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#### CERTIFICATION

I hereby certify that I am the owner of record of the named property, or that the proposed work is authorized by the owner of record and that I have been authorized by the owner to make this application as his authorized agent and I agree to conform to all applicable laws of this jurisdiction. In addition, if a permit for work described in the application is issued, I certify that the code official's authorized representative shall have the authority to enter all areas covered by such permit at any reasonable hour to enforce the provision of the code(s) applicable to such permit.

SIGNATURE OF APPLICANT	ADDRESS	DATE	PHONE
RESPONSIBLE PERSON IN CHARGE OF WORK, TITLE		DATE	DUONE
RESPONSIBLE PERSON IN CHARGE OF WORK, ITTLE		DATE	PHONE

Form # P 04 DISPLAY THIS CARE	O ON PRINCIPAL FRONTAGE OF WORK
Please Read Application And Notes, If Any, Attached	PERMIT PERMIT ISSUED PERMIT Permit Number: 051564 0CT 2 7 2005
This is to certify thatKIMCO REALTY LLC /The	
has permission to FOUNDATION ONLY - con	cted w/ mit #0. 90 CITY OF PORTLAND
AT 599 WARREN AVE	C _ 314 A007001
provided that the person or persons, of the provisions of the Statutes of I the construction, maintenance and u this department.	ine and of the second ances of the City of Portland regulating of buildings and substures, and of the application on file in fication inspection must
Apply to Public Works for street linegand grade if nature of work requiresbsuch information.bbbbbbbbbbbbbbb	A certificate of occupancy must be pre this building or writ thereo and or construction of the section of the section of the section of the BR NOTICE IS REQUIRED.
OTHER REQUIRED APPROVALS	
Fire Dept Health Dept	
Appeal Board Other Department Name	Director - Building & Inspection Services
PENA	ALTY FOR REMOVING THIS CARD $\Box$

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City of Portland, Maine - Build	ding or Use Permit		Permit No:	Date Applied For:	CBL:
389 Congress Street, 04101 Tel: (2	207) 874-8703, Fax: (2	07) 874-8716	05-1564	10/26/2005	314 A007001
Location of Construction:	Owner Name:		Owner Address:		Phone:
599 WARREN AVE	KIMCO REALTY LLC		65 GRAY RD BOX	<u> </u>	
Business Name:	Contractor Name:	1	Contractor Address:	Phone	
	Thompson Building Ser		497 Northern Ave.	Farming Dale	(207) 582-6100
Lessee/Buyer's Name	Phone:	1	Permit Type:		
		L	Foundation Only/C	commercial	
Proposed Use:		-	Project Description:		
FOUNDATION ONLY - connected w	// permit #050990	FOUN	DATION ONLY - (	connected w/ permit	#030990
Dept: Building Status: A	pproved	Reviewer:	Mike Nugent	Approval Da	ite: 10/26/2005
Note:				• •	Ok to Issue: 🔽
Dept: Fire Status: A	pproved	<b>Reviewer:</b>	Lt. MacDougal	Approval Da	te: 06/16/2004
Note:					Ok to Issue: 🗹
	1 11 0 111				02/02/0005
	pproved with Conditions	Reviewer:	Unris Earle/Steve	Bush Approval Da	_
Note:					Ok to Issue: 🗹
1) see planning conditions					(
Dept: Planning Status: A	pproved with Conditions	Reviewer:	Kandi Talbot	Approval Da	te: 03/22/2005
Note:					Ok to Issue: 🗹
1) vi. No building permit shall be iss	ued until the applicant rea	ceives the requ	ired wetlands permi	t from DEP.	
<ol> <li>vii. That the Traffic Engineer revi \$30,000 prior to issuance of a build</li> </ol>			1arch 14, 2005 men	no and that the appli	cant contribute
<ol> <li>v. That the site plans be revised to Engineer.</li> </ol>			subject to the revie	w and approval of th	e Traffic
4) iv. That a revised site plan for the building permit.	Wendy's property shall be	e submitted to	staff for review and	approval prior to iss	uance of a
5) ii. That the City Arborist review as	nd approve the landscapin	ng plan prior to	issuance of a buildi	ing permit.	
6) i. That the applicant revise the plan	ns based on the Traffic E	ngineer's memo	dated March 14, 20	005 and that the app	licant contribute
\$30,000 prior to issuance of a build proposed MDOT/City improvment applicant.	ding permit to the improv	ements at the F	liverside Street/War	ren Avenue intersec	tion. If the
7) iii. That a photometric plan be sub	mitted for review and app	proval by staff,	prior to issuance of	a building permit.	
<ol> <li>viii. That the Traffic Engineer revi may have on accidents at this locati time.</li> </ol>	iew the safety of the intersion. Based on this analys	section regardines	ng the fatal accident Engineer shall deter	and any other recor mine if the intersecti	ds that the City on is safe at this
Comments:			<u> </u>		
10/26/2005-mjn: Fire and Zoning Sign	ed off on permit # 05099	0			

