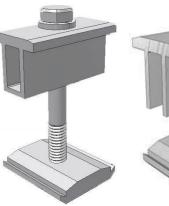
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) $Edge\ distance\ a=0.1*LDH\ (Least\ Horizontal\ Dimension)$



X-Clamp



- 1) 4 brackets minimum per PV panel to rail connection
- 2) Only one corner of one PV panel may be located in zone 3
- 3) Zone 2 may have multiple panels located in this zone



Mid Clamp 1

Mid Clamp 2

Lag Bolt Design 2012 NDS for 6063 Alloy Rail



Mean Roof Height

30

Lag Bolt Calculations for Roof Connection 65" long Panel

Bolt Connection to Roof Structure

2012 National Design Specifications 5/16" Diameter Lag Bolt 2 1/2" min. embedment into framing member

Allowable Tension 258 #/in 1.81 in Embedment length Duration of Load 1.6 wind Allowable Tension 747.2 # Allowable Uplift 339.6 #

	65" Long Panels											
Maxii	Maximum Wind Uplift (psf) per Span Based On Lag Bolt											
Span Zone 2 Zone 3 Zone 2E Zone 31												
2 ft	62.7	62.7	62.7	125.4								
4 ft	31.3	31.3	31.3	62.7								
6 ft	20.9	20.9	20.9	41.8								
8 ft												

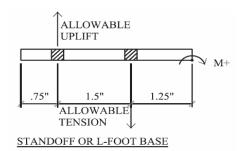
Lag Bolt Calculations for Roof Connection 78" long Panel

Bolt Connection to Roof Structure

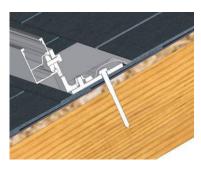
2012 National Design Specifications 5/16" Diameter Lag Bolt 2 1/2" min. embedment into framing member

Allowable Tension 258 #/in Embedment length 1.81 in Duration of Load 1.6 wind Allowable Tension 747.2 # 339.6 # Allowable Uplift

78" Long Panels										
Maximum Wind Uplift (psf) per Span Based On Lag Bolt										
Span	Span Zone 2 Zone 3 Zone 2E Zone 3E									
2 ft	52.2	52.2	52.2	104.5						
4 ft	26.1	26.1	26.1	52.2						
6 ft	17.4	17.4	17.4	34.8						
8 ft	13.1	13.1	13.1	26.1						







Notes

1) Only one corner of one PV panel may be located in zone 3E

Rail Spans per ASCE 7-10 Loads Tilt Angle 0 to 19 degrees for 6063 Alloy Rail



Mean Roof Height

0

30

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angle 0 to 19 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	lh	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_{g}	$P_{\rm s}$	-10.7	-11.7	-12.7	-13.8	-14.9	-16.1	-17.3	-18.6	-19.9	-21.2	-22.6	-25.5	-28.6	-31.9
	0	0	116	110	104	99	95	91	87	83	80	77	75	70	65	62
	10	8	114	110	104	99	95	91	87	83	80	77	75	70	65	62
(bst)	20	15	89	89	89	89	89	89	87	83	80	77	75	70	65	62
) pac	30	23	75	75	75	75	75	75	75	75	75	75	75	70	65	62
Snow Load	40	31	66	66	66	66	66	66	66	66	66	66	66	66	65	62
Sno	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	60
	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- $8. \ \ 0.6D + 0.7E$
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

Rail Spans per ASCE 7-10 Loads Tilt Angle 19 to 37 degrees for 6063 Alloy Rail



Mean Roof Height

0

o 30

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angle 20 to 36 Degrees													egrees		
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	lh	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_{g}	$P_{\rm s}$	-7.0	-7.6	-8.3	-9.0	-9.7	-10.5	-11.3	-12.1	-13.0	-13.8	-14.7	-16.6	-18.7	-20.8
	0	0	120	120	120	120	120	118	112	108	103	99	95	89	83	78
_	10	8	112	111	110	109	108	107	105	104	103	99	95	89	83	78
(bst)	20	15	89	89	89	89	89	89	88	88	87	87	86	85	83	78
) pac	30	23	75	75	75	75	75	75	75	75	75	75	75	75	74	73
Snow Load	40	31	66	66	66	66	66	66	66	66	66	66	66	66	66	66
Sno	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	60
	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

Rail Spans per ASCE 7-10 Loads Tilt Angle 37 to 45 degrees for 6063 Alloy Rail



Mean Roof Height

0

30

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angle 37 to 45 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	Ç	lh	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_{g}	$P_{\rm s}$	-6.7	-7.3	-7.9	-8.6	-9.3	-10.0	-10.8	-11.6	-12.4	-13.2	-14.1	-15.9	-17.8	-19.9
	0	0	120	120	120	120	120	120	116	111	106	102	98	91	85	80
_	10	8	112	111	110	109	108	107	105	104	103	102	98	91	85	80
Snow Load (psf)	20	15	89	89	89	89	89	89	88	88	87	87	86	85	83	80
) pac	30	23	75	75	75	75	75	75	75	75	75	75	75	75	74	73
M C	40	31	66	66	66	66	66	66	66	66	66	66	66	66	66	66
Sno	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	60
	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

Rail Spans per ASCE 7-10 Loads Tilt Angle 45 to 60 degrees for 6063 Alloy Rail



Mean Roof Height

0

30

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angles 46 to 60 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	lh	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_{g}	$P_{\rm s}$	-6.3	-6.9	-7.6	-8.2	-8.9	-9.6	-10.3	-11.0	-11.8	-12.6	-13.4	-15.2	-17.0	-18.9
	0	0	120	120	120	120	118	115	113	110	107	105	101	94	88	82
	10	8	106	105	104	102	101	100	98	97	96	94	93	90	88	82
(bst)	20	15	89	88	87	87	86	85	84	83	82	82	81	79	77	76
) pac	30	23	75	75	75	75	75	75	75	74	74	73	72	71	70	69
Snow Load	40	31	66	66	66	66	66	66	66	66	66	66	66	65	64	63
Sno	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	59
	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

Wind Design ASCE 7-10 Main Force Resisting System 6063 Alloy Rail



Mean Roof Height 30

ft

Risk Category: II (Table 1.5-2)

Wind Exposure Category

 \mathbf{C}

Velocity Pressure 28.3.2 ASCE 7-10

$$q_z = q_h = 0.00256 k_z k_{zt} k_d V^2$$

Velocity Pressure Exposure Coefficients (Table 26.8-1) 1.13

Topographic Factor (Fig. 26.8-1) K_{zt} 1.00

Wind Directionality Factor (Table 26.6-1) 0.85

Velocity Pressures														
Wind Speed	110	115	120	125	130	135	140	145	150	155	160	170	180	190
q_{h}	29.75	32.52	35.41	38.42	41.56	44.81	48.19	51.70	55.32	59.07	62.95	71.06	79.67	88.77
ASD (0.6W)	17.85	19.51	21.24	23.05	24.93	26.89	28.92	31.02	33.19	35.44	37.77	42.64	47.80	53.26

$$P = q_h [GC_{pf} - GC_{pi}]$$

Velocity Pressure (psf)

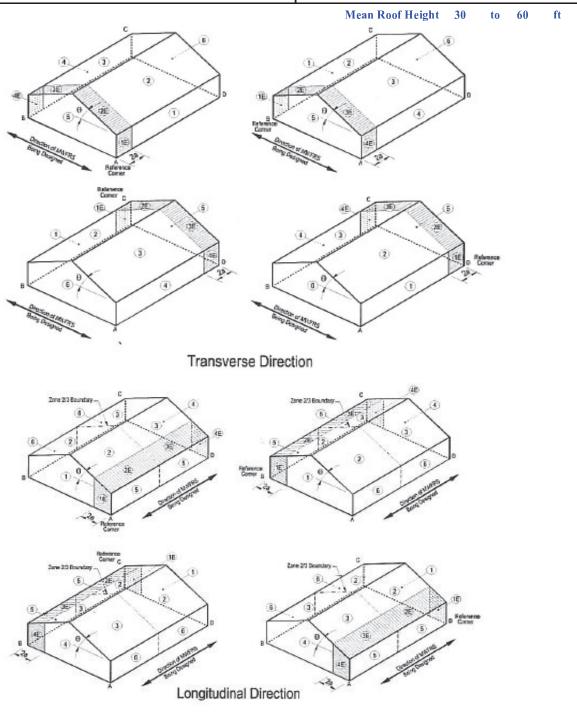
+/- Internal Pressure Coefficient GC_{pi} External Pressure Coefficient GC_{pf}

	GC_{pf}	Roof Zones	Fig 28.4-1 A	SCE 7-10	
Pitch	Slope	Zone 2	Zone 3	Zone 2E	Zone 3E
0/12	0.0	-0.69	-0.37	-1.07	-0.53
1/12	4.8	-0.69	-0.37	-1.07	-0.53
2/12	9.5	-0.69	-0.40	-1.07	-0.53
3/12	14.0	-0.69	-0.44	-1.07	-0.53
4/12	18.4	-0.69	-0.47	-1.07	-0.54
5/12	22.6	-0.45	-0.35	-0.72	-0.65
6/12	26.6	-0.10	-0.15	-0.19	-0.58
7/12	30.3	0.21	-0.43	0.27	-0.53
8/12	33.7	0.21	-0.43	0.27	-0.53
9/12	36.9	0.21	-0.43	0.27	-0.53
10/12	39.8	0.21	-0.43	0.27	-0.53
11/12	42.5	0.21	-0.43	0.27	-0.53
12/12	45.0	0.21	-0.43	0.27	-0.53
21/12	60.0	0.32	-0.41	0.40	-0.51

- 1) GCpi equal + -0.10 based onpublished data from the Solar America Board for Codes and
- 2) Wind Exposure B and C covered in this document.

Wind Design ASCE 7-10 Main Force Resisting System 6063 Alloy Rail





of

Zone Locations Main Force Resisting Systems ASCE 7-10

Wind Design ASCE 7-10 Components and Cladding Walls 6063 Alloy Rail



Mean Roof Height

60

ft

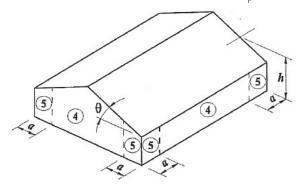
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

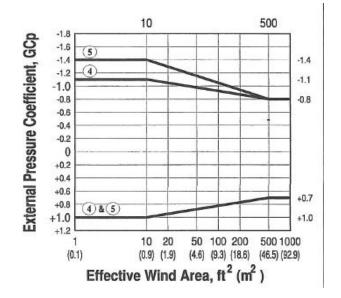
Velocity Pressure (psf)

+/- Internal Pressure Coefficient $GC_{\mathfrak{p}i}$

 $GC_{\mathfrak{p}}$ External Pressure Coefficient



GC _p Walls (Fig. 30.4-1)			
Slope in Degrees	Zone 4	Zone 5	Zone 4 & 5
0 to 10	-1.00	-1.27	0.91
10 to 45	-1.10	-1.39	-1.00



Notes

- 1) Roof slopes from 0° to 45 $^{\circ}$
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) $Edge\ distance\ a=0.1*LDH\ (Least\ Horizontal\ Dimension)$
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel

of

5022 Sunrise Boulevard Fair Oaks CA 95628 (916) 536-9585

Wind Design ASCE 7-10 Components and Cladding Roof 0 to 7 degrees for 6063 Alloy Rail



Mean Roof Height

60

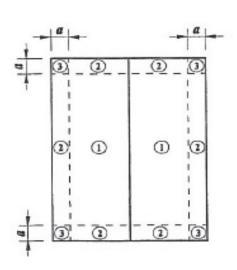
ft

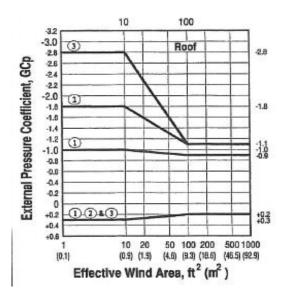
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$\mathbf{P} = \mathbf{q_h} \left[\mathbf{GC_p} - \mathbf{GC_{pi}} \right]$$

Velocity Pressure (psf)

 GC_{pi} +/- Internal Pressure Coefficient $GC_{\mathfrak{p}}$ External Pressure Coefficient





GC _p Roofs Fig. 30.4-2A					
Slope in Degrees Zone 1 Zone 2 Zone 3 Zone 1,2,3					
0 to 7	-0.99	-1.71	-2.59	0.29	

5022 Sunrise Boulevard Fair Oaks CA 95628 (916) 536-9585

Notes

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel

Wind Design ASCE 7-10 Components and Cladding Roof 7 to 27 degrees for 6063 Alloy Rail



Mean Roof Height

60

ft

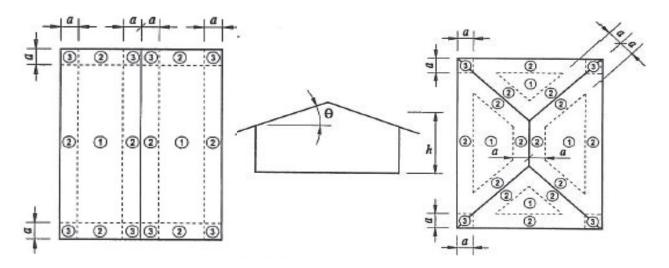
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

Velocity Pressure (psf)

 GC_{pi} +/- Internal Pressure Coefficient

 $GC_{\mathfrak{p}}$ External Pressure Coefficient

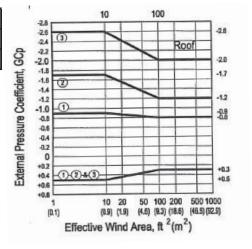


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GC _p Roofs Fig. 30.4-2B					
Slope in Degrees Zone 1 Zone 2 Zone 3 Zone 1,2,3					
7 to 27	-0.89	-1.64	-2.53	0.48	

Notes

- 1) Roof slopes from 0 $^{\circ}$ to 45 $^{\circ}$
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel



Wind Design ASCE 7-10 Components and Cladding Roof 27 to 45 degrees for 6063 Alloy Rail



Mean Roof Height 30

to (

60

ft

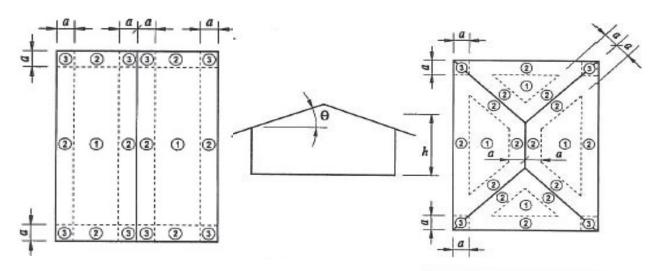
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

 q_h = Velocity Pressure (psf)

 $GC_{pi} = +/-$ Internal Pressure Coefficient

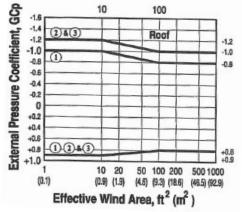
GC_p = External Pressure Coefficient



GC _p Roofs Fig. 30.4-2C					
Slope in Degrees	Zone 3	Zone 1,2,3			
27 to 45	-0.98	-1.18	-1.18	0.89	

Notes

- 1) Roof slopes from 0° to 45 $^{\circ}$
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel



Seismic Design ASCE 7-10 Chapter 11 and 13 Alloy Rail

6063



Mean Roof Height 30 to

to 60

ASCE 7-10 Seismic Design Section 13.6.9

Site Classificat	ion	D	Default "D"						
Seismic Use G	roup	II	Table 11.5-1						
R_p	=	2.5	Input from Table	13.6-1 ASC	E 7-10				
A_p	=	1.0	Input from Table	13.6-1 ASC	E 7-10				
I_p	=	1.0	Input from Table	11.5-1 ASC	E 7-10				
S_s	=	3.0	Input from USGS	Program					
S_1	=	1.5	Input from USGS	Program					
F_a	=	1.0	Site Coefficient T	Table 11.4-1					
$F_{\rm v}$	=	1.5	Site Coefficient T	Table 11.4-2					
S_{ms}	=	3.0	ASCE 7-10 Section	on 11.4.3					
S_{m1}	=	2.3	ASCE 7-10 Section	on 11.4.3					
S_{ds}	=	2.0	ASCE 7-10 Section	on 11.4.3					
S_{d1}	=	1.5	ASCE 7-10 Section	on 11.4.3					
Z	=	60.5	Height at point of	Attachment	(ft.)				
h	=	60.0	Average Roof He	ight of Struc	ture (ft.)				
F_{p}	=	0.97	Wn		(Eq. 13.3.	.1)			
F _{p max}	=	3.20	•		` -	- 1	Spc Wn	7.	
F _{p min}	=	0.60	_		$\mathbf{F}_{\mathbf{p}} = $	р	$\frac{S_{DS} W_p}{R_p}$ (1+	-2 -2 h	-)
р нин			··· <u>r</u>			(-	$\frac{P}{I_p}$		
Use F _p	=	0.97	Wp		(Eq. 13.3	.2)	$\mathbf{F}_{\mathbf{p}} = 1.6 \; \mathbf{S}_{\mathbf{DS}} \; \mathbf{I}$	$I_p W_p$	Max
					(Eq. 13.3	.3)	$\mathbf{F}_{\mathbf{p}} = 0.3 \mathbf{S}_{\mathbf{DS}}$	$\mathbf{I}_{p} \; \mathbf{W}_{p}$	Min

Vertical Accelerations

$$0.20$$
 (S_{ds}) W_p

Notes

1) Based on an average deal load of 4 psf the anticipated maximum seismic load is approximately 4 psf with a vertical accelerations of 1.6 psf wind loads govern the design of the PV system.

