



May 23, 2016

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**Subject:** **Structural Analysis Report**

**Carrier Designation:** **Verizon Wireless Co-Locate**  
**Carrier Site Name:** Portland 12 ME

**Crown Castle Designation:** **Crown Castle BU Number:** 878782  
**Crown Castle Site Name:** Portland Warren Ave  
**Crown Castle JDE Job Number:** 356689  
**Crown Castle Work Order Number:** 1232451  
**Crown Castle Application Number:** 321952 Rev. 13

**Engineering Firm Designation:** **B+T Group Project Number:** 86959.008.01

**Site Data:** **188 Warren Ave, Portland, Cumberland County, ME**  
**Latitude 43° 41' 15.16", Longitude -70° 18' 14.96"**  
**180 Foot - Monopole Tower**

Dear Sean Dempsey,

B+T Group is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 904844, in accordance with application 321952, revision 13.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

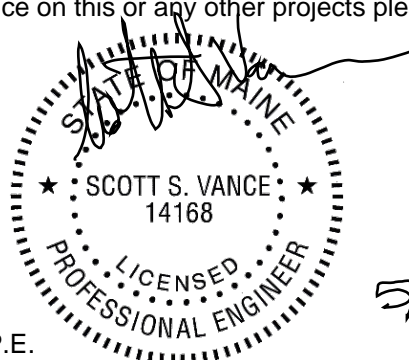
LC7: Existing + Reserved + Proposed Equipment **Sufficient Capacity**  
Note: See Table 1 and Table 2 for the proposed and existing/reserved loading, respectively.

The analysis has been performed in accordance with the TIA-222-G standard and 2009 International Building Code based upon a wind speed of 100 mph 3-second gust, exposure category C.

All equipment proposed in this report shall be installed in accordance with the attached drawings for the determined available structural capacity to be effective.

We at B+T Group appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:  
B+T Engineering, Inc.



5/23/16

Leena Kantheti, E.I.T.  
Project Engineer

Scott S. Vance, P.E.  
Engineer of Record

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## 1) INTRODUCTION

This is a 180 ft. monopole designed by Pittsburg Monopole Division in February of 1997. The monopole was originally designed for a wind speed of 85 mph per TIA/EIA-222-F. This monopole has been modified by Crown Castle in April of 2012, B+T Group in March of 2013 and July 2015 and Crown Castle in February of 2016 and those modifications were incorporated in this analysis.

## 2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA-222-G Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a 3-second gust wind speed of 100 mph with no ice, 40 mph with 1 inch ice thickness and 60 mph under service loads, exposure category C with topographic category 1 and crest height of 0 feet.

**Table 1 - Proposed Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
110.0	110.0	3	Alcatel Lucent	B13 RRH 4X30	2	1-5/8	--
		3	Alcatel Lucent	B25 RRH4X30			
		3	Alcatel Lucent	RRH2X60-AWS			
		6	Commscope	SBNHH-1D65C			
		2	Rfs Celwave	DB-B1-6C-12AB-0Z			
		1	--	Platform Mount [LP 1301-1]			

**Table 2 - Existing and Reserved Antenna and Cable Information**

Matches Antenna Rec dated 4/30/16

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note			
177.0	179.0	1	RFS Celwave	APXV9ERR18-C-A20	3	1-1/4	1			
		2	RFS Celwave	APXVSP18-C-A20						
		3	RFS Celwave	IBC1900BB-1						
		3	RFS Celwave	IBC1900HG-2A						
	177.0	1	--	Platform Mount [LP 715-1]						
175.0	176.0	3	Alcatel Lucent	PCS 1900MHz 4x45W-65MHz	--	--	1			
	175.0	1	--	Side Arm Mount [SO 102-3]						
171.0	171.0	<b>6</b>	<b>DAPA</b>	<b>58010</b>	<b>6</b>	<b>1-5/8</b>	<b>3</b>			
		1	--	Platform Mount [LP 401-1]						
162.0	162.0	2	KMW Comm.	AM-X-CD-16-65-00T-RET	--	--	1			
		3	Powerwave Tech.	7020.00						
		3	Powerwave Tech.	7770.00						
		1	Powerwave Tech.	P65-17-XLH-RR						
		1	Raycap	DC6-48-60-18-8F						
		2	CCI Antennas	HPA-65R-BUU-H6				12 4 2	1-5/8 5/8 3/8	2
		1	CCI Antennas	HPA-65R-BUU-H8						
		2	CCI Antennas	OPA-65R-LCUU-H6						
1	CCI Antennas	OPA-65R-LCUU-H8								

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
		3	Ericsson	RRUS 11			
		3	Ericsson	WCS RRUS-32-B30			
		1	Raycap	DC6-48-60-18-8F			
		1	--	Platform Mount [LP 1301-1]			
	161.0	3	Ericsson	RRUS A2			
		4	Powerwave Tech.	LGP21401			
		1	Powerwave Tech.	TT19-08BP111-001			
		6	Ericsson	RRUS-11			

Notes:

- 1) Existing Equipment
- 2) Reserved Equipment
- 3) Equipment To Be Removed; Not Considered in This Analysis

**Table 3 - Design Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
180	180	12	Generic	Antenna (4 sq. ft)	--	--
170	170	2	Generic	6'Dish	--	--
160	160	12	Generic	Antenna (4 sq. ft)	--	--

### 3) ANALYSIS PROCEDURE

**Table 4 - Documents Provided**

Document	Remarks	Reference	Source
Online Application	Verizon Wireless Co-Locate, Rev# 13	321952	CCI Sites
Tower Manufacturer Drawings	Pittsburg Monopole Division, Project No. 96088-88	1451234	CCI Sites
Foundation Drawings	Pittsburg Monopole Division, Project No. 96088-88	1480918	CCI Sites
Geotech Report	GGA Inc., Project No. 96127ME	1562092	CCI Sites
Tower Modification Drawings	Crown Castle, Project No. 489572	3160195	CCI Sites
Post Modification Inspection	TEP, Project No. 127768	3360218	CCI Sites
Tower Modification Drawings	B+T Group, Project No. 86959.001.01	3671974	CCI Sites
Post Modification Inspection	TEP, Project No. 30386.4873	4138879	CCI Sites
Tower Modification Drawings	B+T Group, Project No. 86959.005.01	5755010	CCI Sites
Tower Modification Drawings	Crown Castle, Project No. 1183035	6110071	CCI Sites
Antenna Configuration	Crown CAD Package	Date:05/05/2016	CCI Sites

#### 3.1) Analysis Method

tnxTower (version 7.0.5.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

### 3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Mount areas and weights are assumed based on photographs provided.
- 5) The existing base plate grout was not considered in this analysis.

This analysis may be affected if any assumptions are not valid or have been made in error. B+T Group should be notified to determine the effect on the structural integrity of the tower.

### 4) ANALYSIS RESULTS

**Table 5 - Section Capacity (Summary)**

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	180 - 145.7	Pole	P24x3/8	1	-10.679	901.775	68.4	Pass
L2	145.7 - 140	Pole	P24x3/8 [0.677164]	2	-11.840	2026.420	50.7	Pass
L3	140 - 106.42	Pole	P36x1/2	3	-23.518	1806.730	75.9	Pass
L4	106.42 - 100	Pole	P36x1/2 [0.759201]	4	-25.816	3354.020	59.6	Pass
L5	100 - 86.25	Pole	P42x1/2	5	-29.923	2112.090	86.3	Pass
L6	86.25 - 78	Pole	P42x1/2 [0.732342]	6	-33.456	3686.900	71.6	Pass
L7	78 - 60	Pole	P42x1/2 [0.914993]	7	-42.981	4586.050	73.6	Pass
L8	60 - 46.25	Pole	P48x5/8	8	-48.727	3013.870	91.8	Pass
L9	46.25 - 32.67	Pole	P48x5/8 [0.826841]	9	-56.171	3753.930	84.1	Pass
L10	32.67 - 20	Pole	P48x5/8 [0.983981]	10	-64.391	5731.410	79.6	Pass
L11	20 - 11.25	Pole	P54x5/8	11	-68.515	3395.570	104.8	Pass <sup>2</sup>
L12	11.25 - 9	Pole	P54x5/8 [0.793292]	12	-69.864	4116.960	87.1	Pass
L13	9 - 0	Pole	P54x5/8 [0.884318]	13	-75.746	4480.350	84.7	Pass
							Summary	
						Pole (L11)	104.8	Pass <sup>2</sup>
						Rating =	104.8	Pass <sup>2</sup>

**Table 6 - Tower Component Stresses vs. Capacity - LC7**

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Bridge Stiffeners	140	28.6	Pass
1	Flange Bolts	140	13.0	Pass
1	Flange Plate	140	10.3	Pass
1	Bridge Stiffeners	100	75.2	Pass
1	Flange Bolts	100	46.0	Pass
1	Flange Plate	100	20.5	Pass
1	Bridge Stiffeners	60	82.4	Pass
1	Flange Bolts	60	40.3	Pass
1	Flange Plate	60	18.4	Pass
1	Bridge Stiffeners	20	62.3	Pass
1	Flange Bolts	20	37.4	Pass
1	Flange Plate	20	16.8	Pass

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1,2	Anchor Rods	Base	103.7	Pass
1	Base Plate	Base	43.1	Pass
1	Base Foundation	Base	86.7	Pass

<b>Structure Rating (max from all components) =</b>	<b>104.8%</b>
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Notes:

- 1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.
- 2) Capacities up to 105% are considered acceptable based on analysis methods used.