All Purpose Building Permit Application If you or the property owner owes real estate or personal property taxes or user charges on any property within the City, payment arrangements must be made before permits of any kind are accepted.

Location/Address of Construction:	599 WG	scen AU	<u>l -</u>	
Total Square Footage of Proposed Structu /		Footage of Lot 8,465		
Tax Assessor's Chart, Block & LotChart#Block#Lot#314A7	Owner: KIMCO REAL	ty lic	Teleph 797	one: - 7 <i>60</i> 0
Lessee/Buyer's Name (If Applicable)	Applicant name, a telephone: ///// 65 GRAY W.Falmuut	OREALTY LLE RA UNIT 4	Cost Of Work: <b>\$_5</b> Fee: \$	25,000
Current use: VACPATLOT				
If the location is currently vacant, what we	is prior use: VACK	INT		
Approximately how long has it been vaca	Int: <u>///A</u>		·	
Proposed use: NEW DUNICIN Project description:	DONUTS	<u></u>		
Contractor's name, address & telephone; Who should we contact when the permit I	THOM Pooh 497 NO sready: FARMIN	BOILDING SE DETNERM AVE C DALEIME	luices inc	-
	SAME - 582:6			
We will contact you by phone when the p eview the requirements before starting ar and a \$100.00 fee if any work starts before	ly work, with a Plan F	Reviewer. A stop		l be issued
THE REQUIRED INFORMATION IS NOT INCLL ENIED AT THE DISCRETION OF THE BUILDING FORMATION IN ORDER TO APROVE THIS PE	PLANNING DEPARTM	-		
ereby certify that I am the Owner of record of the na	catlon as his/her authorize	d agent. I agree to d	conform to all apple Official's authorized	llcable laws of th ed representative
ve been authorized by the owner to make this applic isdiction. In addition, if a permit for work described in all have the authority to enter all areas covered by tf this permit.	this application is issued, i his permit at any reasonab	le hour to enforce the	e provisions of the	coaes applicadi
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## Report on Subsurface and Foundation Investigation

## Proposed Dunkin Donuts Warren Avenue Portland, Maine

for

Kimco Development Corp. Dunkin Donut Plaza 65 Gray Road Falmouth, ME 04105

October 11, 2005

One Chabot Street, P.O. Box 1339, Westbrook, Maine 04098-1339 Ph. 207-856-0277 Fax 856-2206

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## **Sebago** Technics

Engineering Expertise You Can Build On

sebagotechnics.com

One Chabot Street P.O. Box 1339 Westbrook, Maine 04098-1339 Ph. 207-856-0277 Fax 856-2206

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October 11, 2005 03461

Mr. Ed Wolak Kimco Development Corp. Dunkin Donut Plaza 65 Gray Road Falmouth, ME 04105

### <u>Report on Subsurface and Foundation Investigation</u> Proposed Dunkin Donuts, Warren Avenue, Portland, Maine

Dear Mr. Wolak:

This report presents the results of our subsurface and foundation investigation for the proposed Dunkin Donuts Store on Warren Avenue in Portland, Maine.

In summary, it is our opinion that the store may be supported on footings bearing on the naturally deposited, inorganic soil, or on compacted structural fill placed after removal of unsuitable soil. In addition, a slab-on-grade may be used for the ground floor. Specific recommendations regarding subsurface conditions and foundation requirements are presented below.