Snow Loads ASCE 7-10 Chapter 7 6063 Alloy Rail



Mean Roof Height 30 to 60

ft

ASCE 7-10 Snow Loads Chapter 7

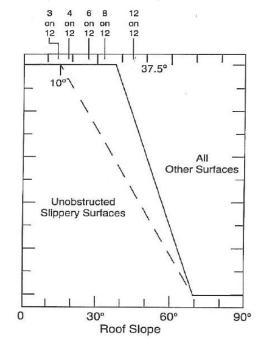
 $P_f = 0.7 C_e C_t I P_g$

 $P_s = C_s P_f$

Snow Load Chart					
Ground Snow Pg	Flat Roof P _f	Sloped Roof P _s	Sloped Roof P _s		
Ground Show 1 g	1 lat 1001 1 ₁	Slope < 9/12	Slope 9/12 to 12/12		
10 psf	8	8	8		
20 psf	15	15	15		
30 psf	23	23	23		
40 psf	31	31	31		
50 psf	39	39	39		
60 psf	46	46	46		
70 psf	54	54	54		
80 psf	62	62	62		
100 psf	77	77	77		
120 psf	92	92	92		

Calculations for Snow Loads Chapter 7

 C_e = 1.00 Exposure Factor (Section 7.3.1) C_t = 1.10 Thermal Factor (Section 7.3.2) I = 1.00 Importance Factor (Section 7.3.3)



7-2b: Cold roofs with $C_t=1.1$

Rail Properties for 6063 Alloy Rail



Mean Roof Height

30

to 60

ft

Rail Properties for Downward Loads

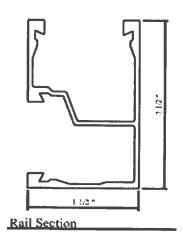
Section Properties

Α	=	0.63	in^2
S	=	0.34	in^3
I	$^{\circ}$	0.46	in^4

Stresses

$\mathbf{F_b}$	=	15.2	ksi
$\mathbf{F}_{\mathbf{v}}$	=	15.2	ksi
E	=	10000	ksi

$$M_{allow}$$
 = 5.17 k-in
 V_{allow} = 6.38 k



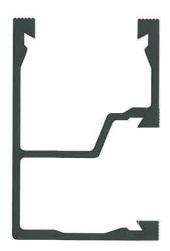
Rail Properties for Upward Loads

Section Properties

Α	=	0.41	in^2
S	=	0.25	in^3
I	=	0.11	in ⁴

Stresses

$$M_{allow}$$
 = 3.84 k-in
 V_{allow} = 4.16 k



SnapNrack Standard Rail 6063 Alloy

Notes

- 1) Rail section properties determined from test data.
- 2) Rail test date performed per guidelines of chapter 17 of the 2015 IBC.
- 3) This report is using 6063 Alloy Rail

PV panel Calculations & Component and Cladding Forces for 6063 Alloy Rail



Mean Roof Height

30

60

ft

PV Panel Calculations for 39" x 65" Panel Connections

D 1	ъ.	
Panel	Dim	ensions

65" Long Panels

Panel Width	=	39.0 in
Panel Length	=.	65.0 in
Panel Weight	=.	70.4 #
Panel Area	=	17.6 ft^2



ASCE 7-10 Component and Cladding

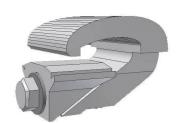
Wind Speed 110 to 190 mph

Exposure Cat. C

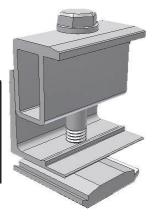
4 Ft Edge Distance (a)

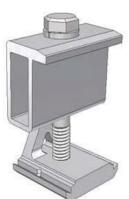
Component and Cladding				
Loading Zone 1 Zone 2 Zone 3 Zones 1, 2, & 3				
Max	-26.48	-35.41	-35.41	79.00
Min	-87.88	-148.24	-228.13	14.58

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) $Edge\ distance\ a=0.1*LDH\ (Least\ Horizontal\ Dimension)$



Universal End Clamp



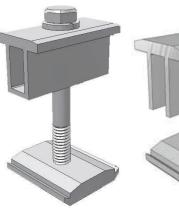


Adjustable End Clamp

X-Clamp

Maximum Force at Mounting Bracket				
Component and Cladding				
Loading Zone 1 Zone 2 Zone 3 Zones 1, 2, & 3				
End Clamp	-387	-652	-1004	348
Int. Clamp	-774	-1305	N/A	695

- 1) 4 brackets minimum per PV panel to rail connection
- 2) Only one corner of one PV panel may be located in zone 3
- 3) Zone 2 may have multiple panels located in this zone





Mid Clamp 1

Mid Clamp 2

PV panel Calculations & Component and Cladding Forces for 6063 Alloy Rail



Mean Roof Height 30

60

PV Panel Calculations for 39" x 78" Panel Connections

Panel Dimensions

78" Long Panels

Panel Width	=	39.0 in
Panel Length	=	78.0 in
Panel Weight	=	84.5 #
Panel Area	=	21.1 ft^2

Wind Loading

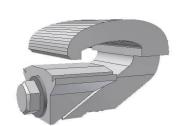
ASCE 7-10 Component and Cladding

Wind Speed 110 to 190 mph Exposure Cat. C

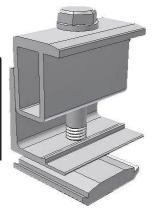
4 Ft Edge Distance (a)

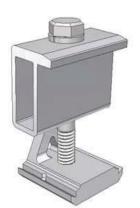
	Component and Cladding											
Loading	Zone 1	Zone 2	Zone 3	Zones 1, 2, & 3								
Max	-26.48	-35.41	-35.41	79.00								
Min	-87.88	-148.24	-228.13	14.58								

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) $Edge\ distance\ a=0.1*LDH\ (Least\ Horizontal\ Dimension)$



Universal End Clamp



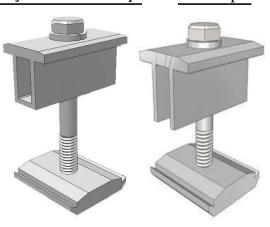


Adjustable End Clamp

X-Clamp

	Maximum Force at Mounting Bracket										
Component and Cladding											
Loading Zone 1 Zone 2 Zone 3 Zones 1, 2, & 3											
End Clamps	-464	-783	-1205	417							
Int. Clamp -928 -1566 N/A 834											
DT 1											

- 1) 4 brackets minimum per PV panel to rail connection
- 2) Only one corner of one PV panel may be located in zone 3
- 3) Zone 2 may have multiple panels located in this zone



Mid Clamp 1

Mid Clamp 2

Lag Bolt Design 2012 NDS for 6063 Alloy Rail



Mean Roof Height

Lag Bolt Calculations for Roof Connection 65" long Panel

Bolt Connection to Roof Structure

2012 National Design Specifications 5/16" Diameter Lag Bolt 2 1/2" min. embedment into framing member

Allowable Tension 258 #/in Embedment length 1.81 in Duration of Load 1.6 wind Allowable Tension 747.2 # Allowable Uplift 339.6 #

	65" Long Panels										
Maximum Wind Uplift (psf) per Span Based On Lag Bolt											
Span	Span Zone 2 Zone 3 Zone 2E										
2 ft	62.7	62.7	62.7	125.4							
4 ft	31.3	31.3	31.3	62.7							
6 ft	20.9	20.9	20.9	41.8							
8 ft	15.7	15.7	15.7	31.3							

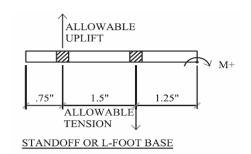
Lag Bolt Calculations for Roof Connection 78" long Panel

Bolt Connection to Roof Structure

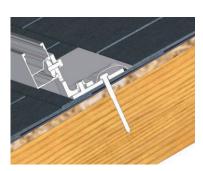
2012 National Design Specifications 5/16" Diameter Lag Bolt 2 1/2" min. embedment into framing member

Allowable Tension 258 #/in Embedment length 1.81 in Duration of Load 1.6 wind Allowable Tension 747.2 # Allowable Uplift 339.6 #

	78" Long Panels											
Maximum Wind Uplift (psf) per Span Based On Lag Bolt												
Span	n Zone 2 Zone 3 Zone 2E Zone 3E											
2 ft	52.2	52.2	52.2	104.5								
4 ft	26.1	26.1	26.1	52.2								
6 ft	17.4	17.4	17.4	34.8								
8 ft	13.1	13.1	13.1	26.1								







Notes

1) Only one corner of one PV panel may be located in zone *3E*

Rail Spans per ASCE 7-10 Loads Tilt Angle 0 to 19 degrees for 6063 Alloy Rail



Mean Roof Height

30

60

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angle 0 to 19 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	lh	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_{g}	$P_{\rm s}$	-12.3	-13.5	-14.7	-15.9	-17.2	-18.6	-20.0	-21.4	-22.9	-24.5	-26.1	-29.4	-33.0	-36.7
	0	0	106	101	96	91	87	83	80	77	74	71	69	64	61	57
	10	8	106	101	96	91	87	83	80	77	74	71	69	64	61	57
(pst)	20	15	89	89	89	89	87	83	80	77	74	71	69	64	61	57
) ad	30	23	75	75	75	75	75	75	75	75	74	71	69	64	61	57
Snow Load	40	31	66	66	66	66	66	66	66	66	66	66	66	64	61	57
Sno	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	57
	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

Rail Spans per ASCE 7-10 Loads Tilt Angle 19 to 37 degrees for 6063 Alloy Rail



Mean Roof Height 30

30

60

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angle 20 to 36 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	lh	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_{g}	$P_{\rm s}$	-8.0	-8.8	-9.6	-10.4	-11.2	-12.1	-13.0	-14.0	-14.9	-16.0	-17.0	-19.2	-21.5	-24.0
	0	0	120	120	120	119	113	108	103	99	95	91	88	82	77	72
	10	8	110	109	108	107	106	104	103	99	95	91	88	82	77	72
(pst)	20	15	89	89	89	89	89	88	87	86	86	85	84	82	77	72
) ad (30	23	75	75	75	75	75	75	75	75	75	75	75	74	73	72
Snow Load	40	31	66	66	66	66	66	66	66	66	66	66	66	66	66	66
Sno	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	60
	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

Rail Spans per ASCE 7-10 Loads Tilt Angle 37 to 45 degrees for 6063 Alloy Rail



Mean Roof Height

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angle 37 to 45 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	lh	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_{g}	$P_{\rm s}$	-7.7	-8.4	-9.1	-9.9	-10.7	-11.6	-12.4	-13.3	-14.3	-15.2	-16.2	-18.3	-20.6	-22.9
	0	0	120	120	120	120	116	111	106	101	97	93	90	84	79	74
_	10	8	110	109	108	107	106	104	103	101	97	93	90	84	79	74
Snow Load (psf)	20	15	89	89	89	89	89	88	87	86	86	85	84	83	79	74
) ad	30	23	75	75	75	75	75	75	75	75	75	75	75	74	73	72
w L(40	31	66	66	66	66	66	66	66	66	66	66	66	66	66	66
Sno	50	39	60	60	60	60	60	60	60	60	60	60	60	60	60	60
	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	55
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

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Rail Spans per ASCE 7-10 Loads Tilt Angle 45 to 60 degrees for 6063 Alloy Rail



Mean Roof Height

30

60

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angles 46 to 60 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	lh	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_{g}	$P_{\rm s}$	-7.3	-8.0	-8.7	-9.5	-10.2	-11.0	-11.9	-12.7	-13.6	-14.5	-15.5	-17.5	-19.6	-21.8
	0	0	120	120	119	116	113	110	107	104	100	96	93	86	81	76
	10	8	104	103	101	100	98	97	96	94	93	91	90	86	81	76
(bst)	20	15	88	87	86	85	84	83	82	81	81	80	79	77	75	73
oad (30	23	75	75	75	75	75	74	73	73	72	72	71	70	68	67
Snow Load	40	31	66	66	66	66	66	66	66	66	66	65	65	64	63	62
Sno	50	39	60	60	60	60	60	60	60	60	60	60	60	60	59	58
	60	46	55	55	55	55	55	55	55	55	55	55	55	55	55	54
	70	54	51	51	51	51	51	51	51	51	51	51	51	51	51	51
	80	62	48	48	48	48	48	48	48	48	48	48	48	48	48	48
	100	77	43	43	43	43	43	43	43	43	43	43	43	43	43	43
	120	92	40	40	40	40	40	40	40	40	40	40	40	40	40	40

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

Wind Design ASCE 7-10 Main Force Resisting System 6005 Alloy Rail



Mean Roof Height

ft

Risk Category: II (Table 1.5-2)

Wind Exposure Category

 \mathbf{C}

 $q_z = q_h = 0.00256 k_z k_{zt} k_d V^2$

Velocity Pressure 28.3.2 ASCE 7-10

Velocity Pressure Exposure Coefficients (Table 26.8-1) 0.98

1.00 Topographic Factor (Fig. 26.8-1)

Wind Directionality Factor (Table 26.6-1) 0.85

Velocity Pressures														
Wind Speed	110	115	120	125	130	135	140	145	150	155	160	170	180	190
q_{h}	25.80	28.20	30.71	33.32	36.04	38.86	41.80	44.84	47.98	51.23	54.59	61.63	69.09	76.98
ASD (0.6W)	15.48	16.92	18.42	19.99	21.62	23.32	25.08	26.90	28.79	30.74	32.75	36.98	41.46	46.19

$$P = q_h [GC_{pf} - GC_{pi}]$$

Velocity Pressure (psf)

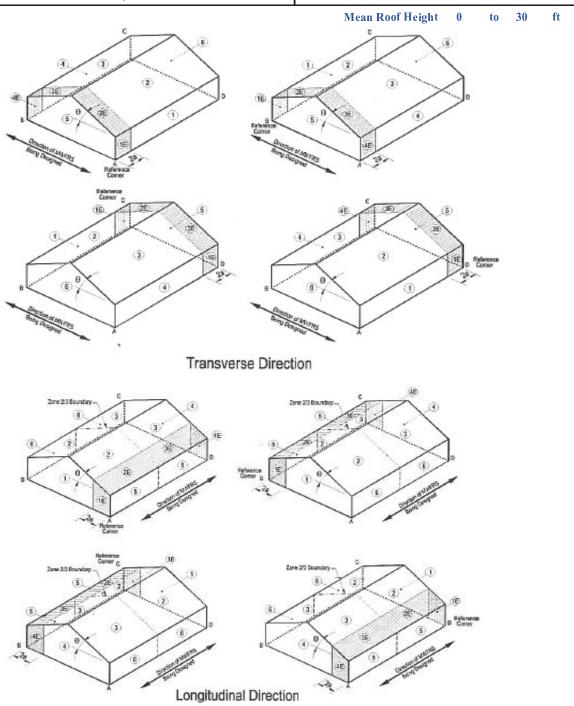
+/- Internal Pressure Coefficient GC_{pi} GC_{pf} External Pressure Coefficient

	GC_{pf}	Roof Zones	Fig 28.4-1 A	SCE 7-10	
Pitch	Slope	Zone 2	Zone 3	Zone 2E	Zone 3E
0/12	0.0	-0.69	-0.37	-1.07	-0.53
1/12	4.8	-0.69	-0.37	-1.07	-0.53
2/12	9.5	-0.69	-0.40	-1.07	-0.53
3/12	14.0	-0.69	-0.44	-1.07	-0.53
4/12	18.4	-0.69	-0.47	-1.07	-0.54
5/12	22.6	-0.45	-0.35	-0.72	-0.65
6/12	26.6	-0.10	-0.15	-0.19	-0.58
7/12	30.3	0.21	-0.43	0.27	-0.53
8/12	33.7	0.21	-0.43	0.27	-0.53
9/12	36.9	0.21	-0.43	0.27	-0.53
10/12	39.8	0.21	-0.43	0.27	-0.53
11/12	42.5	0.21	-0.43	0.27	-0.53
12/12	45.0	0.21	-0.43	0.27	-0.53
21/12	60.0	0.32	-0.41	0.40	-0.51

- 1) GCpi equal + 0.10 based on published data from the Solar America Board for Codes and Standards.
- 2) Wind Exposure B and C covered in this document.

Wind Design ASCE 7-10 Main Force Resisting System 6005 Alloy Rail





Zone Locations Main Force Resisting Systems ASCE 7-10

6005 Alloy Rail

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Wind Design ASCE 7-10 Components and Cladding Walls 6005 Alloy Rail



Mean Roof Height

0

30

ft

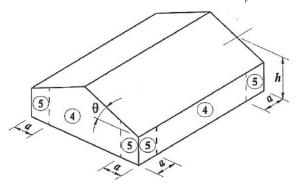
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

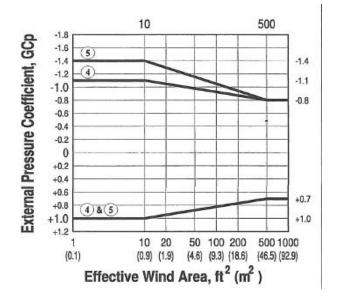
 q_h = Velocity Pressure (psf)

 $GC_{pi} = +/-$ Internal Pressure Coefficient

GC_p = External Pressure Coefficient



GC _p Walls (Fig. 30.4-1)										
Slope in Degrees Zone 4 Zone 5 Zone 4 & 5										
0 to 10	-1.00	-1.27	0.91							
10 to 45	-1.10	-1.39	-1.00							



Notes

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel

Wind Design ASCE 7-10 Components and Cladding Roof 0 to 7 degrees for 6005 Alloy Rail



Mean Roof Height

0 1

30

ft

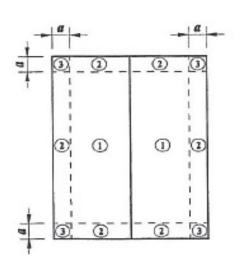
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

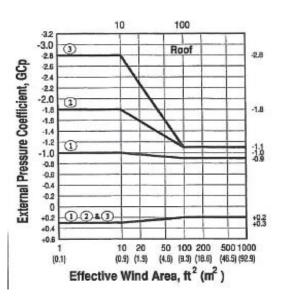
$$P = q_h [GC_p - GC_{pi}]$$

 q_h = Velocity Pressure (psf)

 GC_{pi} = +/- Internal Pressure Coefficient

GC_p = External Pressure Coefficient





GC _p Roofs Fig. 30.4-2A				
Slope in Degrees Zone 1 Zone 2 Zone 3 Zone 1,2,3				
0 to 7	-0.99	-1.71	-2.59	0.29

Notes

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel

Wind Design ASCE 7-10 Components and Cladding Roof 7 to 27 degrees for 6005 Alloy Rail



Mean Roof Height

0

30

ft

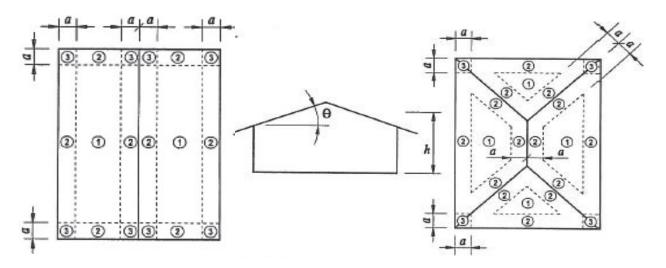
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

 q_h = Velocity Pressure (psf)

 $GC_{pi} = +/-$ Internal Pressure Coefficient

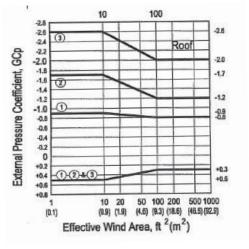
 GC_p = External Pressure Coefficient



GC _p Roofs Fig. 30.4-2B				
Slope in Degrees Zone 1 Zone 2 Zone 3 Zone 1,2,3				Zone 1,2,3
7 to 27	-0.89	-1.64	-2.53	0.48

Notes

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel



Wind Design ASCE 7-10 Components and Cladding Roof 27 to 45 degrees for 6005 Alloy Rail