**4.1) Recommendations**

The tower and its foundation have sufficient capacity to carry the existing, reserved, and proposed loads. No modifications are required at this time.

**APPENDIX A**  
**TNXTOWER OUTPUT**

**DESIGNED APPURTENANCE LOADING**

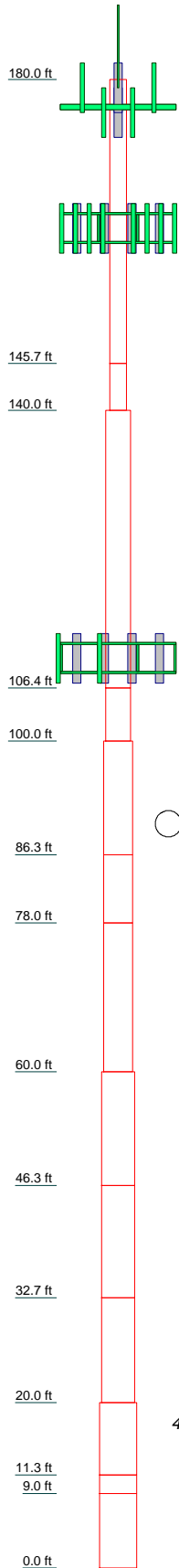
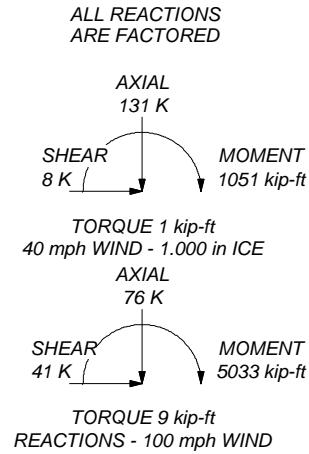
TYPE	ELEVATION	TYPE	ELEVATION
Lighting Rod 5/8" x 8' (E)	184	DC6-48-60-18-8F (E)	162
APXVSP18-C-A20 w/ Mount Pipe (E)	177	HPA-65R-BUU-H8 (R)	162
APXV9ERR18-C-A20 w/ Mount Pipe (E)	177	HPA-65R-BUU-H6 (R)	162
APXVSP18-C-A20 w/ Mount Pipe (E)	177	HPA-65R-BUU-H6 (R)	162
IBC1900BB-1 (E)	177	OPA-65R-LCUU-H8 (R)	162
IBC1900BB-1 (E)	177	OPA-65R-LCUU-H6 (R)	162
IBC1900BB-1 (E)	177	OPA-65R-LCUU-H6 (R)	162
IBC1900BB-1 (E)	177	TT19-08BP111-001 (R)	162
IBC1900HG-2A (E)	177	RRUS A2 (R)	162
IBC1900HG-2A (E)	177	RRUS A2 (R)	162
IBC1900HG-2A (E)	177	RRUS A2 (R)	162
(3) 3' x 2" Pipe Mount (E)	177	RRUS 11 (R)	162
(3) 3' x 2" Pipe Mount (E)	177	RRUS 11 (R)	162
(3) 3' x 2" Pipe Mount (E)	177	RRUS 11 (R)	162
Platform Mount [LP 715-1] (E)	177	WCS RRUS-32-B30 (R)	162
PCS 1900MHz 4x45W-65MHz (E)	175	WCS RRUS-32-B30 (R)	162
PCS 1900MHz 4x45W-65MHz (E)	175	WCS RRUS-32-B30 (R)	162
PCS 1900MHz 4x45W-65MHz (E)	175	(2) LGP21401 (R)	162
4' x 2" Pipe Mount (E)	175	(2) LGP21401 (R)	162
4' x 2" Pipe Mount (E)	175	DC6-48-60-18-8F (R)	162
4' x 2" Pipe Mount (E)	175	Platform Mount [LP 1301-1] (R-4M.P/Sec)	162
Side Arm Mount [SO 102-3] (E)	175	Bridge Stiffener (48"x1.25"x11.5") (E)	140
7770.00 (E)	162	Bridge Stiffener (48"x1.25"x11.5") (E)	140
7770.00 (E)	162	Bridge Stiffener (48"x1.25"x11.5") (E)	140
7770.00 (E)	162	(2) DB-B1-6C-12AB-0Z (P)	110
P65-17-XLH-RR (E)	162	(3) RRH2X60-AWS (P)	110
AM-X-CD-16-65-00T-RET (E)	162	(3) B25 RRH4X30 (P)	110
AM-X-CD-16-65-00T-RET (E)	162	Platform Mount [LP 1301-1] (P-4M.P/Sec)	110
7020.00 (E)	162	(4) SBNHH-1D65C (P)	110
7020.00 (E)	162	(2) SBNHH-1D65C (P)	110
7020.00 (E)	162	(3) B13 RRH 4X30 (P)	110
(2) RRUS-11 (E)	162		
(2) RRUS-11 (E)	162		
(2) RRUS-11 (E)	162		

**MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A36	36 ksi	58 ksi	34.039003ksi	34 ksi	49 ksi
45.379688ksi	45 ksi	60 ksi	43.816406ksi	44 ksi	59 ksi
44.3375ksi	44 ksi	59 ksi	34.497269ksi	34 ksi	49 ksi
43.146429ksi	43 ksi	58 ksi	33.7356ksi	34 ksi	49 ksi

**TOWER DESIGN NOTES**

1. Tower is located in Cumberland County, Maine.
2. Tower designed for Exposure C to the TIA-222-G Standard.
3. Tower designed for a 100 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 40 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.000 ft
8. TOWER RATING: 104.8%



Section	Size	Length (ft)	Grade	Weight (K)
1	P24x3/8	34.300	A36	3.2
2	P24x3/8 [0.677164]	5.700	45.379688ksi	0.9
3	P36x1/2	33.580	A36	6.4
4	P42x1/2 P36x1/2 [0.759201]	6.420	44.3375ksi	1.8
5	P42x1/2 P36x1/2 [0.732342]	13.750	A36	3.1
6	P42x1/2 [0.914993]	8.250	43.146429ksi	2.7
7	P42x1/2 [0.914993]	18.000	43.146429ksi	7.4
8	P48x5/8	13.750	A36	4.4
9	P48x5/8 [0.826841]	13.580	34.039003ksi	5.8
10	P48x5/8 [0.98398]	12.670	43.816406ksi	6.4
11	P48x5/8 [0.952023]	8.750	33.7356ksi	3.1
12	P54x5/8 [0.952023]	2.250	33.7356ksi	1.0
13	P54x5/8 [0.952023]	9.000	33.7356ksi	4.6
				50.8

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Job: **86959.008.01 - PORTLAND WARREN AVE, ME (BU# 87878)**  
Project:  
Client: Crown Castle  
Code: TIA-222-G  
Path:  
Drawn by: T. Baidur  
Date: 05/21/16  
App'd:  
Scale: NTS  
Dwg No: E-1