#### Introduction

The site is located on Warren Avenue, adjacent to the east side of the Wendy's Restaurant site. The site is presently open and covered in tall grass and weeds. Ground surface elevations within the limits of the proposed building are on the order of El. 56 to El. 57. We understand that the store will be one story with ground floor at El. 57.1.

#### **Subsurface Explorations**

On October 10, 2005, C. H. Stevenson (CHS) of Wayne, Maine excavated four test pits, TP1 to TP4, at locations shown on Sheet 1, Subsurface Exploration Plan. CHS excavated the test pits to depths below ground surface varying from 6.0 feet to 7.0 feet. Sebago Technics, Inc. monitored the test pits and prepared the logs included in Appendix A. CHS backfilled the test pits with the excavated material.

Test pit locations were determined by Sebago Technics, Inc. by pacing from existing site features. Ground surface elevations at test pits were determined by linear interpolation between ground surface contours at the plotted locations.

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The test pit logs and related information depict the subsurface conditions and water levels encountered at the locations and during the times indicated on the logs. Subsurface conditions at other locations may differ from those encountered in the test pits. The passage of time may result in a change in groundwater conditions at the explorations.

#### Subsurface Conditions

The test pits encountered four principal soil units at the site: recent topsoil, fill, original topsoil and marine deposits. Encountered thickness and generalized descriptions are presented below in order of increasing depth below ground surface.

**Recent Topsoil** – Recent topsoil consists of gray brown SILT (ML) with roots. Encountered thickness varied from 0.4 foot to 0.5 foot.

Fill – Fill consists of gray brown mottled SILT (ML); to lean CLAY (CL) with various amounts of sand, gravel and cobbles and trace roots. Encountered thickness varied from 3.3 feet to 5.1 feet.

**Original Topsoil** – The original topsoil encountered below the fill consists of dark gray sandy SILT (ML) with occasional roots. Encountered thickness varied from 0.3 foot to 1.0 foot

**Marine Deposit** – The marine deposit consists of gray lean CLAY (CL). Undrained shear strength in the top of the deposit, as measured by Shear Vane tests, varied from 1,300 pounds per square foot (psf) to 2,500 psf. Test pits penetrated up to 2.3 feet into the marine deposit.

Water was observed seeping slowly into the test pits at depths below ground surface varying from 4.0 feet to 4.5 feet. However, observations of water were made over a relatively short period of time and may not reflect the stabilized groundwater level. In addition, water levels at the site will vary with season, precipitation, temperature and construction activity in the area. Therefore, water levels during and following construction will vary from those observed in the test pits.

#### **Recommendations for Foundation Design**

#### Recommended Foundation Type and Design Criteria

The topsoil and existing fill are not considered suitable for support of the building. All topsoil and fill should be excavated from within the limits of foundations. We recommend that the building be supported on spread and continuous footings bearing on undisturbed, naturally deposited soil or on compacted structural fill placed after removal of unsuitable soil.

For uniformity, footings may be proportioned for an allowable bearing stress equal to 1,000 pounds per square foot (psf) multiplied by the least lateral dimension of the footing in feet, up to a maximum of 3,000 psf. All footings should be at least 1.5 feet wide.

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Exterior footings should be founded at least 4.5 feet below the lowest adjacent ground surface exposed to freezing. Interior footings should be founded a minimum of 1.5 feet below the ground floor slab.

Compacted structural fill supporting footings should extend laterally from the footings to at least the limits defined by 1 horizontal to 1 vertical lines sloped outward and downward from points located at least 2 feet horizontally beyond the bottom edges of the footings.

Subsurface information in the vicinity indicates that the clay extends to depths of 40 feet or more. Correlations with shear strength indicate that the clay is overconsolidated, that is the previous stress is greater than the existing overburden stress. At the recommended bearing stress, we anticipate that settlement will be less than 1 inch. We anticipate that settlement of this magnitude is acceptable. However, final acceptability of settlement should be determined by the structural engineer.

#### Ground Floor Slab

We recommend that the lowest level floor slab be designed as an earth-supported slab-on-grade bearing on a minimum 6-inch thickness of compacted structural fill. All fill containing debris and wood and organics should be removed from within the building limits prior to placing structural fill. The existing fill should be proofrolled with fully-loaded, ten-wheel dump trucks, or equivalent. Any soft or unsuitable area disclosed should be excavated and replaced with compacted structural fill.