Mean Roof Height

0

30

ft

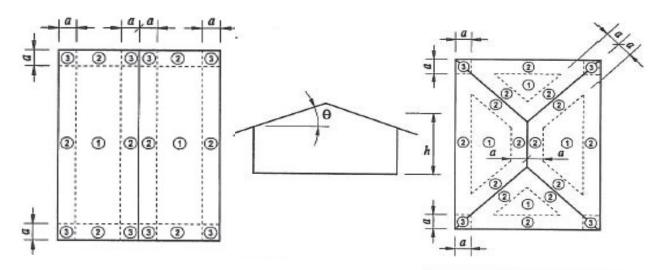
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

 q_h = Velocity Pressure (psf)

 $GC_{pi} = +/-$ Internal Pressure Coefficient

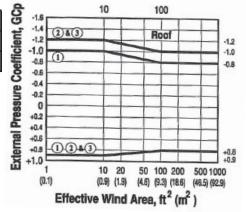
 GC_p = External Pressure Coefficient



GC _p Roofs Fig. 30.4-2C				
Slope in Degrees	Zone 1	Zone 2	Zone 3	Zone 1,2,3
27 to 45	-0.98	-1.18	-1.18	0.89

Notes

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel



Seismic Design ASCE 7-10 Chapter 11 and 13 6005 Alloy Rail



Mean Roof Height

30

ASCE 7-10 Seismic Design Section 13.6.9

Site Classificat	ion	D	Default "D"	
Seismic Use G	roup	II	Table 11.5-1	
R_p	=	2.5	Input from Table 13.6-1	ASCE 7-10
A_p	=	1.0	Input from Table 13.6-1	ASCE 7-10
I_p	=	1.0	Input from Table 11.5-1	ASCE 7-10
S_s	=	3.0	Input from USGS Progra	am
S_1	=	1.5	Input from USGS Progra	am
F_a	=	1.0	Site Coefficient Table 1	1.4-1
F_{v}	=	1.5	Site Coefficient Table 1	1.4-2
S_{ms}	=	3.0	ASCE 7-10 Section 11.4	4.3
S_{m1}	=	2.3	ASCE 7-10 Section 11.4	4.3
S_{ds}	=	2.0	ASCE 7-10 Section 11.4	4.3
S_{d1}	=	1.5	ASCE 7-10 Section 11.4	4.3
Z	=	30.5	Height at point of Attach	hment (ft.)
h	=	30.0	Average Roof Height of	f Structure (ft.)
F_{p}	=	0.97	Wp	(Eq. 13.3.1)
F _{p max}	=	3.20		
$F_{p \text{ min}}$	=	0.60		$F_{p} = \frac{0.4 a_{p} S_{DS} W_{p}}{(\frac{R_{p}}{I_{p}})} (1+2\frac{Z}{h})$
				I_p
Use F _p	=	0.97	Wp	(Eq. 13.3.2) $F_p = 1.6 S_{DS} I_p W_p Max$
				(Eq. 13.3.3) $F_p = 0.3 S_{DS} I_p W_p$ Min

Vertical Accelerations

$$0.20$$
 (S_{ds}) W_p

1) Based on an average deal load of 4 psf the anticipated maximum seismic load is approximately 4 psf with a vertical accelerations of 1.6 psf wind loads govern the design of the PV system.

Snow Loads ASCE 7-10 Chapter 7 6005 Alloy Rail



Mean Roof Height 0

0

30

ft

ASCE 7-10 Snow Loads Chapter 7

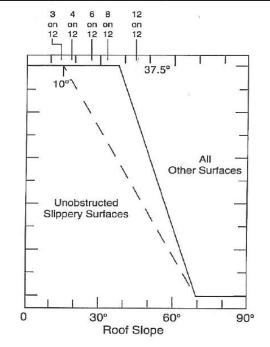
D –	0.7	C	C	T	D
$P_f =$	U. /	∪ e	\mathbf{v}_{t}	1	\mathbf{r}_{g}

$$P_s = C_s P_f$$

Snow Load Chart					
Ground Snow Pg	Flat Roof P _f	Sloped Roof P _s	Sloped Roof P _s		
Ground Show 1 g	Tiat Roof I f	Slope < 9/12	Slope 9/12 to 12/12		
10 psf	8	8	8		
20 psf	15	15	15		
30 psf	23	23	23		
40 psf	31	31	31		
50 psf	39	39	39		
60 psf	46	46	46		
70 psf	54	54	54		
80 psf	62	62	62		
100 psf	77	77	77		
120 psf	92	92	92		

Calculations for Snow Loads Chapter 7

C_e	=	1.00	Exposure Factor (Section 7.3.1)
C_t	=	1.10	Thermal Factor (Section 7.3.2)
T	=	1.00	Importance Factor (Section 7.3.3)



7-2b: Cold roofs with $C_t=1.1$

Rail Properties for 6005 Alloy Rail



Mean Roof Height

n

to 30

ft

Rail Properties for Downward Loads

Section Properties

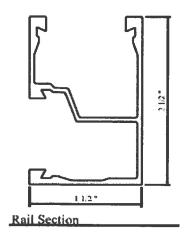
A	=	0.63	
S	=	0.34	in ³
I	=	0.46	in ⁴

Stresses

F_b	=	21.9	ksi
$\mathbf{F}_{\mathbf{v}}$	=	21.9	ksi
E	=	10000	ksi
M_{allow}	=	7.45	k-in

6.38

k



Rail Properties for Upward Loads Section Properties

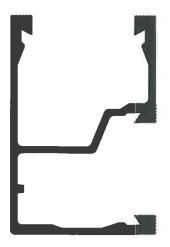
 $V_{\rm allow}$

Α	=	0.41	
S	=	0.25	in^3
I	=	0.11	in ⁴

Stresses

F_b	=	21.9	ksi
$\mathbf{F_v}$	=	21.9	ksi
E	=	10000	ksi

M_{allow}	=	5.53	k-in
V_{allow}	=	4.16	k



SnapNrack Standard Rail Keyed 6005 Alloy

Notes

- 1) Rail section properties determined from test data.
- 2) Rail test date performed per guidelines of chapter 17 of the 2015 IBC.
- 3) This report is using 6005 alloy rails

PV panel Calculations & Component and Cladding Forces for 6005 Alloy Rail



Mean Roof Height

0

30

ft

PV Panel Calculations for 39" x 65" Panel Connections

D 1	ъ.	
Panel	Dime	ensions

65" Long Panels

Panel Width	=	39.0 in
Panel Length	=	65.0 in
Panel Weight	=	70.4 #
Panel Area	=	17.6 ft^2



ASCE 7-10 Component and Cladding

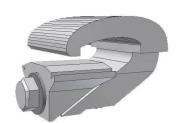
Wind Speed 110 to 190 mph

Exposure Cat. C

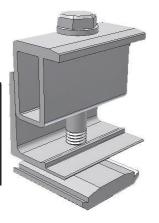
Edge Distance (a) 4 Ft

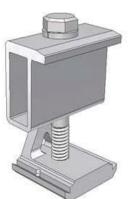
Component and Cladding											
Loading	Zone 1	Zone 2	Zone 3	Zones 1, 2, & 3							
Max	-22.96	-30.71	-30.71	68.51							
Min	-76.21	-128.56	-197.85	12.64							

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) $Edge\ distance\ a=0.1*LDH\ (Least\ Horizontal\ Dimension)$



Universal End Clamp



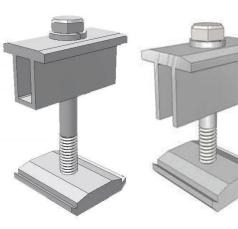


Adjustable End Clamp

X-Clamp

	Maximum	Force at Mount	ing Bracket								
	Component and Cladding										
Loading	Zone 1	Zone 2	Zone 3	Zones 1, 2, & 3							
End Clamp	-335	-566	-871	302							
Int. Clamp	-671	-1132	N/A	603							

- 1) 4 brackets minimum per PV panel to rail connection
- 2) Only one corner of one PV panel may be located in zone 3
- 3) Zone 2 may have multiple panels located in this zone



Mid Clamp 1

Mid Clamp 2

PV panel Calculations & Component and Cladding Forces for 6005 Alloy Rail



Mean Roof Height

0

o 30

ft

PV Panel Calculations for 39" x 78" Panel Connections

Panel Dimensions

78" Long Panels

Panel Width	=	39.0 in
Panel Length	=	78.0 in
Panel Weight	=	84.5 #
Panel Area	=	21.1 ft^2

Wind Loading

ASCE 7-10 Component and Cladding

Wind Speed 110 to 190 mph Exposure Cat. C

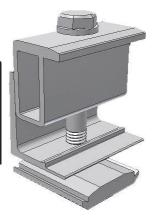
Edge Distance (a) 4 Ft

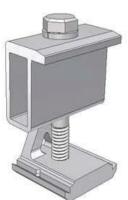
Component and Cladding											
Loading	Zone 1	Zone 2	Zone 3	Zones 1, 2, & 3							
Max	-22.96	-30.71	-30.71	68.51							
Min	-76.21	-128.56	-197.85	12.64							

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) $Edge\ distance\ a=0.1*LDH\ (Least\ Horizontal\ Dimension)$



Universal End Clamp



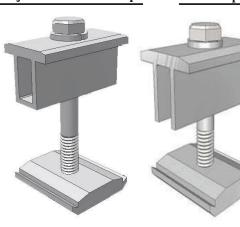


Adjustable End Clamp

X-Clamp

	Maximum Force at Mounting Bracket											
Component and Cladding												
Loading	Zone 1	Zone 2	Zone 3	Zones 1, 2, & 3								
End Clamps	-402	-679	-1045	362								
Int. Clamp	-805	-1358	N/A	724								

- 1) 4 brackets minimum per PV panel to rail connection
- 2) Only one corner of one PV panel may be located in zone 3
- 3) Zone 2 may have multiple panels located in this zone



Mid Clamp 1

Mid Clamp 2

Lag Bolt Design 2012 NDS for 6005 Alloy Rail



Mean Roof Height

30

ft

Lag Bolt Calculations for Roof Connection 65" long Panel

Bolt Connection to Roof Structure

2012 National Design Specifications 5/16" Diameter Lag Bolt 2 1/2" min. embedment into framing member

Allowable Tension 258 #/in Embedment length 1.81 in Duration of Load 1.6 wind Allowable Tension 747.2 # Allowable Uplift 339.6 #

	65" Long Panels												
Maximum Wind Uplift (psf) per Span Based On Lag Bolt													
Span	Zone 2	Zone 3	Zone 2E	Zone 3E									
2 ft	62.7	62.7	62.7	125.4									
4 ft	31.3	31.3	31.3	62.7									
6 ft	20.9	20.9	20.9	41.8									
8 ft	15.7	15.7	15.7	31.3									

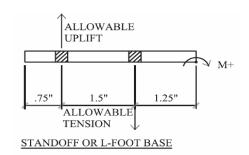
Lag Bolt Calculations for Roof Connection 78" long Panel

Bolt Connection to Roof Structure

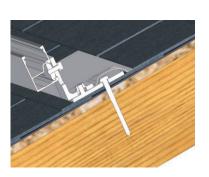
2012 National Design Specifications 5/16" Diameter Lag Bolt 2 1/2" min. embedment into framing member

Allowable Tension 258 #/in Embedment length 1.81 in Duration of Load 1.6 wind Allowable Tension 747.2 # Allowable Uplift 339.6 #

	78" Long Panels											
Maximum Wind Uplift (psf) per Span Based On Lag Bolt												
Span	Zone 2	Zone 3	Zone 2E	Zone 3E								
2 ft	52.2	52.2	52.2	104.5								
4 ft	26.1	26.1	26.1	52.2								
6 ft	17.4	17.4	17.4	34.8								
8 ft	13.1	13.1	13.1	26.1								







Notes

1) Only one corner of one PV panel may be located in zone *3E*

Rail Spans per ASCE 7-10 Loads Tilt Angle 0 to 19 degrees for 6005 Alloy Rail



Mean Roof Height

t

30

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

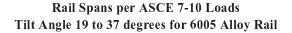
	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angle 0 to 19 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	l h	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_{g}	$P_{\rm s}$	-10.7	-11.7	-12.7	-13.8	-14.9	-16.1	-17.3	-18.6	-19.9	-21.2	-22.6	-25.5	-28.6	-31.9
	0	0	140	132	125	119	114	109	104	100	96	93	89	84	79	74
	10	8	137	132	125	119	114	109	104	100	96	93	89	84	79	74
(pst)	20	15	106	106	106	106	106	106	104	100	96	93	89	84	79	74
) pac	30	23	90	90	90	90	90	90	90	90	90	90	89	84	79	74
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	79	79	79	74
Sno	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	72
	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

6005 Alloy Rail





Mean Roof Height

to

30

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

		Load (Combin	ations 3	3, 5, 6,	7 and L	ag Bol	t Tensio	n Valu	es	Tilt Aı	ngle 20	to 36 D	egrees		
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	q_h		15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_{g}	$P_{\rm s}$	-7.0	-7.6	-8.3	-9.0	-9.7	-10.5	-11.3	-12.1	-13.0	-13.8	-14.7	-16.6	-18.7	-20.8
	0	0	144	144	144	144	144	141	135	129	124	119	114	107	100	94
	10	8	134	133	132	130	129	128	127	125	124	119	114	107	100	94
(pst)	20	15	106	106	106	106	106	106	106	105	105	104	103	101	100	94
oad (30	23	90	90	90	90	90	90	90	90	90	90	90	90	89	88
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	79	79	79	79
Sno	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	72
	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

6005 Alloy Rail

Rail Spans per ASCE 7-10 Loads Tilt Angle 37 to 45 degrees for 6005 Alloy Rail



Mean Roof Height

to

30

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

		Load (Combin	ations 3	3, 5, 6,	7 and L	ag Bol	t Tensio	on Valu	es	Tilt Aı	ngle 37	to 45 D	egrees		
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	q_h		15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_{g}	$P_{\rm s}$	-6.7	-7.3	-7.9	-8.6	-9.3	-10.0	-10.8	-11.6	-12.4	-13.2	-14.1	-15.9	-17.8	-19.9
	0	0	144	144	144	144	144	144	139	133	127	122	118	109	102	96
	10	8	134	133	132	130	129	128	127	125	124	122	118	109	102	96
(pst)	20	15	106	106	106	106	106	106	106	105	105	104	103	101	100	96
oad (30	23	90	90	90	90	90	90	90	90	90	90	90	90	89	88
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	79	79	79	79
Sno	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	72
	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

6005 Alloy Rail

Rail Spans per ASCE 7-10 Loads Tilt Angle 45 to 60 degrees for 6005 Alloy Rail



Mean Roof Height

30

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angles 46 to 60 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	l h	15.5	16.9	18.4	20.0	21.6	23.3	25.1	26.9	28.8	30.7	32.8	37.0	41.5	46.2
	P_{g}	$P_{\rm s}$	-6.3	-6.9	-7.6	-8.2	-8.9	-9.6	-10.3	-11.0	-11.8	-12.6	-13.4	-15.2	-17.0	-18.9
	0	0	144	144	144	144	142	139	135	132	129	126	121	113	105	99
	10	8	128	126	124	123	121	120	118	116	115	113	112	109	105	99
(pst)	20	15	106	106	105	104	103	102	101	100	99	98	97	95	93	91
oad (30	23	90	90	90	90	90	90	90	89	88	88	87	85	84	82
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	79	78	77	76
Sno	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	71
	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

Wind Design ASCE 7-10 Main Force Resisting System 6005 Alloy Rail



Mean Roof Height 30

30

to 60

ft

Velocity Pressure 28.3.2 ASCE 7-10

 $q_z = q_h = 0.00256 k_z k_{zt} k_d V^2$

Risk Category: II (Table 1.5-2)

Wind Exposure Category

 \mathbf{C}

 $k_z = 1.13$ Velocity Pressure Exposure Coefficients (Table 26.8-1)

 $K_{zt} = 1.00$ Topographic Factor (Fig. 26.8-1)

 $K_d = 0.85$ Wind Directionality Factor (Table 26.6-1)

Velocity Pressures														
Wind Speed	110	115	120	125	130	135	140	145	150	155	160	170	180	190
q_{h}	29.75	32.52	35.41	38.42	41.56	44.81	48.19	51.70	55.32	59.07	62.95	71.06	79.67	88.77
ASD (0.6W)	17.85	19.51	21.24	23.05	24.93	26.89	28.92	31.02	33.19	35.44	37.77	42.64	47.80	53.26

$$P = q_h [GC_{pf} - GC_{pi}]$$

 q_h = Velocity Pressure (psf)

 GC_{pi} = +/- Internal Pressure Coefficient GC_{pf} = External Pressure Coefficient

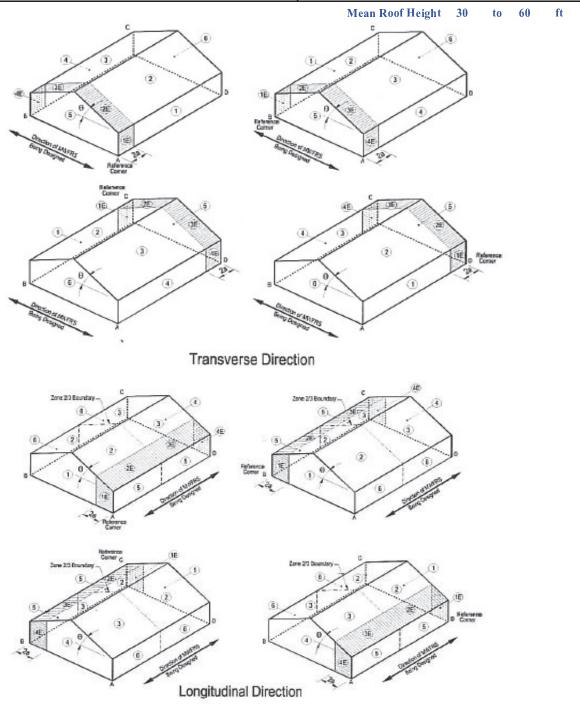
	GC _{pf} Roof Zones Fig 28.4-1 ASCE 7-10								
Pitch	Slope	Zone 2	Zone 3	Zone 2E	Zone 3E				
0/12	0.0	-0.69	-0.37	-1.07	-0.53				
1/12	4.8	-0.69	-0.37	-1.07	-0.53				
2/12	9.5	-0.69	-0.40	-1.07	-0.53				
3/12	14.0	-0.69	-0.44	-1.07	-0.53				
4/12	18.4	-0.69	-0.47	-1.07	-0.54				
5/12	22.6	-0.45	-0.35	-0.72	-0.65				
6/12	26.6	-0.10	-0.15	-0.19	-0.58				
7/12	30.3	0.21	-0.43	0.27	-0.53				
8/12	33.7	0.21	-0.43	0.27	-0.53				
9/12	36.9	0.21	-0.43	0.27	-0.53				
10/12	39.8	0.21	-0.43	0.27	-0.53				
11/12	42.5	0.21	-0.43	0.27	-0.53				
12/12	45.0	0.21	-0.43	0.27	-0.53				
21/12	60.0	0.32	-0.41	0.40	-0.51				

Notes

- 1) GCpi equal + 0.10 based on published data from the Solar America Board for Codes and Standards.
- 2) Wind Exposure B and C covered in this document.