Vx

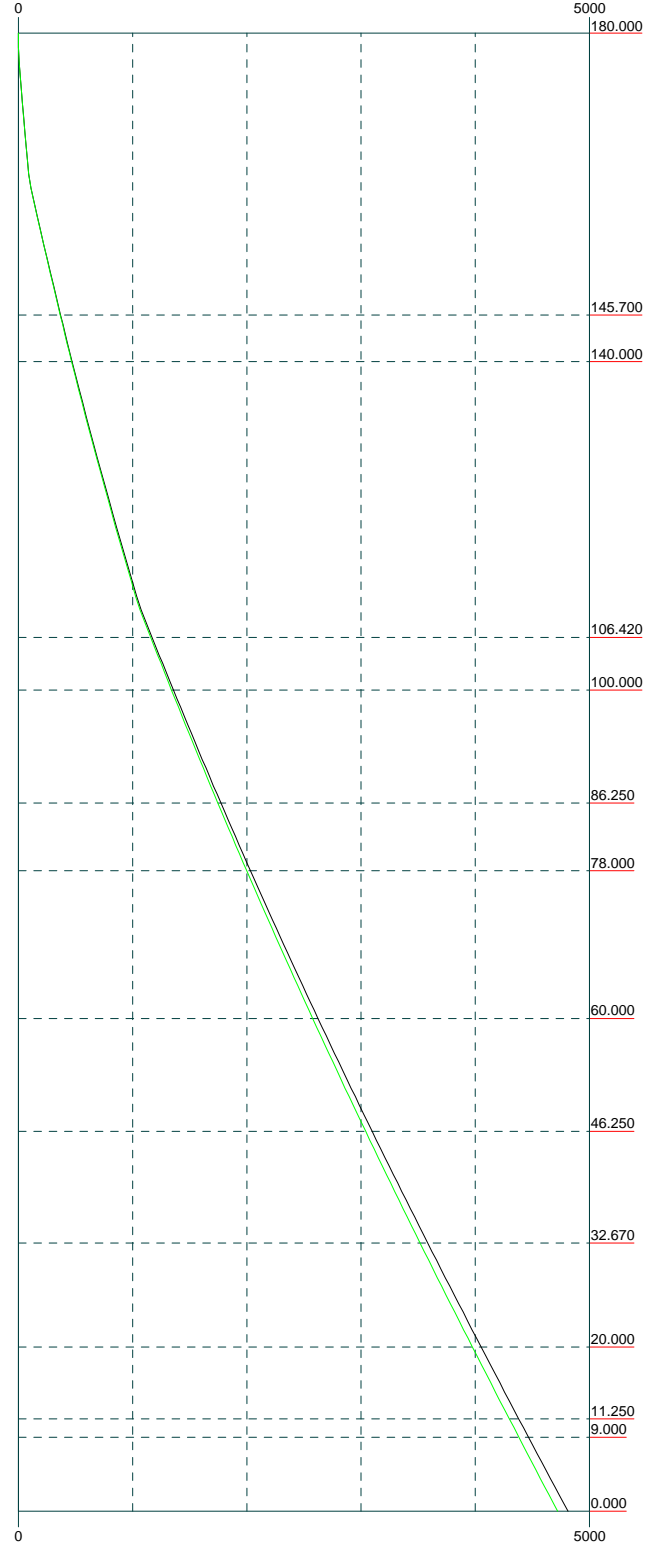
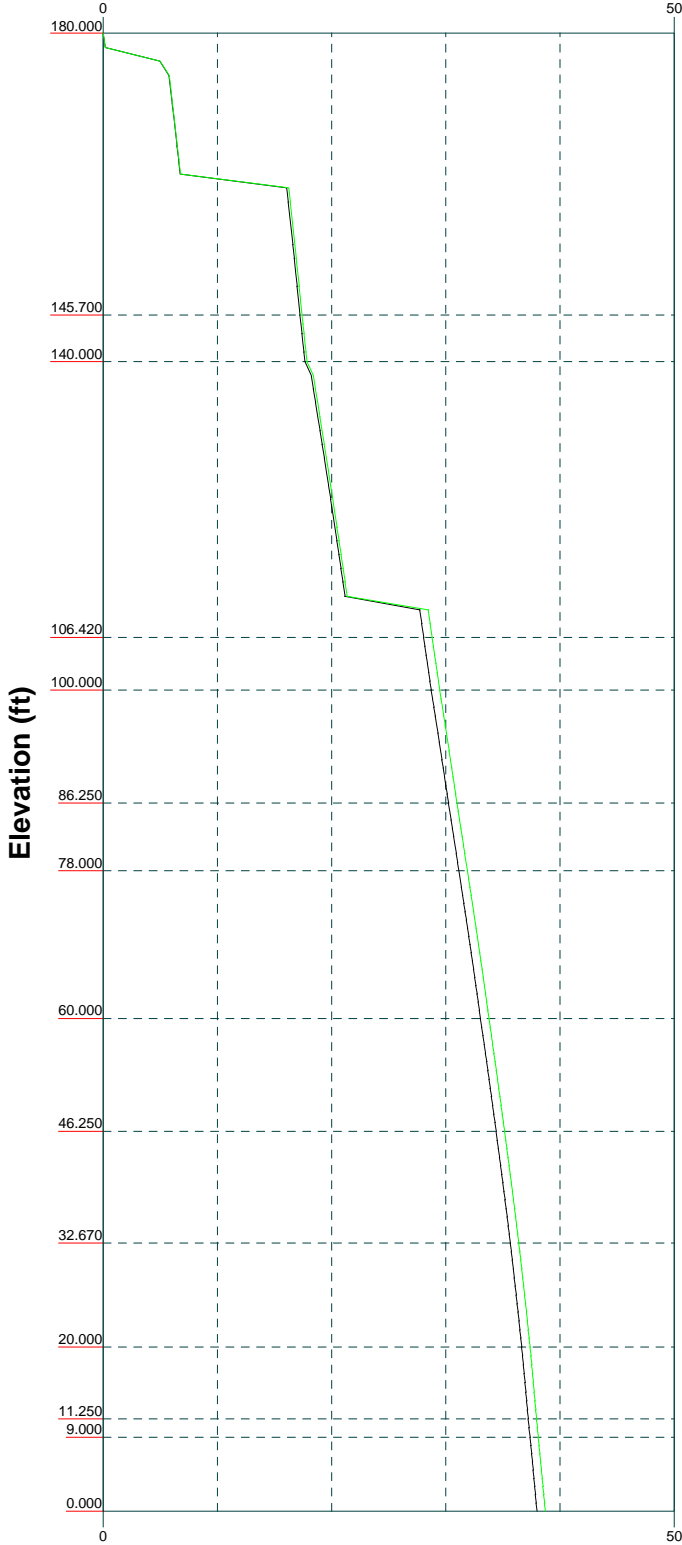
Vz