All fill placed below the floor slabs for raises-in-grade should consist of compacted structural fill. Normal dampproofing and vapor barriers should be provided below the slab.

#### Seismic Design Considerations

We recommend that the building be designed in accordance with the seismic requirements of the latest edition of the International Building Code; the site classification is Class E; the site response coefficient  $F_a$  is 2.1 for a short period spectral response acceleration  $S_s$  of 0.375g; the site response coefficient  $F_v$  is 3.5 for the one-second period spectral response acceleration  $S_1$  of 0.10g. The subgrade soils are not considered liquefaction susceptible.

#### Lateral Foundation Loads

We recommend that lateral loads be resisted by bottom friction on footings. We recommend that a coefficient of friction equal to 0.35 be used for footings bearing on soil. If this does not provide sufficient resistance, we will study the problem in more detail to take into account other factors.

#### Backfill Materials

Structural fill used below foundations and floor slabs and for backfill adjacent to walls should consist of sandy gravel to gravelly sand. It should be free of organic material, loam, trash, snow, ice, frozen soil and other objectionable material, and should conform to the following gradation:

l

Sieve Size	Percent Finer by Weight
6 inches	100
No. 4	30 to 90
No. 40	10 to 50
No. 200	0 to 8

Compacted structural fill should be placed in layers not exceeding eight inches in loose measure and compacted by self-propelled vibratory equipment at the approximate optimum moisture content to a dry density of at least 95 percent of the maximum dry density, as determined in accordance with ASTM Test Designation D1557. In confined areas, the maximum particle size should be reduced to 3 inches and the loose layer thickness should be reduced to 6 inches, and compaction performed by hand-guided vibratory equipment.

Compacted structural fill on the outside of the foundation walls should extend laterally a minimum of 2 feet from the wall. Backfill beyond this limit may consist of common fill. The surface of fill on the exterior of the building should consist of low permeability material or bituminous pavement to minimize water infiltration next to the building. Grading should provide for runoff away from the building.

Common fill may consist of inorganic mineral soil that can be placed in layers and compacted. Common fill should be placed and spread in layers not exceeding 12 inches in thickness and compacted with a minimum of two systematic passes of the equipment placing the fill.

#### **Construction Considerations**

#### <u>General</u>

The primary purpose of this section of the report is to comment on items related to excavation, earthwork, and related geotechnical aspects of proposed construction. It is written primarily for the engineer having responsibility for preparation of plans and specifications. Since it identifies potential construction problems related to foundations and earthwork, it will also aid personnel who monitor the construction activity.

#### Excavation, Lateral Support and Control of Groundwater

We anticipate that foundation excavation can be accomplished with sloped open excavation through the overburden soils provided safe side slopes can be maintained. Some sloughing and raveling should be anticipated in temporary slopes. Temporary excavations should be made in accordance with all OSHA and other applicable regulatory agency requirements.

We anticipate that groundwater may be encountered at proposed subgrade level or bearing level of footings. If encountered, open pumping from sumps can likely control groundwater. In general, the contractor should control groundwater and water from runoff and other sources by methods which prevent disturbance of bearing surfaces or adjacent soils and allow construction in-the-dry.

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#### Subgrade Preparation

The subgrade soil is susceptible to disturbance from construction traffic. Equipment and personnel should not be permitted to travel across exposed footing bearing surfaces or exposed slab subgrades. Any subgrade areas that are disturbed should be recompacted or excavated and replaced with compacted structural fill prior to placing of concrete. Subgrades should be protected against freezing temperatures if exposed during construction. Final excavation to subgrade should be performed using equipment with smooth-edge buckets.

#### **Construction Monitoring**

The foundation recommendations contained herein are based on the known and predictable behavior of a properly engineered and constructed foundation. Monitoring of the foundation construction is required to enable the geotechnical engineer to keep in contact with procedures and techniques used in construction. Therefore, we recommend that a person qualified by training and experience be present to provide monitoring at the site during excavation of bearing surfaces and placement of compacted structural fill.