Wind Design ASCE 7-10 Main Force Resisting System 6005 Alloy Rail





Zone Locations Main Force Resisting Systems ASCE 7-10

Wind Design ASCE 7-10 Components and Cladding Walls 6005 Alloy Rail



60

ft

Mean Roof Height 30 to

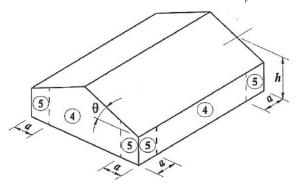
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

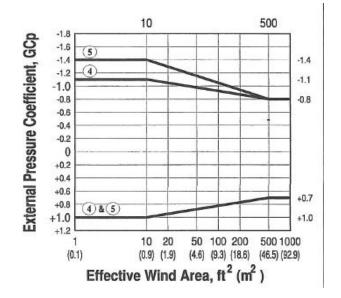
 q_h = Velocity Pressure (psf)

 $GC_{pi} = +/-$ Internal Pressure Coefficient

GC_p = External Pressure Coefficient



GC _p Walls (Fig. 30.4-1)								
Slope in Degrees	Zone 4	Zone 5	Zone 4 & 5					
0 to 10	-1.00	-1.27	0.91					
10 to 45	-1.10	-1.39	-1.00					



Notes

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel

Wind Design ASCE 7-10 Components and Cladding Roof 0 to 7 degrees for 6005 Alloy Rail



Mean Roof Height 30 to

to 60

ft

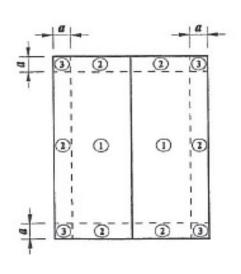
Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

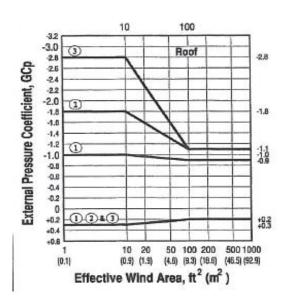
$$P = q_h [GC_p - GC_{pi}]$$

 q_h = Velocity Pressure (psf)

 GC_{pi} = +/- Internal Pressure Coefficient

GC_p = External Pressure Coefficient





GC _p Roofs Fig. 30.4-2A								
Slope in Degrees	Zone 1	Zone 2	Zone 3	Zone 1,2,3				
0 to 7	-0.99	-1.71	-2.59	0.29				

Notes

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel

Wind Design ASCE 7-10 Components and Cladding Roof 7 to 27 degrees for 6005 Alloy Rail



Mean Roof Height

60

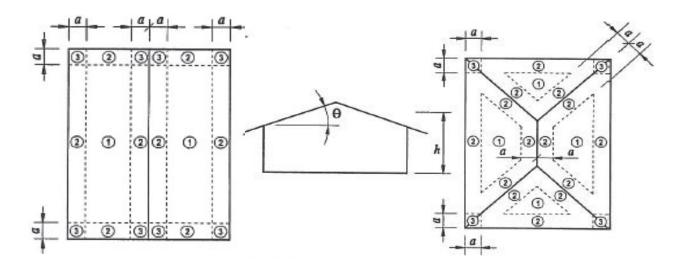
ft

Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

$$P = q_h [GC_p - GC_{pi}]$$

Velocity Pressure (psf)

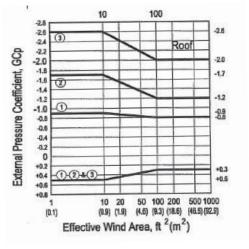
 $GC_{\mathfrak{p}\mathrm{i}}$ +/- Internal Pressure Coefficient $GC_{\mathfrak{p}}$ External Pressure Coefficient



GC _p Roofs Fig. 30.4-2B									
Slope in Degrees	Zone 1	Zone 2	Zone 3	Zone 1,2,3					
7 to 27	-0.89	-1.64	-2.53	0.48					

Notes

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel



Wind Design ASCE 7-10 Components and Cladding Roof 27 to 45 degrees for 6005 Alloy Rail

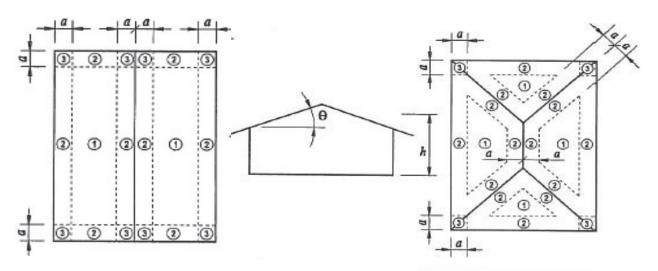


Mean Roof Height 30 to 60

ft

Components and Cladding Low-Rise Buildings ASCE 7-10 30.4-1

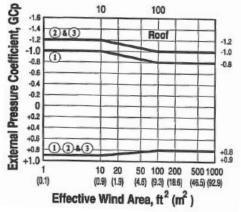
 GC_{pi} = +/- Internal Pressure Coefficient GC_{p} = External Pressure Coefficient



GC _p Roofs Fig. 30.4-2C									
Slope in Degrees	Zone 1	Zone 2	Zone 3	Zone 1,2,3					
27 to 45	-0.98	-1.18	-1.18	0.89					



- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 0.1 * LDH (Least Horizontal Dimension)
- 4) Based on an area equal to the maximum area of one 39" x 78" PV panel



Seismic Design ASCE 7-10 Chapter 11 and 13 6005 Alloy Rail



60

ft

Mean Roof Height 30 to

ASCE 7-10 Seismic Design Section 13.6.9

Site Classificat	ion	D	Default "D"			
Seismic Use G	roup	II	Table 11.5-1			
R_p	=	2.5	Input from Table 13.6-1 ASO	CE 7-10		
A_p	=	1.0	Input from Table 13.6-1 ASO	CE 7-10		
I_p	=	1.0	Input from Table 11.5-1 ASO	CE 7-10		
S_s	=	3.0	Input from USGS Program			
S_1	=	1.5	Input from USGS Program			
F_a	=	1.0	Site Coefficient Table 11.4-	I		
F_{v}	=	1.5	Site Coefficient Table 11.4-2	2		
S_{ms}	=	3.0	ASCE 7-10 Section 11.4.3			
S_{m1}	=	2.3	ASCE 7-10 Section 11.4.3			
S_{ds}	=	2.0	ASCE 7-10 Section 11.4.3			
S_{d1}	=	1.5	ASCE 7-10 Section 11.4.3			
Z	=	60.5	Height at point of Attachmen	nt (ft.)		
h	=	60.0	Average Roof Height of Stru	ecture (ft.)		
F_p	=	0.97	7 Wp	(Eq. 13.3.1)		
$F_{p \; max}$	=	3.20) Wp	$F_{n} = \frac{0.4 a_{p}}{}$	$S_{DS} W_p$ (1+2 \overline{z}	-)
$F_{p \; min}$	=	0.60) Wp	(-	$\frac{S_{DS} W_p}{R_p}$ (1+2 $\frac{z}{h}$,
					\mathbf{I}_{p}	
Use F _p	=	0.97	7 Wp	(Eq. 13.3.2)	$F_p = 1.6 S_{DS} I_p W_p$	Max
				(Eq. 13.3.3)	$F_p = 0.3 S_{DS} I_p W_p$	Min

Vertical Accelerations

$$0.20$$
 (S_{ds}) W_p

Notes

1) Based on an average deal load of 4 psf the anticipated maximum seismic load is approximately 4 psf with a vertical accelerations of 1.6 psf wind loads govern the design of the PV system.

Snow Loads ASCE 7-10 Chapter 7 6005 Alloy Rail



60

Mean Roof Height 30 to

ASCE 7-10 Snow Loads Chapter 7

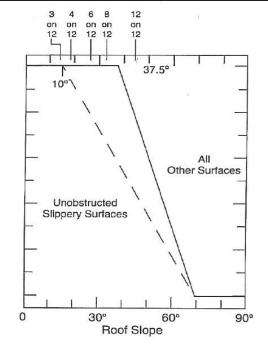
 $P_f = 0.7 C_e C_t I P_g$

 $P_s = C_s P_f$

Snow Load Chart				
Ground Snow Pg	Flat Roof P _f	Sloped Roof P _s	Sloped Roof P _s	
Ground Show 1 g	Tiat Root I f	Slope < 9/12	Slope 9/12 to 12/12	
10 psf	8	8	8	
20 psf	15	15	15	
30 psf	23	23	23	
40 psf	31	31	31	
50 psf	39	39	39	
60 psf	46	46	46	
70 psf	54	54	54	
80 psf	62	62	62	
100 psf	77	77	77	
120 psf	92	92	92	

Calculations for Snow Loads Chapter 7

C_e	=	1.00	Exposure Factor (Section 7.3.1)
C_t	=	1.10	Thermal Factor (Section 7.3.2)
I	=	1.00	Importance Factor (Section 7.3.3)



7-2b: Cold roofs with $C_t=1.1$

Rail Properties for 6005 Alloy Rail



Mean Roof Height

20

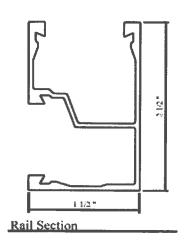
to 60

ft

Rail Properties for Downward Loads Section Properties

Α		0.63	
S	=	0.34	in^3
•		0.46	. 4

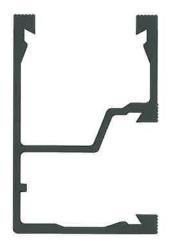
in⁴ 0.46 Ι Stresses 21.9 F_{b} ksi $F_{\mathbf{v}}$ 21.9 ksi E 10000 ksi M_{allow} 7.45 k-in V_{allow} 6.38 k



Rail Properties for Upward Loads Section Properties

Α

4.8		0.41	***
S	=	0.25	in ³
I	=	0.11	in^4
	Stresses		
F_b	=	21.9	ksi
$F_{\mathbf{v}}$	=	21.9	ksi
Е	=	10000	ksi
$\mathbf{M}_{\mathrm{allow}}$	=	5.53	k-in
V_{allow}	=	4.16	k



SnapNrack Standard Rail Keyed 6005 Alloy

Notes

- 1) Rail section properties determined from test data.
- 2) Rail test date performed per guidelines of chapter 17 of the 2015 IBC.
- 3) This report is using 6005 alloy rails

 in^2

0.41

of

PV panel Calculations & Component and Cladding Forces for 6005 Alloy Rail



Mean Roof Height

30

to

60

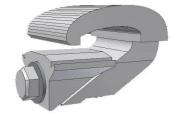
ft

PV Panel Calculations for 39" x 65" Panel Connections

D 1	ъ.	
Panel	Dime	ensions

65" Long Panels

Panel Width	=	39.0 in
Panel Length	=	65.0 in
Panel Weight	=	70.4 #
Panel Area	=	17.6 ft^2



Universal End Clamp

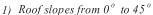
Wind Loading

ASCE 7-10 Component and Cladding

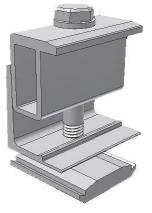
Wind Speed	110 to 190 mph
Exposure Cat.	C

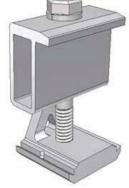
Edge Distance (a) 4 Ft

Component and Cladding				
Loading	Zone 1	Zone 2	Zone 3	Zones 1, 2, & 3
Max	-26.48	-35.41	-35.41	79.00
Min	-87.88	-148.24	-228.13	14.58



- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 4 ft based on a 40 ft least width or depth and a mean roof height less than 60 ft.



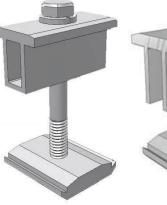


Adjustable End Clamp

X-Clamp

Maximum Force at Mounting Bracket				
	Component and Cladding			
Loading	Zone 1	Zone 2	Zone 3	Zones 1, 2, & 3
End Clamp	-387	-652	-1004	348
Int. Clamp	-774	-1305	N/A	695

- 1) 4 brackets minimum per PV panel to rail connection
- 2) Only one corner of one PV panel may be located in zone 3
- 3) Zone 2 may have multiple panels located in this zone





Mid Clamp 1

Mid Clamp 2

PV panel Calculations & Component and Cladding Forces for 6005 Alloy Rail



Mean Roof Height

30

to

60

ft

PV Panel Calculations for 39" x 78" Panel Connections

Panel Dimensions

78" Long Panels

Panel Width	=	39.0 in
Panel Length	=	78.0 in
Panel Weight	=	84.5 #
Panel Area	=	21.1 ft^2

Wind Loading

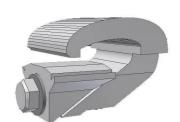
ASCE 7-10 Component and Cladding

Wind Speed 110 to 190 mph Exposure Cat. C

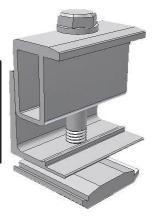
Edge Distance (a) 4 Ft

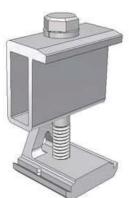
	Component and Cladding			
Loading	Zone 1	Zone 2	Zone 3	Zones 1, 2, & 3
Max	-26.48	-35.41	-35.41	79.00
Min	-87.88	-148.24	-228.13	14.58

- 1) Roof slopes from 0° to 45°
- 2) Wind loading from 110 mph to 190 mph 3-s Gust.
- 3) Edge distance a = 4 ft based on a 40 ft least width or depth and a mean roof height less than 60 ft.



Universal End Clamp



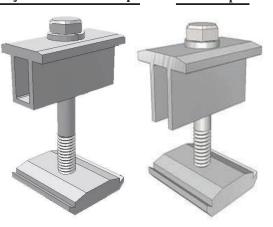


Adjustable End Clamp

X-Clamp

Maximum Force at Mounting Bracket				
	Component and Cladding			
Loading Zone 1 Zone 2 Zone 3 Zones 1, 2, & 3				
End Clamps	-464	-783	-1205	417
Int. Clamp	-928	-1566	N/A	834
			-	

- 1) 4 brackets minimum per PV panel to rail connection
- 2) Only one corner of one PV panel may be located in zone 3
- 3) Zone 2 may have multiple panels located in this zone



Mid Clamp 1

Mid Clamp 2

Lag Bolt Design 2012 NDS for 6005 Alloy Rail



Mean Roof Height 3

30

to

60

ft

Lag Bolt Calculations for Roof Connection 65" long Panel

Bolt Connection to Roof Structure

2012 National Design Specifications 5/16" Diameter Lag Bolt 2 1/2" min. embedment into framing member

Allowable Tension = 258 #/in

Embedment length = 1.81 in

Duration of Load = 1.6 wind

Allowable Tension = 747.2 #

Allowable Uplift = 339.6 #

	65" Long Panels							
Maxiı	Maximum Wind Uplift (psf) per Span Based On Lag Bolt							
Span	zan Zone 2 Zone 3 Zone 2E							
2 ft	62.7	62.7	62.7	125.4				
4 ft	31.3	31.3	31.3	62.7				
6 ft	20.9	20.9	20.9	41.8				
8 ft	15.7	15.7	15.7	31.3				

Lag Bolt Calculations for Roof Connection 78" long Panel

Bolt Connection to Roof Structure

2012 National Design Specifications 5/16" Diameter Lag Bolt 2 1/2" min. embedment into framing member

Allowable Tension = 258 #/in

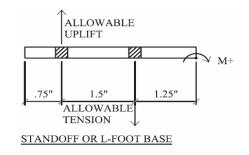
Embedment length = 1.81 in

Duration of Load = 1.6 wind

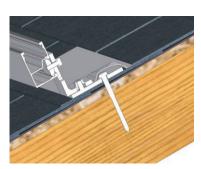
Allowable Tension = 747.2 #

Allowable Uplift = 339.6 #

	78" Long Panels								
Maximum Wind Uplift (psf) per Span Based On Lag Bolt									
Span	Zone 2	Zone 3E							
2 ft	52.2	52.2	52.2	104.5					
4 ft	26.1	26.1	26.1	52.2					
6 ft	17.4	17.4	17.4	34.8					
8 ft	13.1	13.1	13.1	26.1					







Notes

1) Only one corner of one PV panel may be located in zone 3E

Rail Spans per ASCE 7-10 Loads Tilt Angle 0 to 19 degrees for 6005 Alloy Rail



Mean Roof Height 3

30

0 60

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angle 0 to 19 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	l h	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_{g}	$P_{\rm s}$	-12.3	-13.5	-14.7	-15.9	-17.2	-18.6	-20.0	-21.4	-22.9	-24.5	-26.1	-29.4	-33.0	-36.7
	0	0	128	121	115	109	105	100	96	92	89	86	83	77	73	69
	10	8	128	121	115	109	105	100	96	92	89	86	83	77	73	69
(pst)	20	15	106	106	106	106	105	100	96	92	89	86	83	77	73	69
oad (30	23	90	90	90	90	90	90	90	90	89	86	83	77	73	69
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	79	77	73	69
Sno	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	69
	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

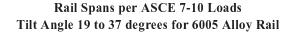
Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

6005 Alloy Rail

of





Mean Roof Height 3

30

60

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angle 20 to 36 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	l h	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_{g}	$P_{\rm s}$	-8.0	-8.8	-9.6	-10.4	-11.2	-12.1	-13.0	-14.0	-14.9	-16.0	-17.0	-19.2	-21.5	-24.0
	0	0	144	144	144	142	135	129	123	118	114	109	105	98	92	87
	10	8	132	131	129	128	127	125	123	118	114	109	105	98	92	87
(pst)	20	15	106	106	106	106	106	105	105	104	103	102	101	98	92	87
oad (30	23	90	90	90	90	90	90	90	90	90	90	90	89	87	86
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	79	79	79	79
Sno	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	72
	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

Notes

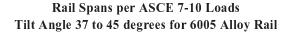
- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.

6005 Alloy Rail

Page

of





Mean Roof Height

30

60

ft

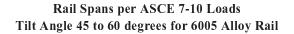
Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angle 37 to 45 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	lh	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_{g}	$P_{\rm s}$	-7.7	-8.4	-9.1	-9.9	-10.7	-11.6	-12.4	-13.3	-14.3	-15.2	-16.2	-18.3	-20.6	-22.9
	0	0	144	144	144	144	139	133	127	122	117	112	108	101	94	89
_	10	8	132	131	129	128	127	125	124	122	117	112	108	101	94	89
Snow Load (psf)	20	15	106	106	106	106	106	105	105	104	103	102	101	99	94	89
) ad	30	23	90	90	90	90	90	90	90	90	90	90	90	89	87	86
w L(40	31	79	79	79	79	79	79	79	79	79	79	79	79	79	79
Sno	50	39	72	72	72	72	72	72	72	72	72	72	72	72	72	72
	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	66
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.