Mx

Mz

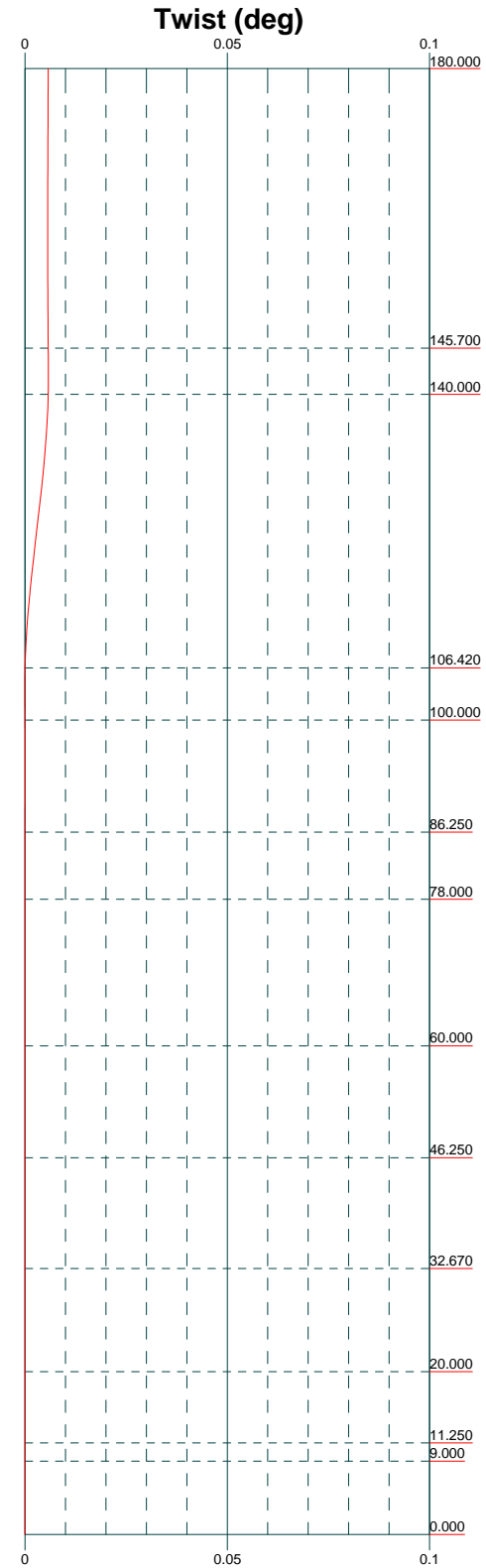
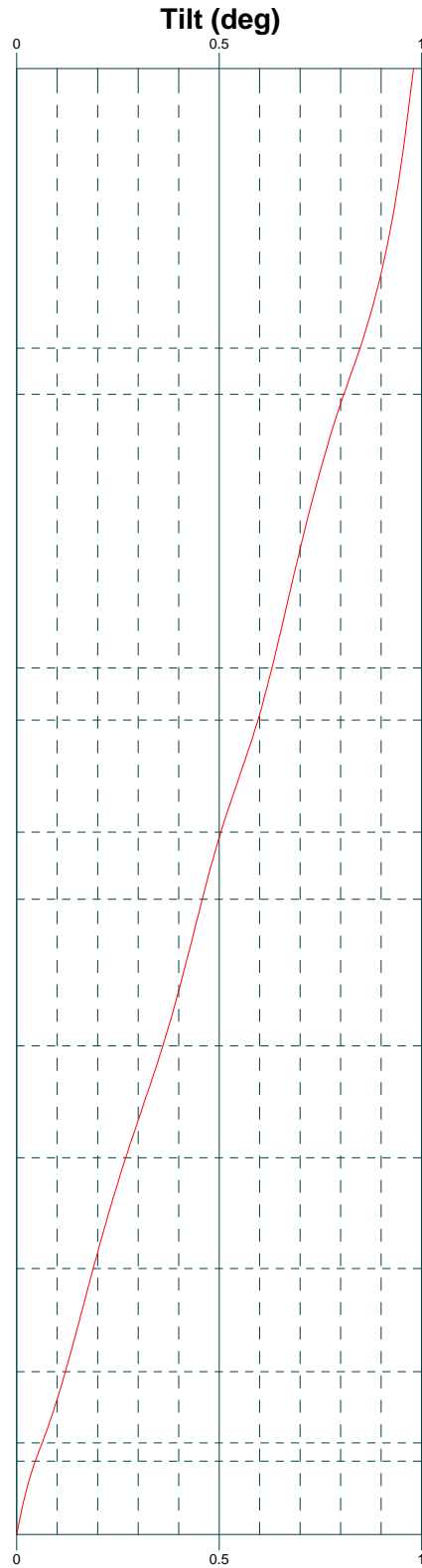
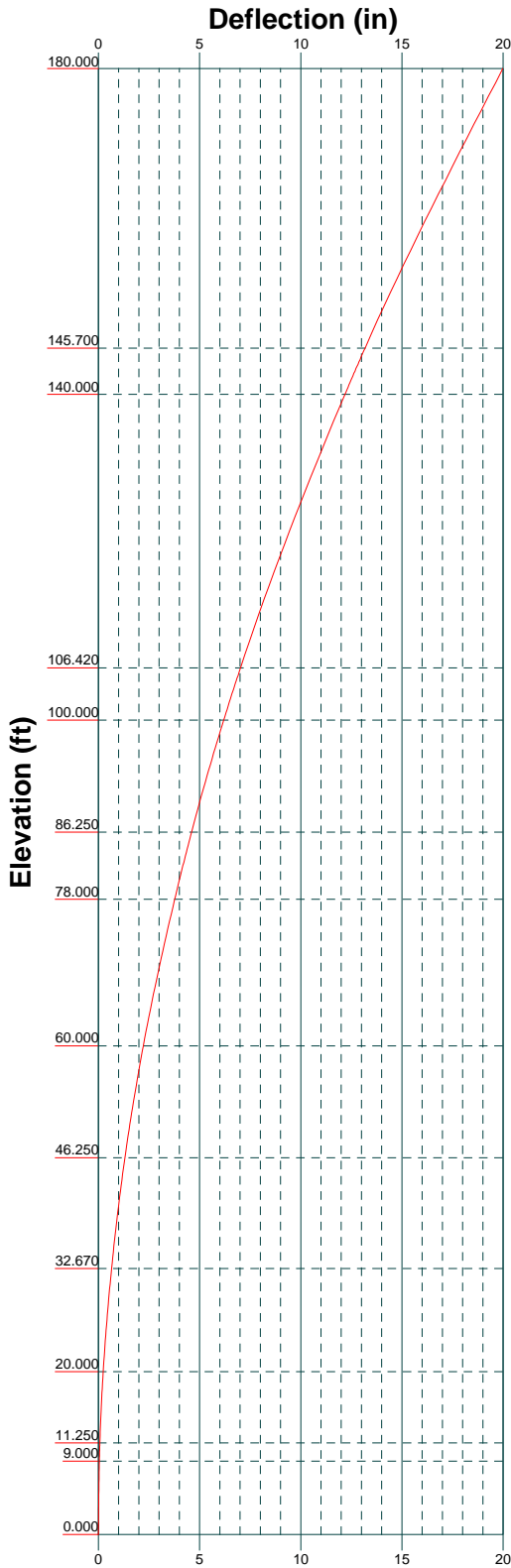
Global Mast Shear (K)

Global Mast Moment (kip-ft)



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Job: <b>86959.008.01 - PORTLAND WARREN AVE, ME (BU# 87878)</b>		
Project:		
Client: Crown Castle	Drawn by: T. Baidur	App'd:
Code: TIA-222-G	Date: 05/21/16	Scale: NTS
Path:	Dwg No: E-4	



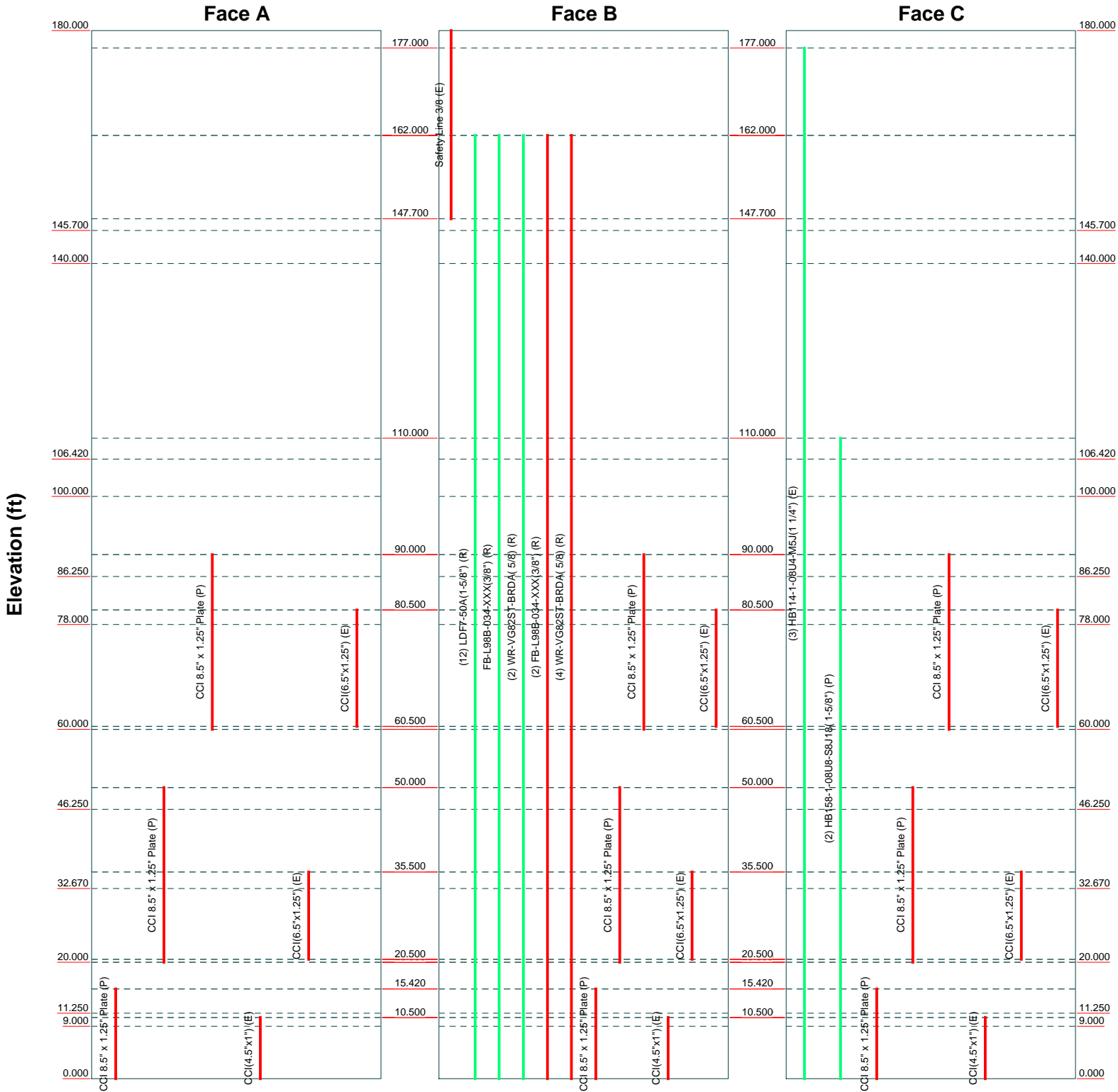
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Job: <b>86959.008.01 - PORTLAND WARREN AVE, ME (BU# 87878)</b>		
Project:		
Client: Crown Castle	Drawn by: T. Baidur	App'd:
Code: TIA-222-G	Date: 05/21/16	Scale: NTS
Path:	Dwg No: E-5	

# Feed Line Distribution Chart

## 0' - 180'

— Round   
 — Flat   
 — App In Face   
 — App Out Face   
 — Truss Leg




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Job: <b>86959.008.01 - PORTLAND WARREN AVE, ME (BU# 87878)</b>		
Project:		
Client: Crown Castle	Drawn by: T. Baidur	App'd:
Code: TIA-222-G	Date: 05/21/16	Scale: NTS
Path:		Dwg No: E-7