#### **Limitations of Recommendations**

This report has been prepared for specific application to the subject project in accordance with generally accepted geotechnical engineering practices. In the event that any changes in the nature, design or location of the building are planned, the conclusions and recommendations contained in this report should not be considered valid, unless the changes are reviewed and the conclusions of this report modified or verified in writing.

The recommendations presented herein are based in part on the data obtained from the referenced test pits. The nature and extent of variations between the explorations may not become evident until construction. If variations then appear evident, it will be necessary to re-evaluate the recommendations of this report.

We request that we be provided the opportunity for a general review of final design and specifications in order to determine that our earthwork and foundation recommendations have been interpreted and implemented in the design and specifications as they were intended.

It has been a pleasure to work with you on this project. Please do not hesitate to contact us if you have any questions or need additional information.

NHHHHH

KENNETH

Willing and Aller

Sincerely,

SEBAGO TECHNICS, INC.

Kenneth L. Recker, P.E. Geotechnical Engineering Manager

KLR:klr/jc Enc.

Sheet 1- Subsurface Exploration PlanAppendix A- Logs of Test Pits

# Appendix A

Logs of Test Pits

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SEBAGO TECHNI INC.				TEST PIT LOG						st Pit		P1			
PROJECT LOCATIO CLIENT CONTRAC EQUIPME	DN CTOR INT		AVENU EVELOP ÆNSON	PORTLAND, MAINE PROJECT N PORTLAND, MAINE PROJECT M ENT CORP. FIELD REP DATE WEATHER		<u>J.</u> <u>K</u> 10	. RE )/10/	Page         1         of           461							
Ground El. El. Datum	·	56.0		Location See Plan	Grou Not E	ndw	ater	depti		itry	rates	s (in/r	min):		
Depth (ft)	Sample ID	Stratum Change	USCS Group	Visual-Manual Identification & Description (density/consistency, color, GROUP NAME & SYMBOL, % oversized, max particle	size,	% Coarse D	kine % Fine %		Sand		7		eld Te		
		Depth (ft) Symbol structure, odor, moisture, optional descriptions, geologic interpretation)							% Medium	% Fine	% Fines	Dilatanc	Plasticity	Strength	
		0.4	ML	ray brown SILT (ML), mps = 0.02 in., roots, damp -TOPSOIL-						5 9	95 S	N	N		
1			ML	ray brown, mottled SILT (ML), mps = 0.02 in., rooys, ocassional gravel and cobble, imp						10 9	0 S	N	N	$\left[ - \right]$	
- 		i							_			+			
_ 2										+		+			
-				-FILL-											
_ 3											+				
_ 4															
-															
											+			_	
- 5		5.5				_			+						
			CL G	lean CLAY (CL), damp					10	90		MI			
- 6				-MARINE DEPOSIT-											
- 7 Bottom of Exploration at 7.0 ft. below ground surface. No refusal  Remarks:											<u>-</u>  -		<u> </u>		
Standing water in completed pit:     Diameter (in.)     Number     Approx. vol. (cu. ft.)     T est Pit Dimension       at depth     Not Encountered     ft.     12 to 24     =     Pit Depth       measured after     hrs. elapsed     over 24     =     Pit Length X Width										7	7.0 x 3.0				