Mean Roof Height

30

60

ft

Rail Spans (in) Based on Load Combinations for ASCE 7-10 Chapter 2

	Load Combinations 3, 5, 6, 7 and Lag Bolt Tension Values Tilt Angles 46 to 60 Degrees															
	Wind Load															
	V	u lt	110	115	120	125	130	135	140	145	150	155	160	170	180	190
	C	l h	17.9	19.5	21.2	23.1	24.9	26.9	28.9	31.0	33.2	35.4	37.8	42.6	47.8	53.3
	P_{g}	$P_{\rm s}$	-7.3	-8.0	-8.7	-9.5	-10.2	-11.0	-11.9	-12.7	-13.6	-14.5	-15.5	-17.5	-19.6	-21.8
	0	0	144	144	143	139	136	132	129	125	120	115	111	104	97	91
	10	8	125	123	122	120	118	116	115	113	111	110	108	104	97	91
(pst)	20	15	105	104	103	102	101	100	99	98	97	96	95	92	90	88
oad (30	23	90	90	90	90	90	89	88	87	87	86	85	83	82	80
Snow Load	40	31	79	79	79	79	79	79	79	79	79	79	78	77	76	74
Sno	50	39	72	72	72	72	72	72	72	72	72	72	72	71	70	69
	60	46	66	66	66	66	66	66	66	66	66	66	66	66	66	65
	70	54	62	62	62	62	62	62	62	62	62	62	62	62	62	62
	80	62	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	100	77	52	52	52	52	52	52	52	52	52	52	52	52	52	52
	120	92	48	48	48	48	48	48	48	48	48	48	48	48	48	48

Notes

- 1) Tables are based on critical rail span for load combinations as specified in chapter 2 of the ASCE 7-10 and lag bolt withdraw values per the 2012 NDS.
- 2) Basic Load Combinations from ASCE 7-10 Section 2.4 Allowable Stress Design.
 - 1. D
 - 2. D + L
 - 3. $D + (Lr \ or \ S \ or \ R)$
 - 4. D + 0.75L + 0.75(Lr or S or R)
 - 5. D + (0.6W or 0.75L)
 - 6a. D + 0.75L + 0.75(0.6W) + 0.75(Lr or S or R)
- 6b. D + 0.75L + 0.75(0.7E) + 0.75S

- 7. 0.6D + 0.6W
- 8. 0.6D + 0.7E
- 3) Edge zone reductions are only required at shaded spans where reduction is 24 inches to a minimum of 32 inches.



Structural Report and Calculations

Appendix A: ASCE-2010 to 2005 conversion sheet

The 100 Series report's results have been calculated according to the ASCE-2010 guidelines. If the results would rather be examined in terms of the ASCE-2005 codes, the following conversions must be applied for the two codes' results to be of equivalence.

This appendix also applies for converting to different years for IBC codes. For 2006 and 2009 IBC, use the ASCE-2005 codes, and for the 2012 and 2015 IBC, use the ASCE-2010 codes.

Factors specific to this report

- 1) The roof-mounted solar panels are in terms of Risk Category II
- 2) The importance factor for the ASCE-2005 code is I = 1.0
- 3) The ASCE-2010 code has no importance factor for the wind loads
- 4) The snow load's importance factor remains the same for both the 2005 and 2010 codes
- 5) Thus, calculations that utilize wind loads are the ONLY ones that need conversions

Velocity Equivalence (mph)

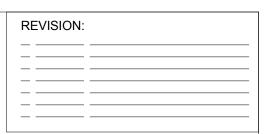
V _{3-sec} (ASCE7-05)	Vult. (ASCE7-10)
85	100
90	116
100	129
110	142
120	155
130	168
140	181
150	194

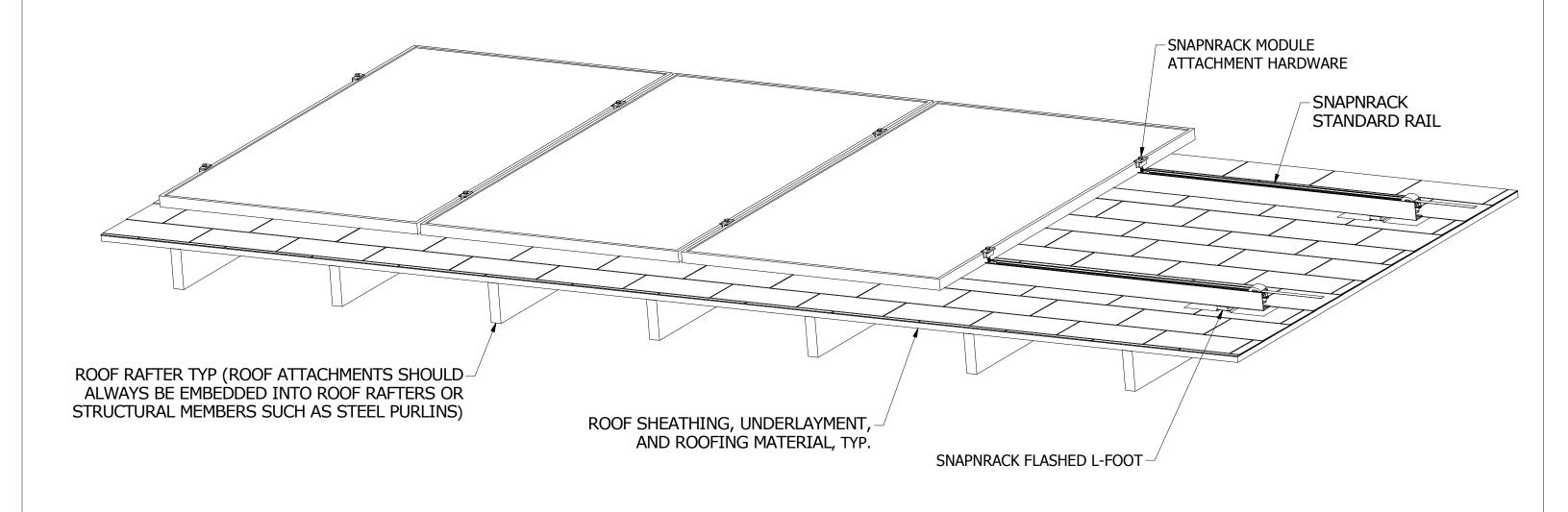
The following velocities listed in the graph refer to some V_{2005} being equal to some V_{2010} . In other words, use the following velocities in accordance with either ASCE-2005 or ASCE-2010.

SNAPNRACK SERIES 100 ON FLASHED L-FEET

FLASHED L-FEET ARE OPTIMIZED FOR QUICK AND ROBUST INSTALLATION ON STANDARD COMPOSITION SHINGLE ROOF SURFACES

FOR OTHER ROOF TYPES STANDOFFS ARE RECOMMENDED







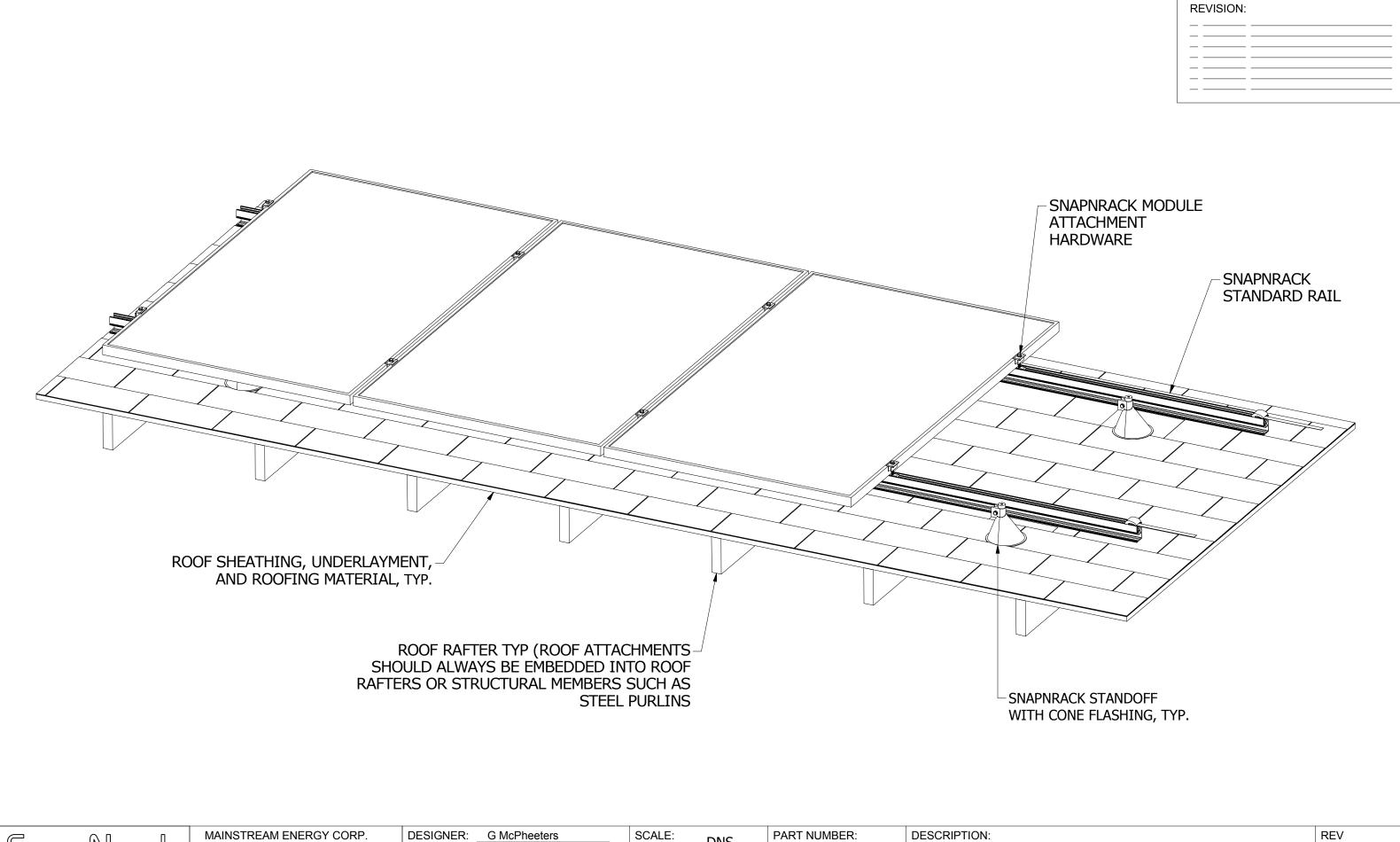
MAINSTREAM ENERGY CORP.

DESIGNER: G McPheeters D Ryan DRAFTER: APPROVED BY:

SCALE: DNS DATE: 120113 PART NUMBER: S100 D01 **DESCRIPTION:**

SERIES 100 OVERVIEW, ON FLASHED L-FEET

REV

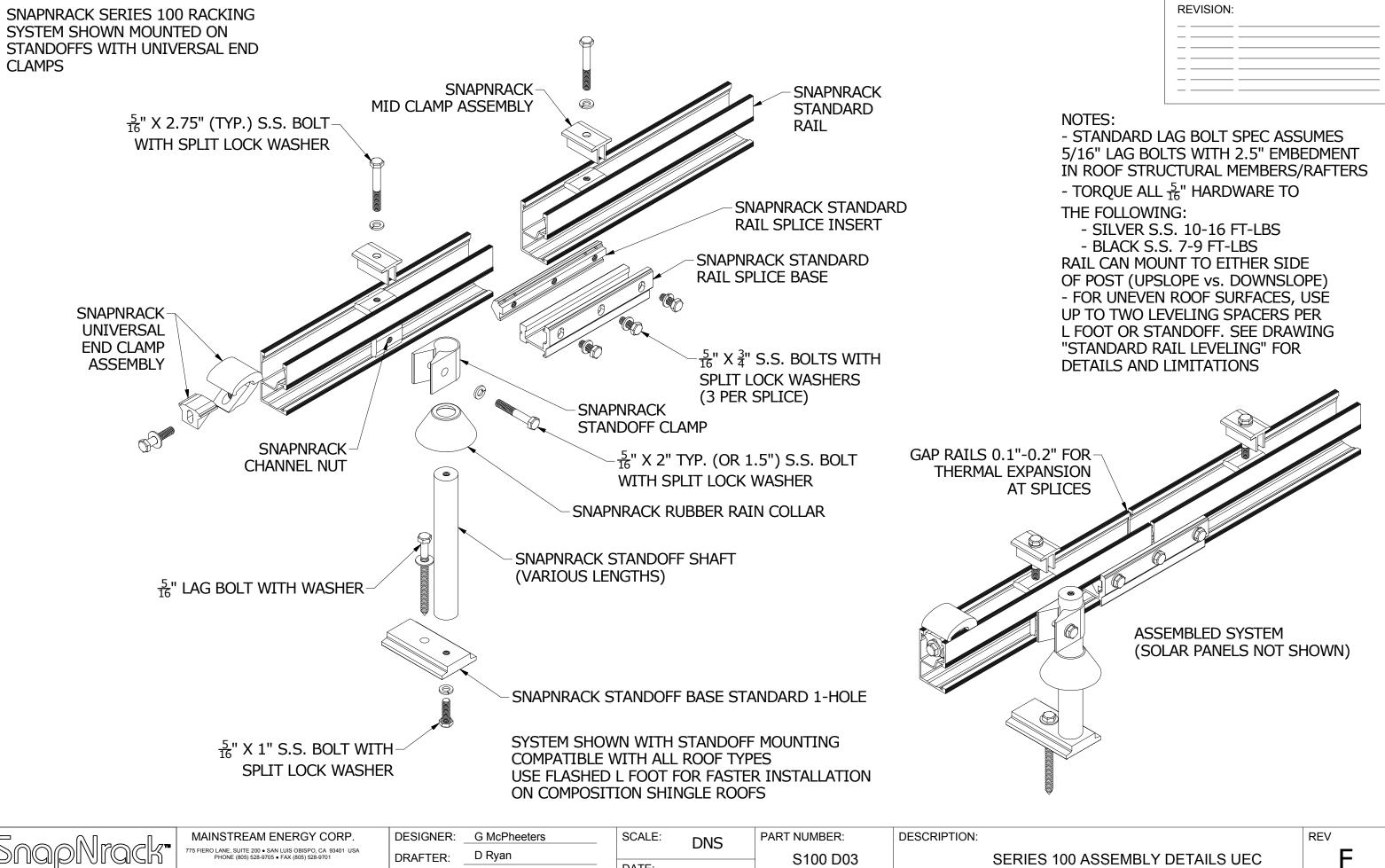


D Ryan DRAFTER: APPROVED BY:

DNS DATE: 120113

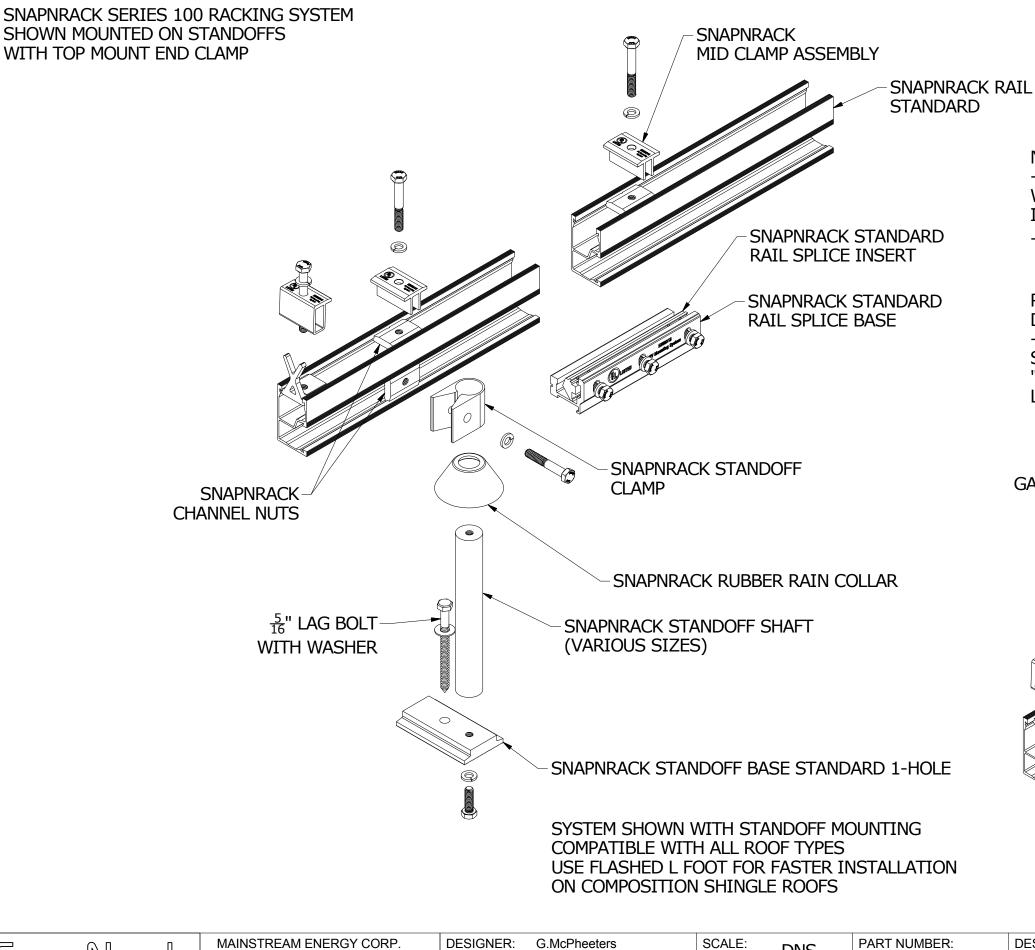
S100 D02

SERIES 100 OVERVIEW, ON STANDOFFS



D Ryan DRAFTER: APPROVED BY:

DATE: 120113



REVISION:

F 12/02/15

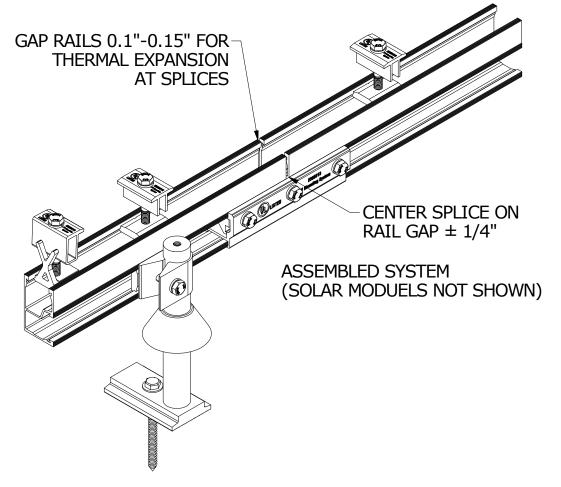
NOTES:

- STANDARD LAG BOLT SPEC ASSUMES 5/16" LAG BOLTS WITH 2.5" EMBEDMENT IN ROOF STRUCTURAL MEMBERS/RAFTERS

- TORQUE ALL 5" HARDWARE TO THE FOLLOWING:
 - SILVER S.S. 10-16 FT-LBS
 - BLACK S.S. 7-9 FT-LBS

RAIL CAN MOUNT TO EITHER SIDE OF POST (UPSLOPE vs. DOWNSLOPE)