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 86959.008.01 - PORTLAND WARREN AVE, ME (BU# 878782)	<b>Page</b> 1 of 21
	<b>Project</b>	<b>Date</b> 16:56:16 05/21/16
	<b>Client</b> Crown Castle	<b>Designed by</b> T. Baidur

## Tower Input Data

There is a pole section.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

- Tower is located in Cumberland County, Maine.
- Basic wind speed of 100 mph.
- Structure Class II.
- Exposure Category C.
- Topographic Category 1.
- Crest Height 0.000 ft.
- Nominal ice thickness of 1.000 in.
- Ice thickness is considered to increase with height.
- Ice density of 56.000 pcf.
- A wind speed of 40 mph is used in combination with ice.
- Temperature drop of 50.000 °F.
- Deflections calculated using a wind speed of 60 mph.
- TOWER RATING: 104.8%.
- A non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- Stress ratio used in pole design is 1.
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

- |  |  |  |
|--|--|--|
| <ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>√ Use Code Safety Factors - Guys</li> <li>Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <li>Include Bolts In Member Capacity</li> <li>Leg Bolts Are At Top Of Section</li> <li>Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sided)</li> <li>SR Members Have Cut Ends</li> <li>SR Members Are Concentric</li> </ul> | <ul style="list-style-type: none"> <li>Distribute Leg Loads As Uniform</li> <li>Assume Legs Pinned</li> <li>√ Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>Use Clear Spans For KL/r</li> <li>Retention Guys To Initial Tension</li> <li>√ Bypass Mast Stability Checks</li> <li>√ Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurt.</li> <li>Autocalc Torque Arm Areas</li> <li>Add IBC .6D+W Combination</li> <li>Sort Capacity Reports By Component</li> <li>Triangulate Diamond Inner Bracing</li> <li>Treat Feed Line Bundles As Cylinder</li> </ul> | <ul style="list-style-type: none"> <li>Use ASCE 10 X-Brace Ly Rules</li> <li>Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feed Line Torque</li> <li>Include Angle Block Shear Check</li> <li>Use TIA-222-G Bracing Resist. Exemption</li> <li>Use TIA-222-G Tension Splice Exemption</li> <li style="background-color: #e0e0e0;">Poles</li> <li>√ Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> </ul> |
|--|--|--|

## Pole Section Geometry

Section	Elevation <i>ft</i>	Section Length <i>ft</i>	Pole Size	Pole Grade	Socket Length <i>ft</i>
L1	180.000-145.700	34.300	P24x3/8	A36 (36 ksi)	
L2	145.700-140.000	5.700	P24x3/8	45.379688ksi	

<p><b>tnxTower</b></p> <p><b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265</p>	<p><b>Job</b> 86959.008.01 - PORTLAND WARREN AVE, ME (BU# 878782)</p>	<p><b>Page</b> 2 of 21</p>
	<p><b>Project</b></p>	<p><b>Date</b> 16:56:16 05/21/16</p>
	<p><b>Client</b> Crown Castle</p>	<p><b>Designed by</b> T. Baidur</p>

Section	Elevation ft	Section Length ft	Pole Size	Pole Grade	Socket Length ft
L3	140.000-106.420	33.580	[0.677164] P36x1/2	(45 ksi) A36	
L4	106.420-100.000	6.420	P36x1/2	44.3375ksi (36 ksi)	
L5	100.000-86.250	13.750	[0.759201] P42x1/2	(44 ksi) A36	
L6	86.250-78.000	8.250	P42x1/2	43.146429ksi (43 ksi)	
L7	78.000-60.000	18.000	P42x1/2	43.146429ksi (43 ksi)	
L8	60.000-46.250	13.750	[0.914993] P48x5/8	(43 ksi) A36	
L9	46.250-32.670	13.580	P48x5/8	34.039003ksi (36 ksi)	
L10	32.670-20.000	12.670	[0.826841] P48x5/8	(34 ksi) 43.816406ksi	
L11	20.000-11.250	8.750	[0.983981] P54x5/8	(44 ksi) A36	
L12	11.250-9.000	2.250	P54x5/8	34.497269ksi (36 ksi)	
L13	9.000-0.000	9.000	[0.793292] P54x5/8	(34 ksi) 33.7356ksi	
			[0.884318]	(34 ksi)	

Tower Elevation ft	Gusset Area (per face) ft <sup>2</sup>	Gusset Thickness in	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
L1 180.000-145.700				1	1	1			
L2 145.700-140.000				1	1	0.924207			
L3 140.000-106.420				1	1	1			
L4 106.420-100.000				1	1	0.953911			
L5 100.000-86.250				1	1	1			
L6 86.250-78.000				1	1	1.02282			
L7 78.000-60.000				1	1	1.02878			
L8 60.000-46.250				1	1	1			
L9 46.250-32.670				1	1	1.01977			
L10 32.670-20.000				1	1	1.02757			
L11 20.000-11.250				1	1	1			
L12 11.250-9.000				1	1	1.03125			

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor $A_f$	Adjust. Factor $A_r$	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
ft	ft <sup>2</sup>	in							
L13 9.000-0.000				1	1	1.01822			

**Feed Line/Linear Appurtenances - Entered As Round Or Flat**

Description	Sector	Component Type	Placement	Total Number	Number Per Row	Start/End Position	Width or Diameter in	Perimeter in	Weight klf
			ft						
***** Safety Line 3/8 (E) *****	B	Surface Ar (CaAa)	180.000 - 147.700	1	1	0.000 0.000	0.375		0.000
FB-L98B-034-XXX(3/8") (R)	B	Surface Ar (CaAa)	162.000 - 0.000	2	1	-0.300 -0.250	0.394		0.000
WR-VG82ST-BRDA( 5/8) (R) *//*/	B	Surface Ar (CaAa)	162.000 - 0.000	4	1	-0.230 -0.210	0.645		0.000
CCI 8.5" x 1.25" Plate (P)	A	Surface Af (CaAa)	15.420 - 0.000	1	1	0.000 0.000	8.500	19.500	0.000
CCI 8.5" x 1.25" Plate (P)	B	Surface Af (CaAa)	15.420 - 0.000	1	1	0.000 0.000	8.500	19.500	0.000
CCI 8.5" x 1.25" Plate (P)	C	Surface Af (CaAa)	15.420 - 0.000	1	1	0.000 0.000	8.500	19.500	0.000
* CCI 8.5" x 1.25" Plate (P)	A	Surface Af (CaAa)	50.000 - 20.000	1	1	0.000 0.000	8.500	19.500	0.000
CCI 8.5" x 1.25" Plate (P)	B	Surface Af (CaAa)	50.000 - 20.000	1	1	0.000 0.000	8.500	19.500	0.000
CCI 8.5" x 1.25" Plate (P)	C	Surface Af (CaAa)	50.000 - 20.000	1	1	0.000 0.000	8.500	19.500	0.000
* CCI 8.5" x 1.25" Plate (P)	A	Surface Af (CaAa)	90.000 - 60.000	1	1	0.000 0.000	8.500	19.500	0.000
CCI 8.5" x 1.25" Plate (P)	B	Surface Af (CaAa)	90.000 - 60.000	1	1	0.000 0.000	8.500	19.500	0.000
CCI 8.5" x 1.25" Plate (P)	C	Surface Af (CaAa)	90.000 - 60.000	1	1	0.000 0.000	8.500	19.500	0.000
* CCI(4.5"x1") (E)	A	Surface Af (CaAa)	10.500 - 0.000	1	1	0.000 0.000	4.500	11.000	0.000
CCI(4.5"x1") (E)	B	Surface Af (CaAa)	10.500 - 0.000	1	1	0.000 0.000	4.500	11.000	0.000
CCI(4.5"x1") (E)	C	Surface Af (CaAa)	10.500 - 0.000	1	1	0.000 0.000	4.500	11.000	0.000
* CCI(6.5"x1.25") (E)	A	Surface Af (CaAa)	35.500 - 20.500	1	1	0.000 0.000	6.500	15.500	0.000
CCI(6.5"x1.25") (E)	B	Surface Af (CaAa)	35.500 - 20.500	1	1	0.000 0.000	6.500	15.500	0.000
CCI(6.5"x1.25") (E)	C	Surface Af (CaAa)	35.500 - 20.500	1	1	0.000 0.000	6.500	15.500	0.000
* CCI(6.5"x1.25") (E)	A	Surface Af (CaAa)	80.500 - 60.500	1	1	0.000 0.000	6.500	15.500	0.000
CCI(6.5"x1.25") (E)	B	Surface Af (CaAa)	80.500 - 60.500	1	1	0.000 0.000	6.500	15.500	0.000

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	<b>Client</b> Crown Castle	<b>Designed by</b> T. Baidur

Description	Sector	Component Type	Placement ft	Total Number	Number Per Row	Start/End Position	Width or Diameter in	Perimeter in	Weight klf
(E) CCI(6.5"x1.25") (E)	C	(CaAa) Surface Af (CaAa)	80.500 - 60.500	1	1	0.000 0.000 0.000	6.500	15.500	0.000

### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number		C <sub>AA</sub> ft <sup>2</sup> /ft	Weight klf
HB114-1-08U4-M5J(1 1/4") (E) ***** ***** ***** ***** ***** ***	C	No	Inside Pole	177.000 - 0.000	3	No Ice 1/2" Ice 1" Ice	0.000 0.000 0.000	0.001 0.001 0.001
LDF7-50A(1-5/8") (R)	B	No	Inside Pole	162.000 - 0.000	12	No Ice 1/2" Ice 1" Ice	0.000 0.000 0.000	0.001 0.001 0.001
FB-L98B-034-XXX(3/8" ) (R)	B	No	Inside Pole	162.000 - 0.000	1	No Ice 1/2" Ice 1" Ice	0.000 0.000 0.000	0.000 0.000 0.000
WR-VG82ST-BRDA( 5/8) (R) *//*/	B	No	Inside Pole	162.000 - 0.000	2	No Ice 1/2" Ice 1" Ice	0.000 0.000 0.000	0.000 0.000 0.000
HB158-1-08U8-S8J18( 1-5/8") (P)	C	No	Inside Pole	110.000 - 0.000	2	No Ice 1/2" Ice 1" Ice	0.000 0.000 0.000	0.001 0.001 0.001

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
L1	180.000-145.700	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	2.904	0.000	0.200
		C	0.000	0.000	0.000	0.000	0.101
L2	145.700-140.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.592	0.000	0.068
		C	0.000	0.000	0.000	0.000	0.018
L3	140.000-106.420	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	3.488	0.000	0.398
		C	0.000	0.000	0.000	0.000	0.118
L4	106.420-100.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.667	0.000	0.076
		C	0.000	0.000	0.000	0.000	0.037
L5	100.000-86.250	A	0.000	0.000	5.313	0.000	0.000
		B	0.000	0.000	6.741	0.000	0.163
		C	0.000	0.000	5.313	0.000	0.080
L6	86.250-78.000	A	0.000	0.000	14.396	0.000	0.000
		B	0.000	0.000	15.253	0.000	0.098
		C	0.000	0.000	14.396	0.000	0.048

Tower Section	Tower Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
L7	78.000-60.000	A	0.000	0.000	44.458	0.000	0.000
		B	0.000	0.000	46.328	0.000	0.213
		C	0.000	0.000	44.458	0.000	0.105
L8	60.000-46.250	A	0.000	0.000	5.313	0.000	0.000
		B	0.000	0.000	6.741	0.000	0.163
		C	0.000	0.000	5.313	0.000	0.080
L9	46.250-32.670	A	0.000	0.000	22.304	0.000	0.000
		B	0.000	0.000	23.715	0.000	0.161
		C	0.000	0.000	22.304	0.000	0.079
L10	32.670-20.000	A	0.000	0.000	31.133	0.000	0.000
		B	0.000	0.000	32.449	0.000	0.150
		C	0.000	0.000	31.133	0.000	0.074
L11	20.000-11.250	A	0.000	0.000	5.907	0.000	0.000
		B	0.000	0.000	6.816	0.000	0.104
		C	0.000	0.000	5.907	0.000	0.051
L12	11.250-9.000	A	0.000	0.000	4.313	0.000	0.000
		B	0.000	0.000	4.546	0.000	0.027
		C	0.000	0.000	4.313	0.000	0.013
L13	9.000-0.000	A	0.000	0.000	19.500	0.000	0.000
		B	0.000	0.000	20.435	0.000	0.107
		C	0.000	0.000	19.500	0.000	0.053

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
L1	180.000-145.700	A	2.346	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	33.359	0.000	1.267
		C		0.000	0.000	0.000	0.000	0.101
L2	145.700-140.000	A	2.316	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	5.872	0.000	0.346
		C		0.000	0.000	0.000	0.000	0.018
L3	140.000-106.420	A	2.282	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	34.138	0.000	1.995
		C		0.000	0.000	0.000	0.000	0.118
L4	106.420-100.000	A	2.242	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	6.423	0.000	0.372
		C		0.000	0.000	0.000	0.000	0.037
L5	100.000-86.250	A	2.219	0.000	0.000	6.976	0.000	0.090
		B		0.000	0.000	20.607	0.000	0.875
		C		0.000	0.000	6.976	0.000	0.171
L6	86.250-78.000	A	2.191	0.000	0.000	19.055	0.000	0.246
		B		0.000	0.000	27.142	0.000	0.708
		C		0.000	0.000	19.055	0.000	0.294
L7	78.000-60.000	A	2.153	0.000	0.000	59.412	0.000	0.763
		B		0.000	0.000	76.783	0.000	1.748
		C		0.000	0.000	59.412	0.000	0.868
L8	60.000-46.250	A	2.098	0.000	0.000	6.886	0.000	0.084
		B		0.000	0.000	19.850	0.000	0.809
		C		0.000	0.000	6.886	0.000	0.164
L9	46.250-32.670	A	2.036	0.000	0.000	28.560	0.000	0.345
		B		0.000	0.000	41.031	0.000	1.032
		C		0.000	0.000	28.560	0.000	0.424
L10	32.670-20.000	A	1.955	0.000	0.000	39.114	0.000	0.471
		B		0.000	0.000	50.340	0.000	1.078
		C		0.000	0.000	39.114	0.000	0.545
L11	20.000-11.250	A	1.856	0.000	0.000	6.403	0.000	0.080



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Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
L12	11.250-9.000	B		0.000	0.000	13.807	0.000	0.471
		C		0.000	0.000	6.403	0.000	0.131
		A	1.777	0.000	0.000	4.888	0.000	0.059
L13	9.000-0.000	B		0.000	0.000	6.721	0.000	0.154
		C		0.000	0.000	4.888	0.000	0.072
		A	1.639	0.000	0.000	22.205	0.000	0.246
		B		0.000	0.000	29.039	0.000	0.591
		C		0.000	0.000	22.205	0.000	0.299

### Feed Line Center of Pressure

Section	Elevation ft	CP <sub>x</sub> in	CP <sub>z</sub> in	CP <sub>x</sub> Ice in	CP <sub>z</sub> Ice in
L1	180.000-145.700	0.087	-0.095	0.629	-0.647
L2	145.700-140.000	0.088	-0.145	0.521	-0.882
L3	140.000-106.420	0.086	-0.141	0.575	-0.975
L4	106.420-100.000	0.086	-0.141	0.569	-0.965
L5	100.000-86.250	0.064	-0.106	0.445	-0.755
L6	86.250-78.000	0.035	-0.057	0.239	-0.405
L7	78.000-60.000	0.028	-0.046	0.188	-0.319
L8	60.000-46.250	0.066	-0.109	0.450	-0.764
L9	46.250-32.670	0.038	-0.063	0.258	-0.437
L10	32.670-20.000	0.030	-0.050	0.199	-0.337
L11	20.000-11.250	0.058	-0.096	0.391	-0.663
L12	11.250-9.000	0.037	-0.062	0.243	-0.413
L13	9.000-0.000	0.035	-0.058	0.213	-0.361

### Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>a</sub> No Ice	K <sub>a</sub> Ice
L1	13	Safety Line 3/8	147.70 - 180.00	1.0000	1.0000
L1	26	FB-L98B-034-XXX(3/8")	145.70 - 162.00	1.0000	1.0000
L1	27	WR-VG82ST-BRDA( 5/8)	145.70 - 162.00	1.0000	1.0000
L2	26	FB-L98B-034-XXX(3/8")	140.00 - 145.70	1.0000	1.0000
L2	27	WR-VG82ST-BRDA( 5/8)	140.00 - 145.70	1.0000	1.0000
L3	26	FB-L98B-034-XXX(3/8")	106.42 - 140.00	1.0000	1.0000
L3	27	WR-VG82ST-BRDA( 5/8)	106.42 - 140.00	1.0000	1.0000
L4	26	FB-L98B-034-XXX(3/8")	100.00 - 106.42	1.0000	1.0000
L4	27	WR-VG82ST-BRDA( 5/8)	100.00 - 106.42	1.0000	1.0000
L5	26	FB-L98B-034-XXX(3/8")	86.25 - 100.00	1.0000	1.0000