										Ţ	est	Pit N	0.										
SEBAGO					<b>TEST PIT LOG</b>							,	TP	2									
TECHNI INC.	CS,									ե	age		1	of	<u> </u>	1							
PROJECT		DUNKIN E	ONTITS			PROJECT NO		034	61	1.	HEC		<u> </u>	UI									
LOCATIO				E. P(	ORTLAND, MAINE	PROJECT MO		J. P		Y													
CLIENT				MENT CORP. FIELD REP K. RECKI																			
CONTRAC	TOR	C.H. STEV	ENSON	DATE 10/10/200																			
EQUIPME	NT	DEERE 16	OC LC			WEATHER		Cloudy, 50s sundwater depths/entry rates (in/min):															
Ground El El. Datum	·	55.4		ft	Location See Plan		Ground Slow se				/ent	ry ra	tes (i	n/m	in):								
El. Datum											_												
<b>!</b>		Stratum USCS Visual-Manual Identification & Description								S	nd			Field Te									
Depth (ft)	Sample ID		Group		(density/consistency, color, GROUP NAME & SYMBOL, % oversize		ize,	ž		ž		٦.	. 6	ess	à	Ŧ							
		Depth (ft) Symbol structure, odor, moisture, optional descriptions, geologic interpretation)						% Coarse	% Fine	% Coarse	nihi :	% Fines	Dilatancy	Toughness	Plasticity	eng							
				L				%	%	**	2	×   ×	قل	l 🛱	ä	ŝ							
			ML		ay brown SILT (ML), mps = 0.02 in., roots, damp				—	-+	$-\frac{1}{1}$	0 90	ils-	N	N								
		0.4	WIL	101	-TOPSOIL-					-	+		f	<u> </u>									
											_			1									
			ML	Da	rk brown to gray sandy SILT (ML), mps = 0.05 in., pockets of loam and	roots, damp		-			3	0 70	s s	N	N								
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1		3.7			· · · · · · · · · · · · · · · · · · ·																		
				-						-+-	5	-	N	м									
4			CL	Gra	ay lean CLAY (CL), damp					-+		- 33	-	1.41	144								
										_													
					-MARINE DEPOSIT-	,,				+	+	+-	+		$\left  - \right $								
					-MARINE DEFOSIT					-†		+-	+		$\left  - \right $								
5														_									
				At	5.5 ft., undrained shear strength by Shear Vane = 1,600 pounds per squa	are foot				-+													
								-+			-	+-	+	-									
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6			]					_															
				Bot	tom of Exploration at 6.0 ft. below ground surface						+	+-	+										
				_	refusal			-			+-		+										
												1											
														$\left  - \right $									
7								-+	-		+-	+	+-										
Obstruction	18:			Rer	narks:								• • • •		ł								
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	Standing	water in com	pleted pi	t:	Boulders: Diameter (in.) Number Approx. vol	(cu. ft.)		т	eet	Pit D	imer	sion	s (ft)			1							
at depth		Not Encou	intered	ft.	12 to 24 =		Pit Dept	h –			mer			6.0									
measure	d after			hrs.	elapsed over 24 =		Pit Leng	th X	Wid	lth			8.	) x 3	.0								
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TECHNI					<b>TEST PIT LOG</b>								]	CP3	3						
INC. PROJECT	<u> </u>		YONI ITS			DDO IECT N		02	441		Pag	<u>ge</u>		1	oſ	1					
LOCATIO		DUNKIN DONUTS     PROJECT NO.     0346       WARREN AVENUE, PORTLAND, MAINE     PROJECT MGR.     J. PEL															,				
CLIENT				PMENT CORP. FIELD REP K. RECKER													-				
CONTRAC	CTOR	C.H. STEV	'ENSON			DATE		10/10/2005													
EQUIPME	INT	DEERE 16	OC LC			Cloudy, 50s															
Ground El.	•										undwater depths/entry rates (in/min):										
El. Datum									at 4.:					<u>`</u>							
Depth (ft)	Sample III	Stratum USCS Visual-Manual Identification & Description e ID Change Group (density/consistency, color, GROUP NAME & SYMBOL, % oversized, max particle size, stru-							avel	<u> </u>	Sand					Test					
		Depth (ft)	Symbol		odor, moisture, optional descriptions, geologic in	terpretation)	siructure,	% Coarse	% Fine	% Coarse	% Mediu	% Fine	% Fines	Dilatancy	Toughness	Plasticity	Strength				
			ML	Gra	y brown SILT (ML), mps = 0.02 in., roots, damp							10	90	s	N	N					
ļ		0.5			-TOPSOIL-									Ĕ		Ï					
			CL	Gra	y brown lean CLAY (CL), roots and pockets of orange brown san	d, damp	<u> </u>		-	-		10	90	s	N	N					
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5										-	-				4	_	_				