- FOR UNEVEN ROOF SURFACES, USE UP TO TWO LEVELING SPACERS PER L FOOT OR STANDOFF. SEE DRAWING "STANDARD RAIL LEVELING" FOR DETAILS AND LIMITATIONS





D.Ryan DRAFTER: APPROVED BY: G.McPheeters DNS

12/02/15

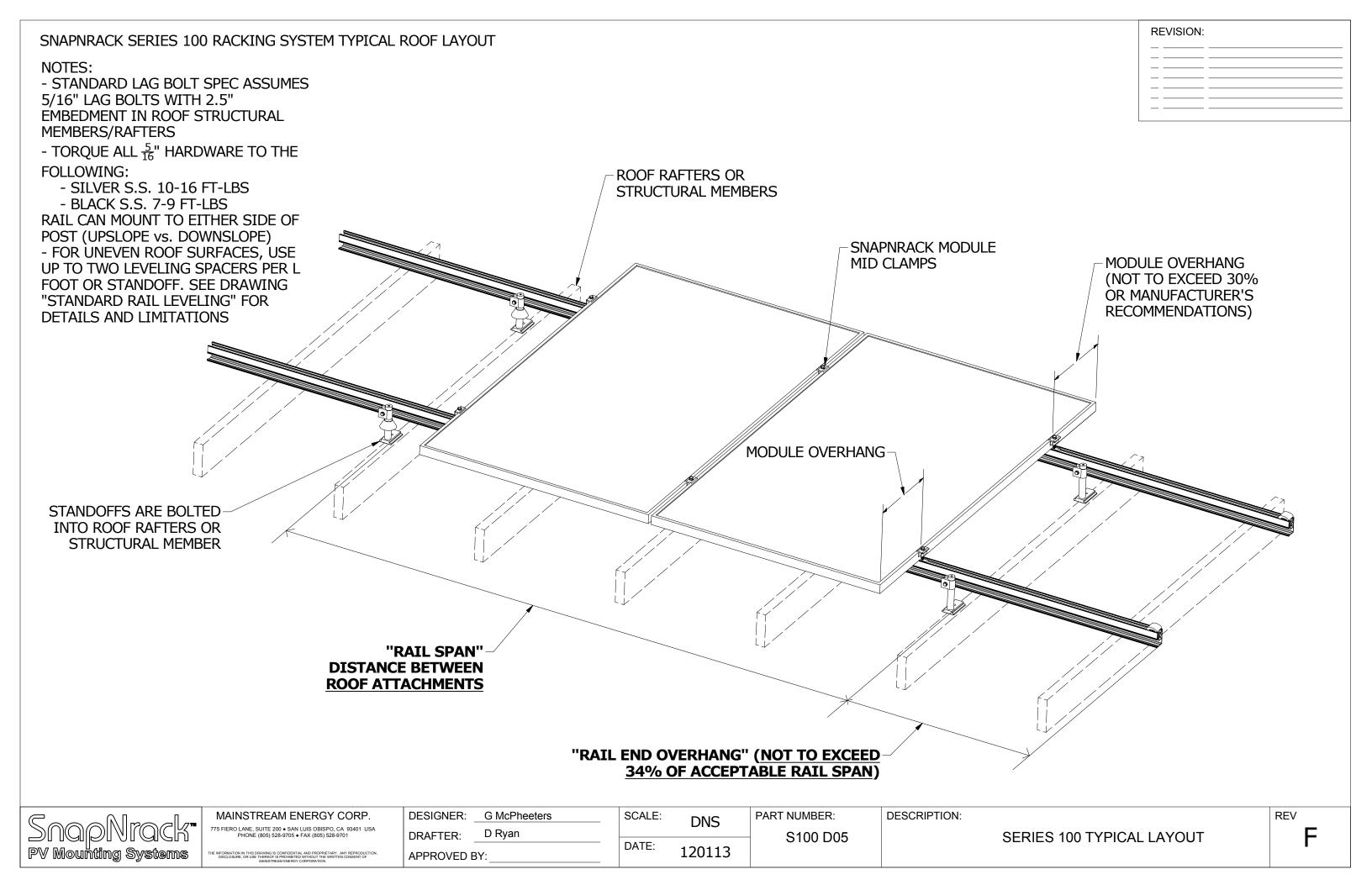
DATE:

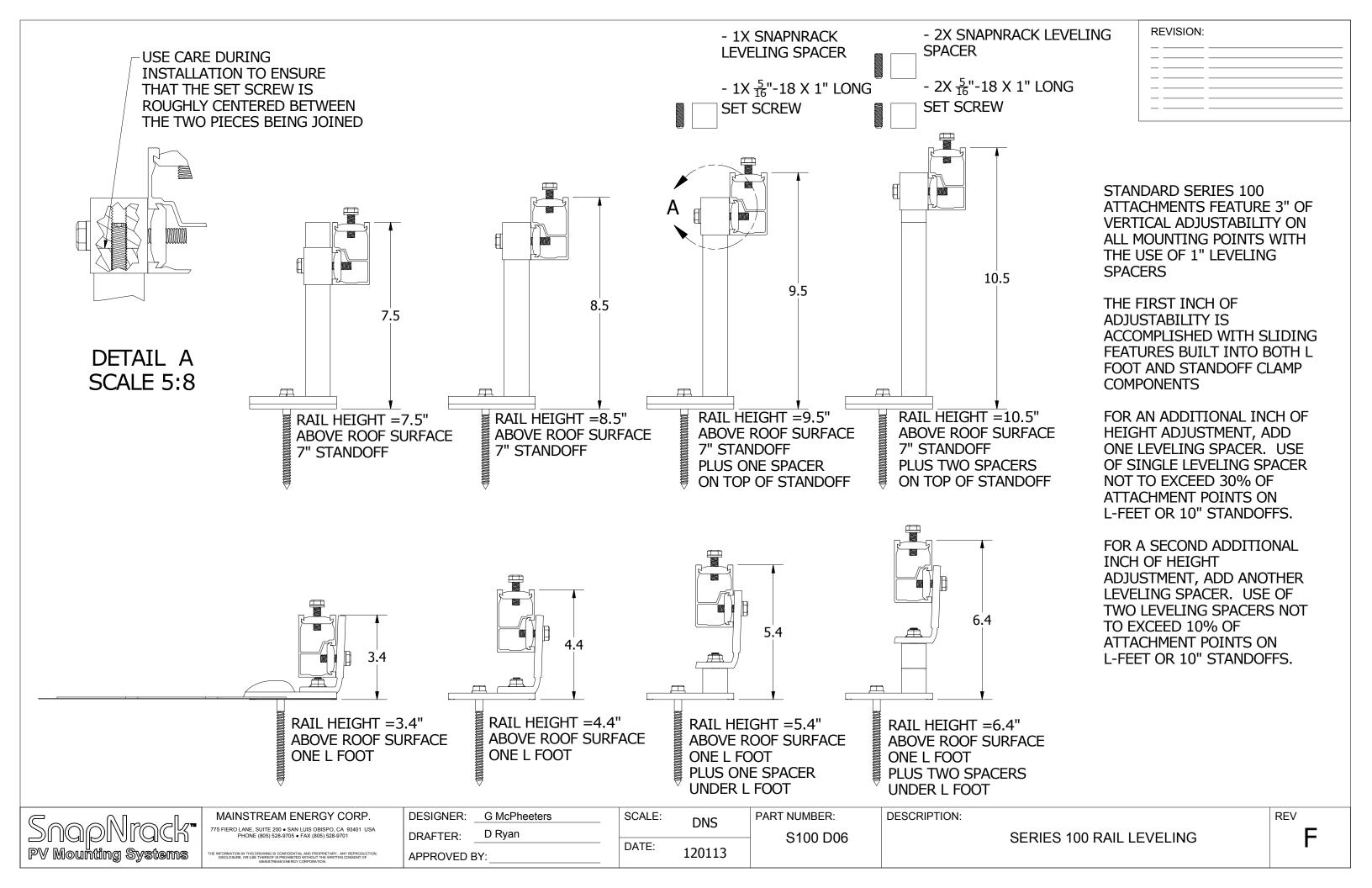
S100 D04

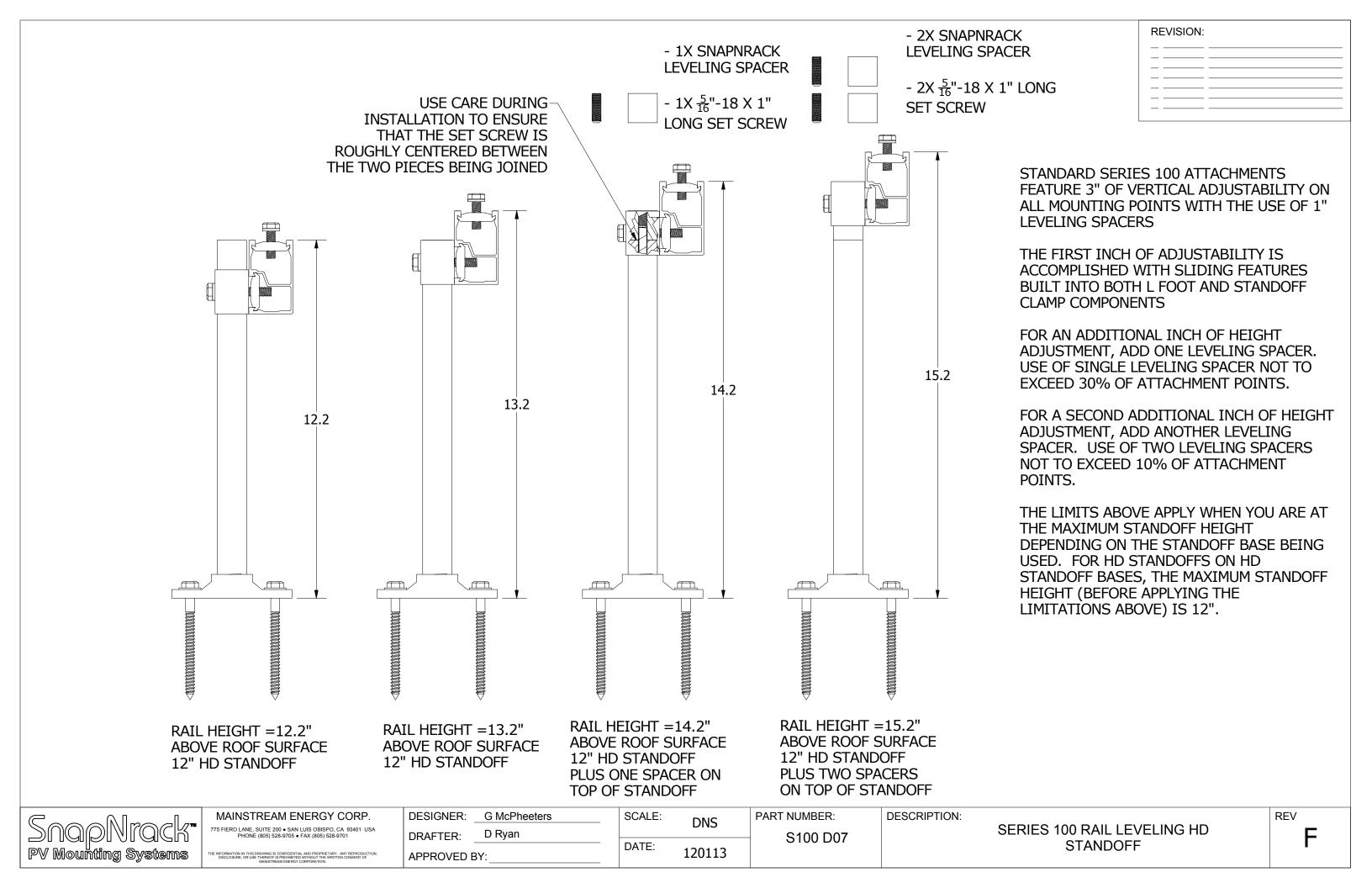
DESCRIPTION:

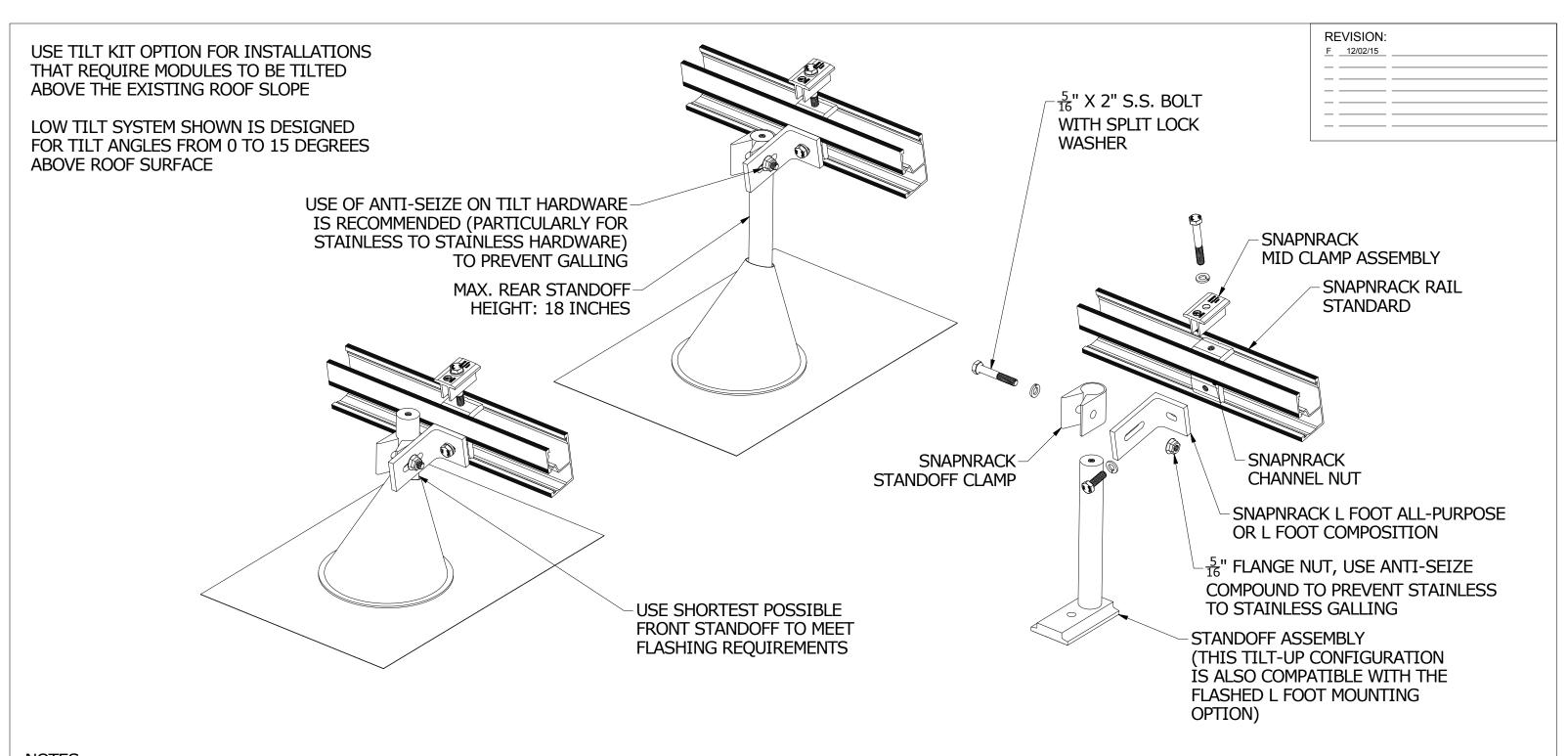
SERIES 100 TILT KITS 0-15 DEG

REV









NOTES:

- TORQUE $\frac{5}{16}$ " HARDWARE TO THE FOLLOWING UNLESS OTHERWISE NOTED:
 - SILVER S.S. 10-16 FT-LBS
 - BLACK S.S. 7-9 FT-LBS
- REFER TO ENGINEERING CHARTS FOR RAIL SPAN BASED ON MODULE TILT ANGLE, WIND SPEED, AND SNOW LOAD
- FOR HIGHER TILT APPLICATIONS SEE "SERIES 100 TILT KIT 10-45 DEG"



MAINSTREAM ENERGY CORP.