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>a</sub> No Ice	K <sub>a</sub> Ice
L5	27	WR-VG82ST-BRDA( 5/8)	86.25 - 100.00	1.0000	1.0000
L5	39	CCI 8.5" x 1.25" Plate	86.25 - 90.00	1.0000	1.0000
L5	40	CCI 8.5" x 1.25" Plate	86.25 - 90.00	1.0000	1.0000
L5	41	CCI 8.5" x 1.25" Plate	86.25 - 90.00	1.0000	1.0000
L6	26	FB-L98B-034-XXX(3/8")	78.00 - 86.25	1.0000	1.0000
L6	27	WR-VG82ST-BRDA( 5/8)	78.00 - 86.25	1.0000	1.0000
L6	39	CCI 8.5" x 1.25" Plate	78.00 - 86.25	1.0000	1.0000
L6	40	CCI 8.5" x 1.25" Plate	78.00 - 86.25	1.0000	1.0000
L6	41	CCI 8.5" x 1.25" Plate	78.00 - 86.25	1.0000	1.0000
L6	51	CCI(6.5"x1.25")	78.00 - 80.50	1.0000	1.0000
L6	52	CCI(6.5"x1.25")	78.00 - 80.50	□	1.0000
L6	53	CCI(6.5"x1.25")	78.00 - 80.50	1.0000	1.0000
L7	26	FB-L98B-034-XXX(3/8")	60.00 - 78.00	1.0000	1.0000
L7	27	WR-VG82ST-BRDA( 5/8)	60.00 - 78.00	1.0000	1.0000
L7	39	CCI 8.5" x 1.25" Plate	60.00 - 78.00	1.0000	1.0000
L7	40	CCI 8.5" x 1.25" Plate	60.00 - 78.00	1.0000	1.0000
L7	41	CCI 8.5" x 1.25" Plate	60.00 - 78.00	1.0000	1.0000
L7	51	CCI(6.5"x1.25")	60.50 - 78.00	1.0000	1.0000
L7	52	CCI(6.5"x1.25")	60.50 - 78.00	1.0000	1.0000
L7	53	CCI(6.5"x1.25")	60.50 - 78.00	1.0000	1.0000
L8	26	FB-L98B-034-XXX(3/8")	46.25 - 60.00	1.0000	1.0000
L8	27	WR-VG82ST-BRDA( 5/8)	46.25 - 60.00	1.0000	1.0000
L8	35	CCI 8.5" x 1.25" Plate	46.25 - 50.00	1.0000	1.0000
L8	36	CCI 8.5" x 1.25" Plate	46.25 - 50.00	1.0000	1.0000
L8	37	CCI 8.5" x 1.25" Plate	46.25 - 50.00	1.0000	1.0000
L9	26	FB-L98B-034-XXX(3/8")	32.67 - 46.25	1.0000	1.0000
L9	27	WR-VG82ST-BRDA( 5/8)	32.67 - 46.25	1.0000	1.0000
L9	35	CCI 8.5" x 1.25" Plate	32.67 - 46.25	1.0000	1.0000
L9	36	CCI 8.5" x 1.25" Plate	32.67 - 46.25	1.0000	1.0000
L9	37	CCI 8.5" x 1.25" Plate	32.67 - 46.25	1.0000	1.0000
L9	47	CCI(6.5"x1.25")	32.67 - 35.50	1.0000	1.0000
L9	48	CCI(6.5"x1.25")	32.67 - 35.50	1.0000	1.0000
L9	49	CCI(6.5"x1.25")	32.67 - 35.50	1.0000	1.0000
L10	26	FB-L98B-034-XXX(3/8")	20.00 - 32.67	1.0000	1.0000
L10	27	WR-VG82ST-BRDA( 5/8)	20.00 - 32.67	1.0000	1.0000
L10	35	CCI 8.5" x 1.25" Plate	20.00 - 32.67	1.0000	1.0000
L10	36	CCI 8.5" x 1.25" Plate	20.00 - 32.67	1.0000	1.0000
L10	37	CCI 8.5" x 1.25" Plate	20.00 - 32.67	1.0000	1.0000
L10	47	CCI(6.5"x1.25")	20.50 - 32.67	1.0000	1.0000
L10	48	CCI(6.5"x1.25")	20.50 - 32.67	1.0000	1.0000
L10	49	CCI(6.5"x1.25")	20.50 - 32.67	1.0000	1.0000
L11	26	FB-L98B-034-XXX(3/8")	11.25 - 20.00	1.0000	1.0000
L11	27	WR-VG82ST-BRDA( 5/8)	11.25 - 20.00	1.0000	1.0000
L11	31	CCI 8.5" x 1.25" Plate	11.25 - 15.42	1.0000	1.0000
L11	32	CCI 8.5" x 1.25" Plate	11.25 - 15.42	1.0000	1.0000
L11	33	CCI 8.5" x 1.25" Plate	11.25 - 15.42	1.0000	1.0000
L12	26	FB-L98B-034-XXX(3/8")	9.00 - 11.25	1.0000	1.0000
L12	27	WR-VG82ST-BRDA( 5/8)	9.00 - 11.25	1.0000	1.0000
L12	31	CCI 8.5" x 1.25" Plate	9.00 - 11.25	1.0000	1.0000
L12	32	CCI 8.5" x 1.25" Plate	9.00 - 11.25	1.0000	1.0000
L12	33	CCI 8.5" x 1.25" Plate	9.00 - 11.25	1.0000	1.0000
L12	43	CCI(4.5"x1")	9.00 - 10.50	1.0000	1.0000
L12	44	CCI(4.5"x1")	9.00 - 10.50	1.0000	1.0000
L12	45	CCI(4.5"x1")	9.00 - 10.50	1.0000	1.0000
L13	26	FB-L98B-034-XXX(3/8")	0.00 - 9.00	1.0000	1.0000
L13	27	WR-VG82ST-BRDA( 5/8)	0.00 - 9.00	1.0000	1.0000
L13	31	CCI 8.5" x 1.25" Plate	0.00 - 9.00	1.0000	1.0000
L13	32	CCI 8.5" x 1.25" Plate	0.00 - 9.00	1.0000	1.0000
L13	33	CCI 8.5" x 1.25" Plate	0.00 - 9.00	1.0000	1.0000
L13	43	CCI(4.5"x1")	0.00 - 9.00	1.0000	1.0000
L13	44	CCI(4.5"x1")	0.00 - 9.00	1.0000	1.0000
L13	45	CCI(4.5"x1")	0.00 - 9.00	1.0000	1.0000

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 86959.008.01 - PORTLAND WARREN AVE, ME (BU# 878782)	<b>Page</b> 8 of 21
	<b>Project</b>	<b>Date</b> 16:56:16 05/21/16
	<b>Client</b> Crown Castle	<b>Designed by</b> T. Baidur

## Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Horz Lateral	Vert					
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
Lighting Rod 5/8" x 8' (E)	C	None			0.000	184.000	No Ice 0.500 1/2" Ice 1.314 1" Ice 2.144	0.500 1.314 2.144	0.031 0.037 0.047
*****									
APXVSP18-C-A20 w/ Mount Pipe (E)	A	From Leg	4.000 0.000 2.000		0.000	177.000	No Ice 8.262 1/2" Ice 8.822 1" Ice 9.346	6.946 8.127 9.021	0.083 0.151 0.227
APXV9ERR18-C-A20 w/ Mount Pipe (E)	B	From Leg	4.000 0.000 2.000		0.000	177.000	No Ice 8.262 1/2" Ice 8.822 1" Ice 9.346	7.471 8.656 9.556	0.088 0.158 0.237
APXVSP18-C-A20 w/ Mount Pipe (E)	C	From Leg	4.000 0.000 2.000		0.000	177.000	No Ice 8.262 1/2" Ice 8.822 1" Ice 9.346	6.946 8.127 9.021	0.083 0.151 0.227
IBC1900BB-1 (E)	A	From Leg	4.000 0.000 2.000		0.000	177.000	No Ice 0.966 1/2" Ice 1.091 1" Ice 1.223	0.463 0.558 0.660	0.022 0.030 0.039
IBC1900BB-1 (E)	B	From Leg	4.000 0.000 2.000		0.000	177.000	No Ice 0.966 1/2" Ice 1.091 1" Ice 1.223	0.463 0.558 0.660	0.022 0.030 0.039
IBC1900BB-1 (E)	C	From Leg	4.000 0.000 2.000		0.000	177.000	No Ice 0.966 1/2" Ice 1.091 1" Ice 1.223	0.463 0.558 0.660	0.022 0.030 0.039
IBC1900HG-2A (E)	A	From Leg	4.000 0.000 2.000		0.000	177.000	No Ice 0.966 1/2" Ice 1.091 1" Ice 1.223	0.463 0.558 0.660	0.022 0.030 0.039
IBC1900HG-2A (E)	B	From Leg	4.000 0.000 2.000		0.000	177.000	No Ice 0.966 1/2" Ice 1.091 1" Ice 1.223	0.463 0.558 0.660	0.022 0.030 0.039
IBC1900HG-2A (E)	C	From Leg	4.000 0.000 2.000		0.000	177.000	No Ice 0.966 1/2" Ice 1.091 1" Ice 1.223	0.463 0.558 0.660	0.022 0.030 0.039
(3) 3' x 2" Pipe Mount (E)	A	From Leg	4.000 0.000 0.000		0.000	177.000	No Ice 0.583 1/2" Ice 0.770 1" Ice 0.967	0.583 0.770 0.967	0.011 0.017 0.024
(3) 3' x 2" Pipe Mount (E)	B	From Leg	4.000 0.000 0.000		0.000	177.000	No Ice 0.583 1/2" Ice 0.770 1" Ice 0.967	0.583 0.770 0.967	0.011 0.017 0.024
(3) 3' x 2" Pipe Mount (E)	C	From Leg	4.000 0.000 0.000		0.000	177.000	No Ice 0.583 1/2" Ice 0.770 1" Ice 0.967	0.583 0.770 0.967	0.011 0.017 0.024
Platform Mount [LP 715-1] (E)	C	None			0.000	177.000	No Ice 44.210 1/2" Ice 53.970 1" Ice 63.730	44.210 53.970 63.730	1.775 2.323 2.871
*****									
PCS 1900MHz 4x45W-65MHz (E)	A	From Leg	1.000 0.000 1.000		0.000	175.000	No Ice 2.322 1/2" Ice 2.527 1" Ice 2.739	2.238 2.441 2.651	0.060 0.083 0.110