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]		5.4	ML	Dark	gray SILT (ML) with roots, damp			_	Ţ	$\square$	$\square$										
ł		5.7		- ai K	-ORIGINAL TOPSOIL-			-+				10 9	10 1	S N	N I	4	4				
ļ			CL	Эгау	lean CLAY (CL), damp -MARINE DEPOSIT-			+	+	-+	-+	-	00 1	NN	a to	1	┥				
- 6			<del> </del>	At 6.	0 ft., undrained shear strength by Shear Vane = 1,300 pounds per	square foot									1		]				
ł				Botto	m of Exploration at 6.0 ft. below ground surface	····		-+	-+							+	_				
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Obstructions	<u> </u>	<u></u>	F	lema	arks:												┦				
			F																		
			F														+				
	<b>.</b>				Boulders:												1				
at depth	Standing v	vater in comp 5.9	pleted pit: fi		Diameter (in.) Number Approx	. vol. (cu. ft.)	Dit Dant		<u>`est</u>	<u>Pit I</u>	Dime	ensic	ons (f		•						
measured	l after	0.25	h	rs. el	apsed over 24		Pit Depth Pit Length		Widt	h		_		6.( 8.0 x			-				
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TECHNI		TEST PIT LOG															ГР	4												
INC.		-												_										Pa	ge		1	of		1
PROJECT		DUNKINE														_	PRC	JECT	'NO.		03	461				_				
LOCATIO	N	WARREN				MAIN	NE									_	PRO	JECT	MG	R.	J. I	PER	RY							
CLIENT CONTRAC	TOP	KIMCO DE C.H. STEV			T CORP.											-		LD RE	P		K. RECKER									
EQUIPME		DEERE 160														-	DAT	TE ATHEI	n		10/10/2005 Cloudy, 50s									
Ground El.		57.0		fi li	Location		See P	Plan		_							W EA	THE												
El. Datum				<u> </u>	Location	نہ -		1 1455												Groun Not E				1s/e	ntry	' rat	es (i	n/m	in):	
		1								<u> </u>		τ-	-	<b></b>	<u> </u>		<b></b>	Τ-												
Depth (ft)	Sample ID	Stratum         USCS         Visual-Manual Identification & Description           (D)         Change         Group         (density/consistency, color, GROUP NAME & SYMBOL, % oversized, max particle size, structure, odor, moisture, optional descriptions, geologic interpretation)						ze,	% Coarse 5	% Fine	% Coarse	San		% Fines	F		Plasticity 5													
			[- <u></u>								·																			
		0.4	ML	Gray	y brown SI	ILT (M	1L), m	nps =	= 0.02		roots, OPSO			<u>-</u>					~		_				10	90	S	N	N	
											01.00					<u> </u>								-		<u> </u>				
			ML	Gray	y brown m	ottled S	SILT	(ML)	.), mp	ps = 0	0.02 in	n., roo	ts and	pock	ets of s	sand,	damp	)							10	90	s	N	N	
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		3.8					_																							
- 4			ML	Dark	gray sand	V SII T	r om	) mn	nc = 0	0.02 :								<u> </u>			_	_		_	_		_		_	_
					<u>Billy</u> 50.70	<u>j 0111</u>	(0.0	<u>., mp</u>	<u>ps v</u>	0.02 1	<u>m., 10</u>	1013, 14											-+-		30	70	s I	× [	N	
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		4.8								-OR	RIGIN,	IAL TO	OPSO	IL							_									_
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- ,			CL	Gray I	iean CLA	Y (CL)	), dam	np													-+	$-\dagger$	-	-	5	95		v l	M	
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E				At 6.5	5 ft., undra	ined sh	hear s	streng	gth by	y She	ear Va	ane = 2	2,500 1	pound	s per s	quar	e foot				-	-+		-	$\rightarrow$	-+		+	-	
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				Botton No res	m of Explo	oration	at 6.5	5 ft. b	below	w groi	und si	urface									1			1				1	1	
7			ť	NU TES	ausal					·					·						+	-+		+	$\downarrow$	_	$\downarrow$	-	-	_
Obstructions	:		l	Rema	arks:																		<u> </u>							4
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	Standing w	ater in comp	leted nit				Dier	meter	r (ir `				ders:						Τ			-		 -						1
at depth	-	Not Encoun	tered f	ł.		—		2 to 2		<u>, r</u>	Numb		=	Ар	prox.	vol. (	(cu. ft	.)	Pir	Denth		est l	Pit D	ime	nsio	ns (	_	.5		
measured	after	Not Encountered     n.     12 to 24     =     Pit Depth       hrs. elapsed     over 24     =     Pit Lengt							hX	Wid	th		_		8.0		)	-												
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