DESIGNER: G McPheeters D Ryan DRAFTER: APPROVED BY: G McPheeters SCALE: PART NUMBER: DNS DATE: 12/02/15

DESCRIPTION:

S100 D08

SERIES 100 TILT KITS 0-15 DEG

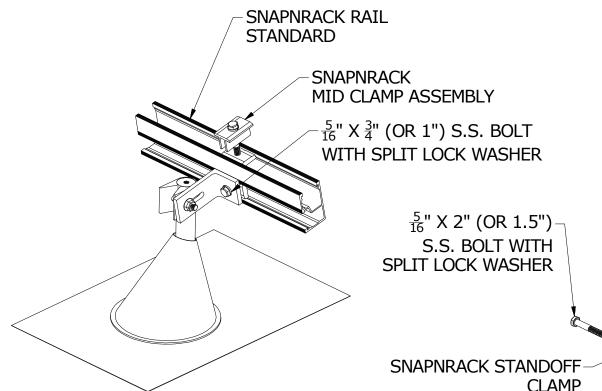
REV

USE TILT KIT OPTION FOR INSTALLATIONS THAT REQUIRE MODULES TO BE TILTED ABOVE THE EXISTING ROOF SLOPE

SYSTEM SHOWN IS DESIGNED FOR TILT ANGLES FROM 10 TO 45 DEGREES ABOVE ROOF SURFACE

USE OF ANTI-SEIZE ON TILT HARDWARE IS RECOMMENDED (PARTICULARLY FOR STAINLESS TO STAINLESS HARDWARE)

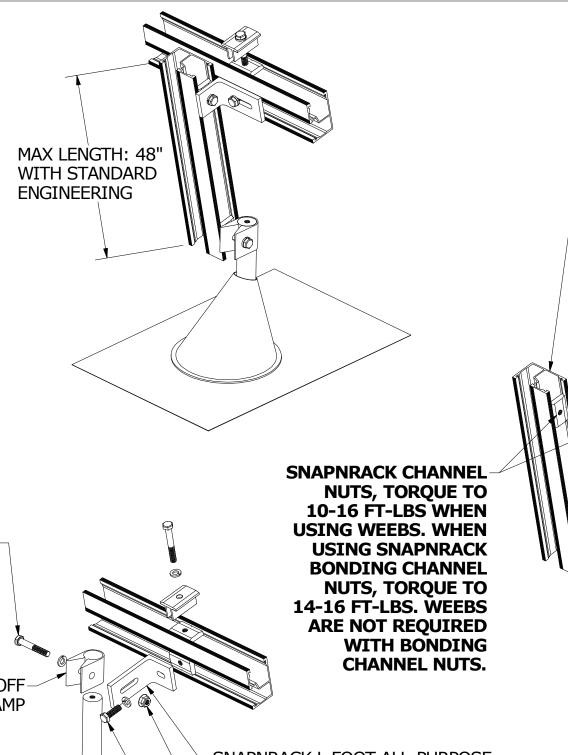
REFER TO S100 TKT SERIES 170 TILT KIT TOOL FOR A SIMPLE TOOL THAT DRAMATICALLY SIMPLIFIES TILT KIT INSTALLATION BY SUPPORTING THE UPPER RAIL AHEAD OF MODULE INSTALLATION



- TORQUE \frac{5}{16}" HARDWARE TO THE FOLLOWING UNLESS OTHERWISE NOTED:
 - SILVER S.S. 10-16 FT-LBS
 - BLACK S.S. 7-9 FT-LBS

NOTES:

- REFER TO ENGINEERING CHARTS FOR RAIL SPAN BASED ON MODULE TILT ANGLE, WIND SPEED, AND NOW LOAD
- BACK SUPPORT "LEG" IS FABRICATED FROM A SCRAP OF RAIL. CALCULATE REQUIRED TILT LEG LENGTH AND CUT RAIL TO LENGTH
- FOR LOWER TILT APPLICATIONS SEE "SERIES 100 TILT KIT 0-15 DEG"
- SNAPNRACK RAIL COVER CAN BE USED TO COVER CHANNEL IN REAR TILT LEG



SNAPNRACK L FOOT ALL-PURPOSE OR L FOOT COMPOSITION

- 등" FLANGE NUT ⁵/₁₆" X 1" (OR 1.25") S.S. BOLT WITH SPLIT LOCK WASHER

S100 D09

STANDOFF ASSEMBLY (THIS CONFIGURATION ALSO COMPATIBLE WITH FLASHED L FOOT MOUNTING



DESIGNER: G McPheeters D Ryan DRAFTER: APPROVED BY:

SCALE: PART NUMBER: DNS DATE:

120113

DESCRIPTION:

SERIES 100 TILT KITS 10-45 DEG

REV

REVISION:

CUT REAR TILT LEG FROM SCRAP

SNAPNRACK RAIL STANDARD

SNAPNRACK L FOOT

L FOOT COMPOSITION

ALL-PURPOSE OR

 $\frac{5}{16}$ " X 1" (OR 1.25") S.S. BOLT

WITH SPLIT LOCK WASHER

SNAPNRACK STANDOFF

CLAMP

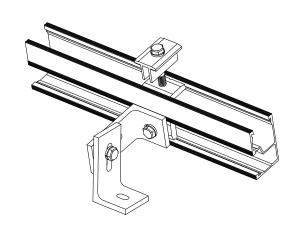
OF STANDARD RAIL

USE TILT KIT OPTION FOR INSTALLATIONS
THAT REQUIRE MODULES TO BE TILTED
ABOVE THE EXISTING ROOF SLOPE

SYSTEM SHOWN IS DESIGNED FOR TILT ANGLES FROM 10 TO 45 DEGREES ABOVE ROOF SURFACE

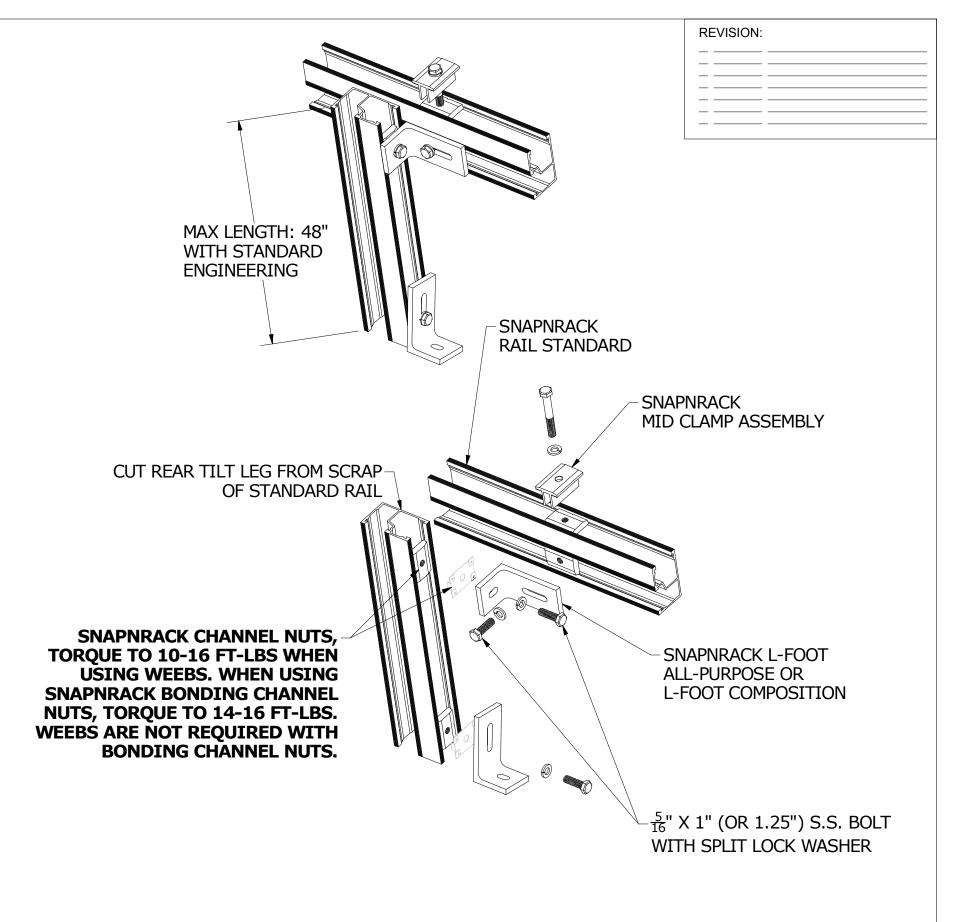
USE OF ANTI-SEIZE ON TILT HARDWARE IS RECOMMENDED (PARTICULARLY FOR STAINLESS TO STAINLESS HARDWARE)

REFER TO S100 TKT SERIES 170 TILT KIT TOOL FOR A SIMPLE TOOL THAT DRAMATICALLY SIMPLIFIES TILT KIT INSTALLATION BY SUPPORTING THE UPPER RAIL AHEAD OF MODULE INSTALLATION



NOTES:

- TORQUE $\frac{5}{16}$ " HARDWARE TO THE FOLLOWING UNLESS OTHERWISE NOTED:
 - SILVER S.S. 10-16 FT-LBS
 - BLACK S.S. 7-9 FT-LBS
- REFER TO ENGINEERING CHARTS FOR RAIL SPAN BASED ON MODULE TILT ANGLE, WIND SPEED, AND SNOW LOAD
- BACK SUPPORT "LEG" IS FABRICATED FROM A SCRAP OF RAIL. CALCULATE REQUIRED TILT LEG LENGTH. USE WEEB GROUNDING WASHERS AT JOINTS BETWEEN L-FEET AND SNAPNRACK STANDARD RAIL SCRAP PIECE
- FOR LOWER TILT APPLICATIONS SEE "SERIES 100 TILT KIT 0-15 DEG"
- SNAPNRACK RAIL COVER CAN BE USED TO COVER CHANNEL IN REAR TILT LEG





MAINSTREAM ENERGY CORP.

75 FIERO LANE. SUITE 200 • SAN LUIS OBISPO. CA. 93401. USA

ISPO, CA 93401 USA 5) 528-9701 DRAFTER: D Ryan
APPROVED BY:

DESIGNER: G McPheeters

DATE: 12011

120113

PART NUMBER: S100 D10

DESCRIPTION:

SERIES 100 TILT KITS 10-45 DEG WITH L FOOT MOUNT REV

USE TILT KIT OPTION FOR INSTALLATIONS THAT REQUIRE MODULES TO BE TILTED ABOVE THE EXISTING ROOF SLOPE

SYSTEM SHOWN IS DESIGNED FOR TILT ANGLES FROM 10 TO 45 DEGREES ABOVE ROOF SURFACE ON STANDING SEAM METAL ROOFS

USE OF ANTI-SEIZE ON TILT HARDWARE IS RECOMMENDED (PARTICULARLY FOR STAINLESS TO STAINLESS HARDWARE)

REFER TO S100 TKT SERIES 170 TILT KIT TOOL FOR A SIMPLE TOOL THAT DRAMATICALLY SIMPLIFIES TILT KIT INSTALLATION BY SUPPORTING THE UPPER RAIL AHEAD OF MODULE INSTALLATION

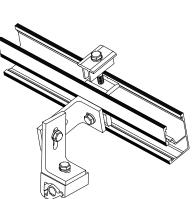
NOTES:

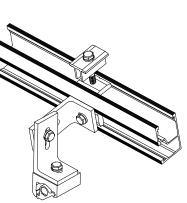
LENGTH

- TORQUE $\frac{5}{16}$ " HARDWARE TO THE FOLLOWING UNLESS OTHERWISE NOTED:
 - SILVER S.S. 10-16 FT-LBS - BLACK S.S. 7-9 FT-LBS
- REFER TO ENGINEERING CHARTS FOR RAIL SPAN BASED ON MODULE

TILT ANGLE, WIND SPEED, AND **SNOW LOAD**

- BACK SUPPORT "LEG" IS FABRICATED FROM A SCRAP OF RAIL. CALCULATE REQUIRED TILT LEG LENGTH AND CUT RAIL TO
- FOR LOWER TILT APPLICATIONS SEE "SERIES 100 TILT KIT 0-15 DEG"
- SNAPNRACK RAIL COVER CAN BE USED TO COVER CHANNEL IN REAR TILT LEG





⁵/₁₆" FLANGE NUT SNAPNRACK L FOOT ALL-PURPOSE OR L FOOT COMPOSITION 5/16" X 1" S.S. BOLT WITH SPLIT LOCK WASHER SNAPNRACK SEAM CLAMP WIDE OR STANDARD BASE

SNAPNRACK

MID CLAMP ASSEMBLY

MAX LENGTH: 48"

WITH STANDARD

ENGINEERING

⁵/₁₆" X 1" (OR 1.25") S.S. BOLT WITH SPLIT LOCK WASHER



MAINSTREAM ENERGY CORP.

DESIGNER: G McPheeters D Ryan DRAFTER: APPROVED BY:

SCALE: PART NUMBER: DNS S100 D11 DATE:

042514

SNAPNRACK CHANNEL NUTS,

USING WEEBS. WHEN USING

BONDING CHANNEL NUTS.

CUT REAR TILT LEG FROM SCRAP

OF STANDARD RAIL

SNAPNRACK SEAM CLAMP

WIDE OR STANDARD BASE

TORQUE TO 10-16 FT-LBS WHEN

SNAPNRACK BONDING CHANNEL NUTS, TORQUE TO 14-16 FT-LBS.

WEEBS ARE NOT REQUIRED WITH

DESCRIPTION:

SERIES 100 TILT KITS 10-45 DEG SEAM **CLAMP MOUNT**

REVISION:

SNAPNRACK

SNAPNRACK

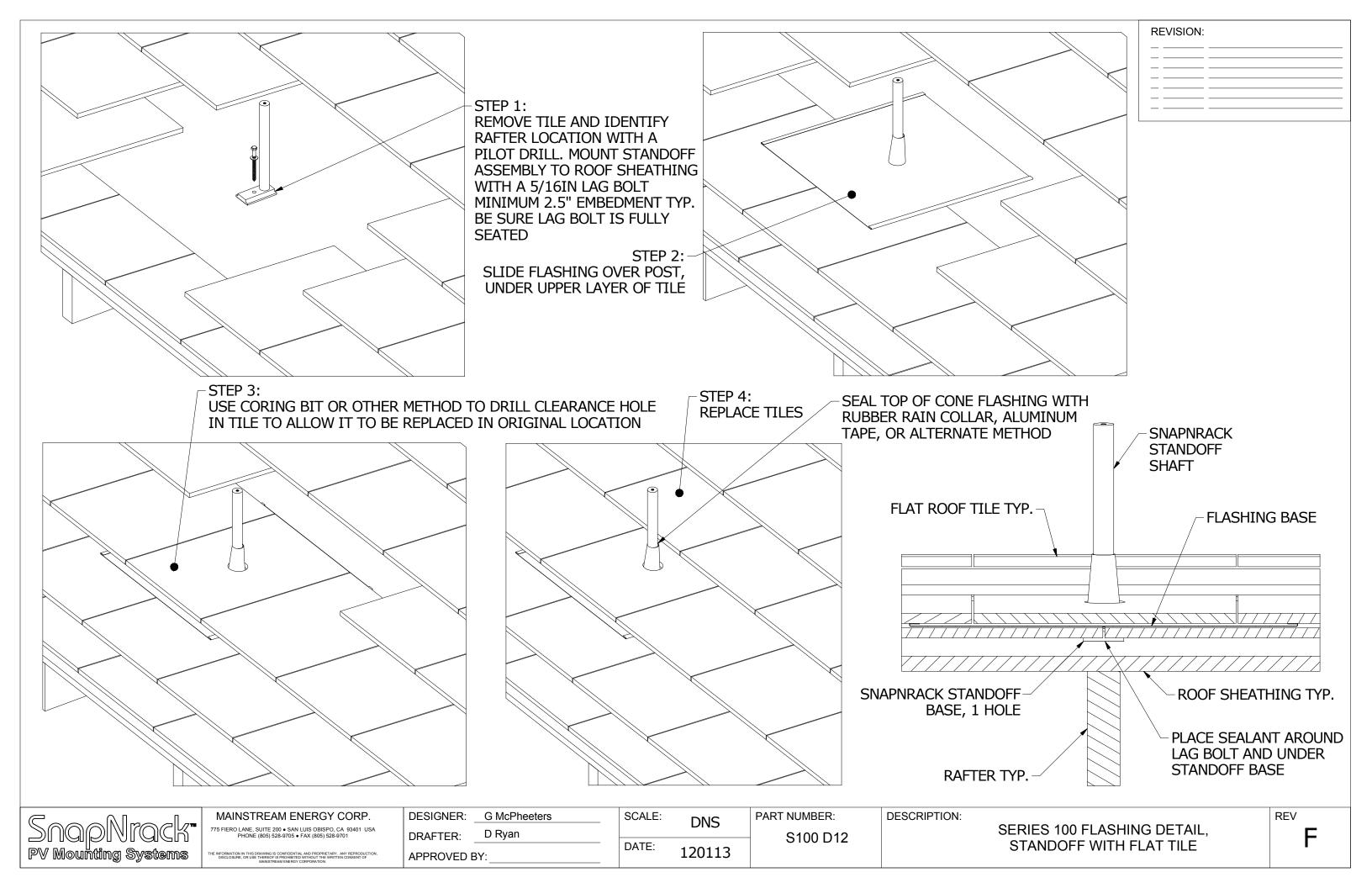
CHANNEL NUT

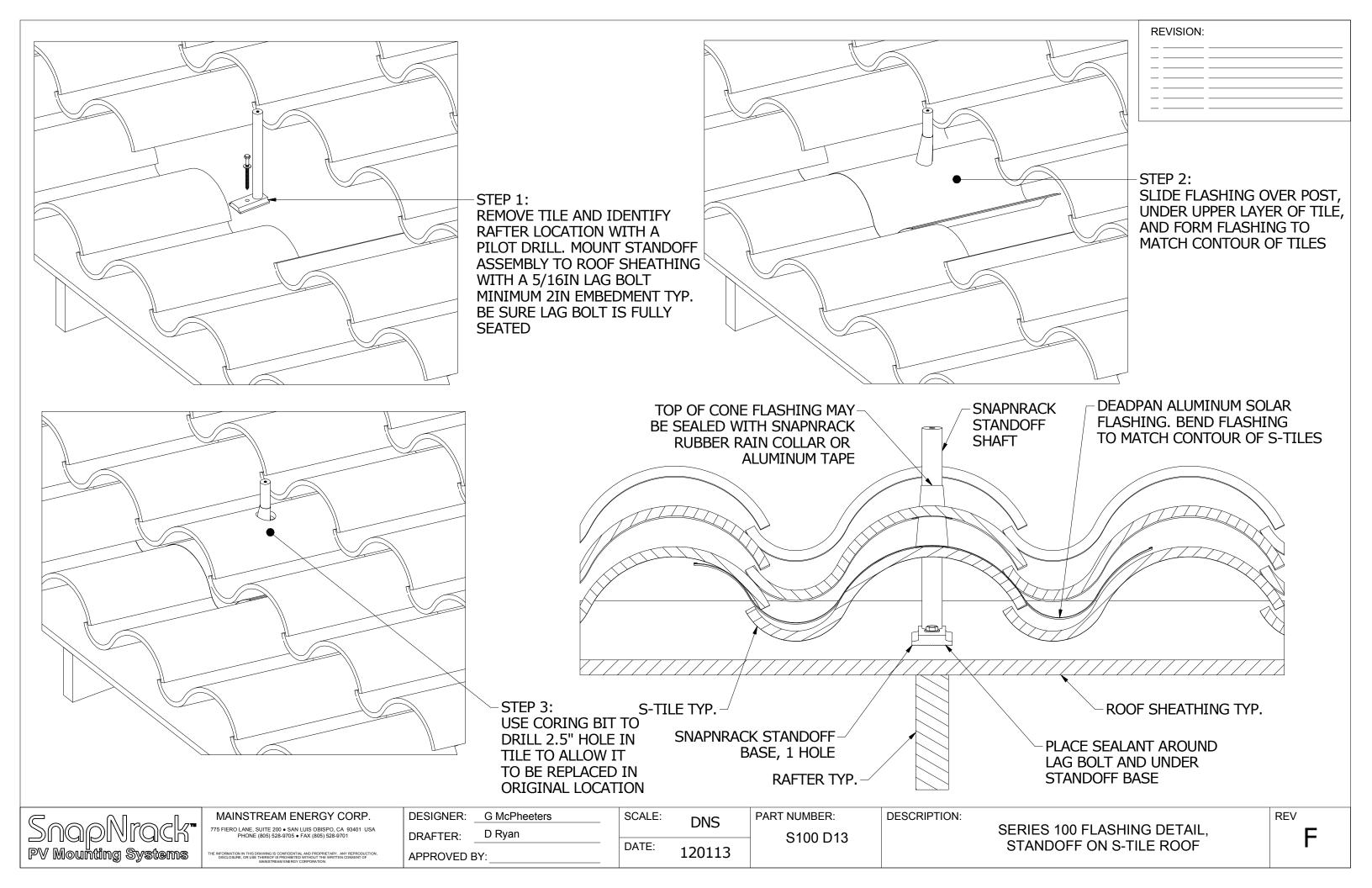
RAIL STANDARD

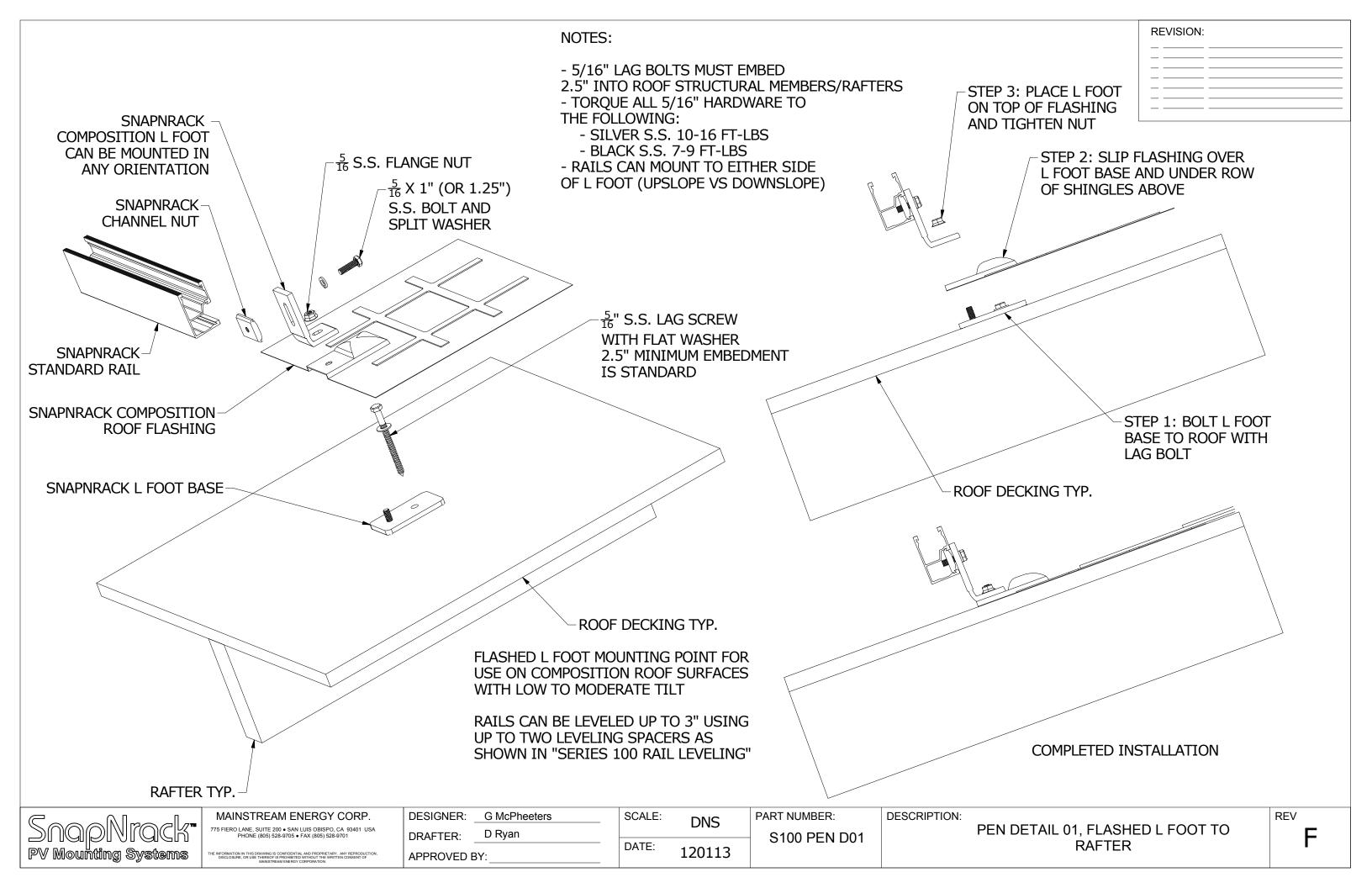
⁵/₁₆" X 1" (OR 1.25") S.S. BOLTS

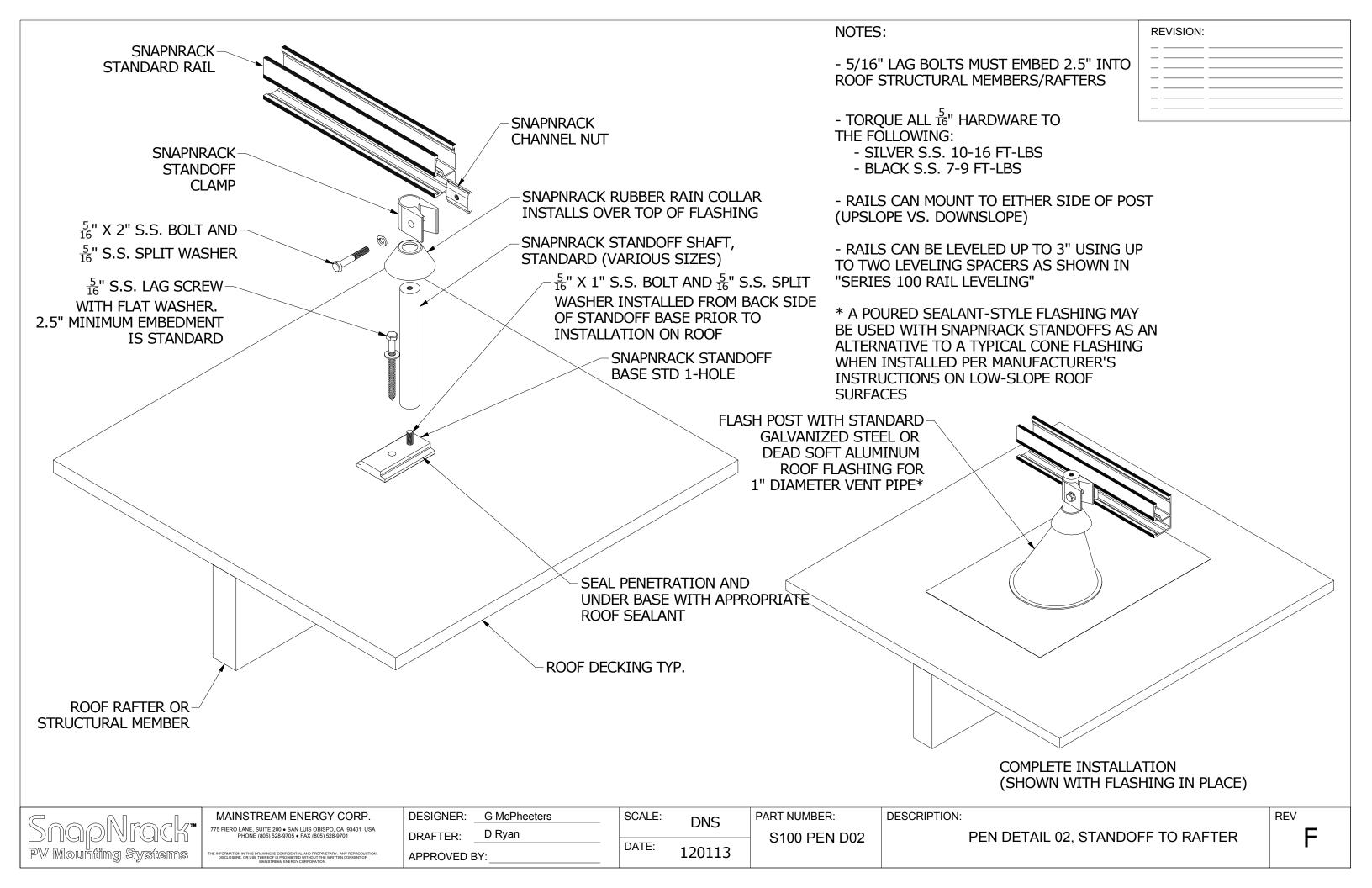
WITH SPLIT LOCK WASHERS

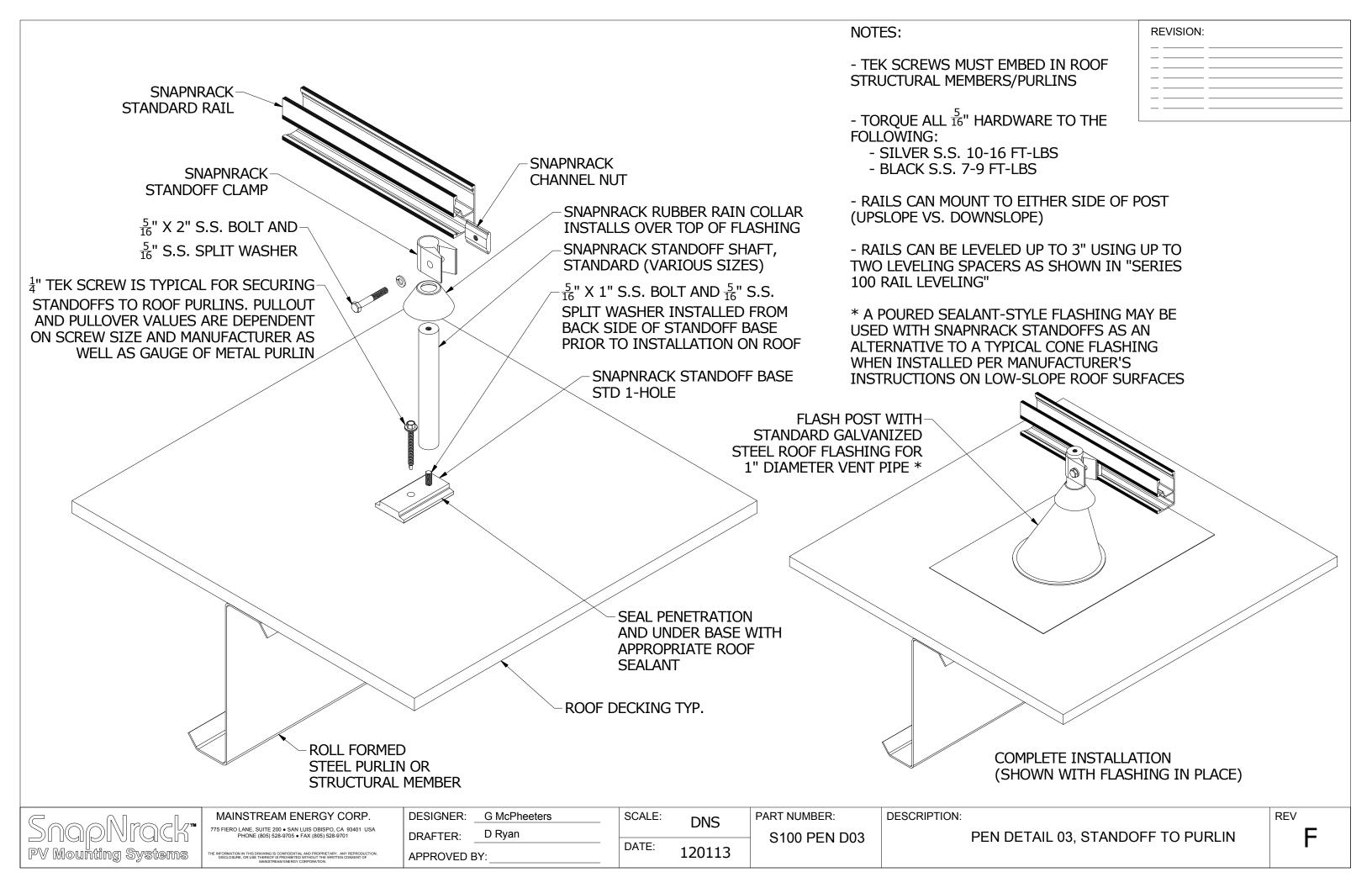
REV











REVISION: CAMMING SEAM CLAMPS ARE SPECIFIED WITH A BLACK OXIDE STAINLESS STEEL BOLT. IT IS IMPORTANT TO USE THE PROVIDED **BOLT AND TO TIGHTEN TO 16** FT-LBS FOR FULL LOAD CAPABILITY CLAMP CAN BE USED TO SECURE RAILS OR DIRECTLY SUPPORT TO DETERMINE BOLT SIZE ADD **SOLAR MODULES** 1.17" TO THE "STACK" ON TOP WITH MODULE CLAMPS OF THE CLAMP (X) AND ROUND UP TO NEAREST 1 BOLT SIZE L FOOT OR SIMILAR TILT-BRACKETS CAN BE ATTACHED TO THE TOP OF THE CLAMP AND PROVIDE A MOUNTING POINT FOR RAILS OR OTHER 3: BOLT IS STRUCTURAL MEMBERS TIGHTENED, SECURING CLAMP AND L 4: TORQUE BOLT FOOT AT THE TO 10-16 FT-LBS SAME TIME "X" SEAM CLAMP BASE (STD BASE SHOWN **BUT INSTALLATION** OF WIDE BASE IS SEAM IDENTICAL) CLAMP CAM 2: OPEN **CLAMP GETS** .5 TYP. 1: INSTALLATION STARTS SEAM **LOWERED ONTO SEAM** CLAMP WITH CLAMP IN **THREAD OPEN POSITION INSERT** WITH BOLT LOOSE 3 4

Sna	PNIACK" nting Systems
PV Moui	nting Systems

MAINSTREAM ENERGY CORP.

775 FIERO LANE, SUITE 200 • SAN LUIS OBISPO, CA 93401 USA PHONE (805) 528-9705 • FAX (805) 528-9701

DESIGNER: G McPheeters D Ryan DRAFTER: APPROVED BY:

SCALE: DNS DATE:

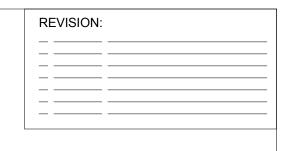
120113

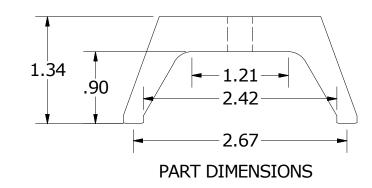
PART NUMBER: S100 PEN D04 **DESCRIPTION:**

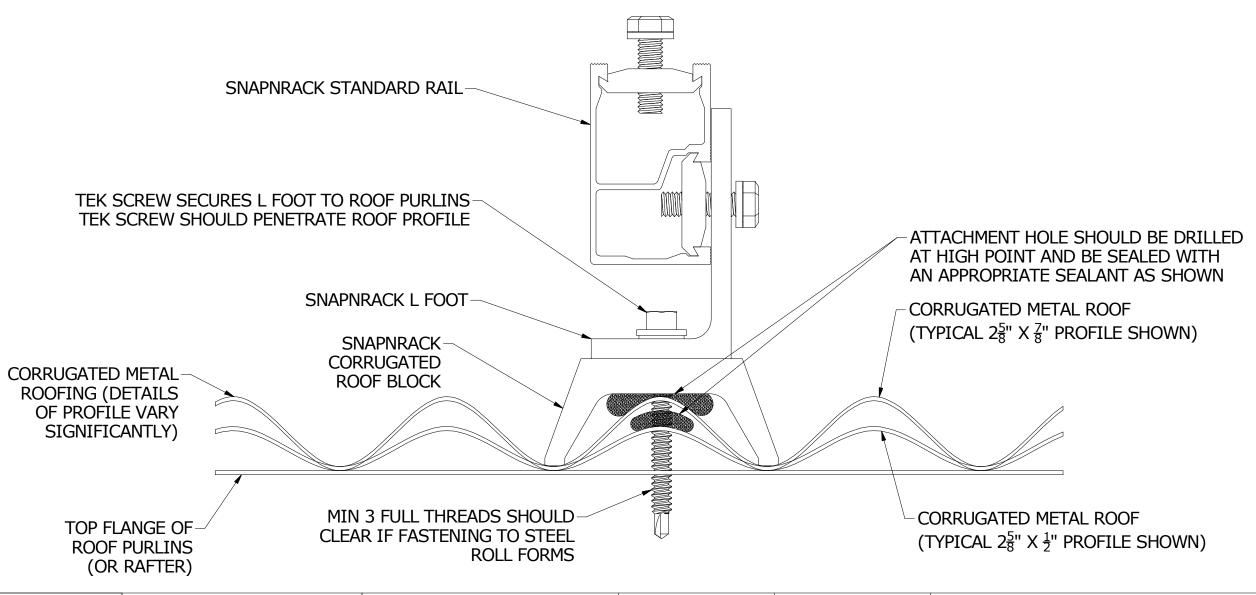
PEN DETAIL 04, SEAM CLAMP

REV

USE THE SNAPNRACK CORRUGATED ROOF BLOCK TO STRADDLE THE RAISED PORTIONS OF CORRUGATED METAL ROOFING MATERIALS. THIS ALLOWS AN L FOOT TO BE MOUNTED WITH THE PENETRATION AT THE HIGH POINT OF THE ROOFING MATERIAL WITHOUT CRUSHING THE ROOF PROFILE. SHOWN WITH A TEK SCREW ATTACHMENT TYPICAL OF A METAL PURLIN STRUCTURE, BUT THE SYSTEM WORKS WELL WITH A LAG BOLT INTO A WOOD RAFTER AS WELL. BE SURE TO USE PROPER SEALANT TO SEAL UP THE HOLE IN THE METAL ROOFING MATERIAL









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DESIGNER: G McPheeters

DRAFTER: D Ryan

APPROVED BY:

SCALE:

DNS

120113

PART NUMBER: S100 PEN D05 DESCRIPTION:

PEN DETAIL 05, CORRUGATED ROOF BLOCK

REV

REVISION: HANGER BOLT CLAMPS HAVE BEEN DESIGNED FOR USE WITH STANDARD 3" STAINLESS HANGER BOLTS. THEY ARE COMPATIBLE WITH ANY 3" STAINLESS BOLT OR THREADED ROD. THE CLAMPS ARE 1.5" TALL AND ENGINEERED TO HAVE A MINIMUM OF 1.25" OF THREAD IN THE CLAMP AT ALL TIMES. MAXIMUM DESIGN LOAD IS 1,000 LBS (AXIAL) OR 250 LBS IF A FACTOR **SNAPNRACK** OF SAFETY OF 4 IS APPLIED. STANDARD RAIL - TORQUE ALL $\frac{5}{16}$ " HARDWARE TO THE FOLLOWING: - SILVER S.S. 10-16 FT-LBS - BLACK S.S. 7-9 FT-LBS **SNAPNRACK CHANNEL NUT** 5/16"x 1.25-1.5" S.S. BOLT W SPLIT LOCK WASHER ASSEMBLED UNIT SNAPNRACK HANGER BOLT CLAMP USE TWO PIECES "BACK TO BACK" PER CLAMP ASSEMBLY, MINIMUM OF 1.25" OF THREADS CLAMPED 3" STAINLESS HANGER BOLT 8" TYPICAL BUT SHORTER SIZES MAY BE USED SO LONG AS 1.25" OF THREADS ARE ENGAGED IN THE BOLT TO RAIL CLAMP MAINSTREAM ENERGY CORP. DESIGNER: G McPheeters SCALE: PART NUMBER: **DESCRIPTION:** REV DNS F D Ryan DRAFTER: S100 PEN D06 PEN DETAIL 06 L HANGER BOLT

DATE:

APPROVED BY:

120113