# tnxTower

**B+T Group**  
 1717 S. Boulder, Suite 300  
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**Job**  
 86959.008.01 - PORTLAND WARREN AVE, ME (BU# 878782)

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**Project**

**Date**  
 16:56:16 05/21/16

**Client**  
 Crown Castle

**Designed by**  
 T. Baidur

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	CAAA Front ft <sup>2</sup>	CAAA Side ft <sup>2</sup>	Weight K
PCS 1900MHz	B	From Leg	1.000	0.000	175.000	No Ice 2.322	2.238	0.060
4x45W-65MHz (E)			0.000			1/2" Ice 2.527	2.441	0.083
			1.000			1" Ice 2.739	2.651	0.110
PCS 1900MHz	C	From Leg	1.000	0.000	175.000	No Ice 2.322	2.238	0.060
4x45W-65MHz (E)			0.000			1/2" Ice 2.527	2.441	0.083
			1.000			1" Ice 2.739	2.651	0.110
4' x 2" Pipe Mount (E)	A	From Leg	0.500	0.000	175.000	No Ice 0.785	0.785	0.029
			0.000			1/2" Ice 1.028	1.028	0.035
			0.000			1" Ice 1.281	1.281	0.044
4' x 2" Pipe Mount (E)	B	From Leg	0.500	0.000	175.000	No Ice 0.785	0.785	0.029
			0.000			1/2" Ice 1.028	1.028	0.035
			0.000			1" Ice 1.281	1.281	0.044
4' x 2" Pipe Mount (E)	C	From Leg	0.500	0.000	175.000	No Ice 0.785	0.785	0.029
			0.000			1/2" Ice 1.028	1.028	0.035
			0.000			1" Ice 1.281	1.281	0.044
Side Arm Mount [SO 102-3] (E)	C	None		0.000	175.000	No Ice 3.000	3.000	0.081
						1/2" Ice 3.480	3.480	0.111
						1" Ice 3.960	3.960	0.141
*****								
*****								
7770.00 (E)	A	From Leg	4.000	0.000	162.000	No Ice 5.508	2.928	0.035
			0.000			1/2" Ice 5.867	3.273	0.068
			0.000			1" Ice 6.233	3.625	0.105
7770.00 (E)	B	From Leg	4.000	0.000	162.000	No Ice 5.508	2.928	0.035
			0.000			1/2" Ice 5.867	3.273	0.068
			0.000			1" Ice 6.233	3.625	0.105
7770.00 (E)	C	From Leg	4.000	0.000	162.000	No Ice 5.508	2.928	0.035
			0.000			1/2" Ice 5.867	3.273	0.068
			0.000			1" Ice 6.233	3.625	0.105
P65-17-XLH-RR (E)	A	From Leg	4.000	0.000	162.000	No Ice 11.467	6.800	0.059
			0.000			1/2" Ice 12.083	7.384	0.121
			0.000			1" Ice 12.707	7.976	0.191
AM-X-CD-16-65-00T-RET (E)	B	From Leg	4.000	0.000	162.000	No Ice 8.024	4.642	0.049
			0.000			1/2" Ice 8.480	5.088	0.095
			0.000			1" Ice 8.943	5.542	0.147
AM-X-CD-16-65-00T-RET (E)	C	From Leg	4.000	0.000	162.000	No Ice 8.024	4.642	0.049
			0.000			1/2" Ice 8.480	5.088	0.095
			0.000			1" Ice 8.943	5.542	0.147
7020.00 (E)	A	From Leg	4.000	0.000	162.000	No Ice 0.102	0.175	0.002
			0.000			1/2" Ice 0.147	0.239	0.005
			0.000			1" Ice 0.199	0.311	0.009
7020.00 (E)	B	From Leg	4.000	0.000	162.000	No Ice 0.102	0.175	0.002
			0.000			1/2" Ice 0.147	0.239	0.005
			0.000			1" Ice 0.199	0.311	0.009
7020.00 (E)	C	From Leg	4.000	0.000	162.000	No Ice 0.102	0.175	0.002
			0.000			1/2" Ice 0.147	0.239	0.005
			0.000			1" Ice 0.199	0.311	0.009
(2) RRUS-11 (E)	A	From Leg	4.000	0.000	162.000	No Ice 2.784	1.187	0.048
			0.000			1/2" Ice 2.992	1.334	0.068
			-1.000			1" Ice 3.207	1.490	0.092
(2) RRUS-11 (E)	B	From Leg	4.000	0.000	162.000	No Ice 2.784	1.187	0.048
			0.000			1/2" Ice 2.992	1.334	0.068
			-1.000			1" Ice 3.207	1.490	0.092
(2) RRUS-11 (E)	C	From Leg	4.000	0.000	162.000	No Ice 2.784	1.187	0.048
			0.000			1/2" Ice 2.992	1.334	0.068
			-1.000			1" Ice 3.207	1.490	0.092
DC6-48-60-18-8F	B	From Leg	4.000	0.000	162.000	No Ice 0.917	0.917	0.019

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz	Lateral					
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
(E)			0.000			1/2" Ice	1.458	1.458	0.037
			0.000			1" Ice	1.643	1.643	0.057
HPA-65R-BUU-H8 (R)	A	From Leg	4.000	0.000	162.000	No Ice	12.976	7.516	0.068
			0.000			1/2" Ice	13.558	8.087	0.142
			0.000			1" Ice	14.147	8.666	0.223
HPA-65R-BUU-H6 (R)	B	From Leg	4.000	0.000	162.000	No Ice	9.658	6.450	0.051
			0.000			1/2" Ice	10.128	6.913	0.114
			0.000			1" Ice	10.606	7.384	0.183
HPA-65R-BUU-H6 (R)	C	From Leg	4.000	0.000	162.000	No Ice	9.658	6.450	0.051
			0.000			1/2" Ice	10.128	6.913	0.114
			0.000			1" Ice	10.606	7.384	0.183
OPA-65R-LCUU-H8 (R)	A	From Leg	4.000	0.000	162.000	No Ice	12.746	7.246	0.088
			0.000			1/2" Ice	13.328	7.817	0.159
			0.000			1" Ice	13.916	8.396	0.238
OPA-65R-LCUU-H6 (R)	B	From Leg	4.000	0.000	162.000	No Ice	9.658	5.517	0.073
			0.000			1/2" Ice	10.128	5.971	0.131
			0.000			1" Ice	10.606	6.434	0.196
OPA-65R-LCUU-H6 (R)	C	From Leg	4.000	0.000	162.000	No Ice	9.658	5.517	0.073
			0.000			1/2" Ice	10.128	5.971	0.131
			0.000			1" Ice	10.606	6.434	0.196
TT19-08BP111-001 (R)	A	From Leg	4.000	0.000	162.000	No Ice	0.545	0.442	0.016
			0.000			1/2" Ice	0.641	0.530	0.022
			-1.000			1" Ice	0.743	0.626	0.029
RRUS A2 (R)	A	From Leg	4.000	0.000	162.000	No Ice	2.066	0.498	0.022
			0.000			1/2" Ice	2.245	0.607	0.035
			-1.000			1" Ice	2.431	0.724	0.050
RRUS A2 (R)	B	From Leg	4.000	0.000	162.000	No Ice	2.066	0.498	0.022
			0.000			1/2" Ice	2.245	0.607	0.035
			-1.000			1" Ice	2.431	0.724	0.050
RRUS A2 (R)	C	From Leg	4.000	0.000	162.000	No Ice	2.066	0.498	0.022
			0.000			1/2" Ice	2.245	0.607	0.035
			-1.000			1" Ice	2.431	0.724	0.050
RRUS 11 (R)	A	From Leg	4.000	0.000	162.000	No Ice	2.784	1.187	0.048
			0.000			1/2" Ice	2.992	1.334	0.068
			0.000			1" Ice	3.207	1.490	0.092
RRUS 11 (R)	B	From Leg	4.000	0.000	162.000	No Ice	2.784	1.187	0.048
			0.000			1/2" Ice	2.992	1.334	0.068
			0.000			1" Ice	3.207	1.490	0.092
RRUS 11 (R)	C	From Leg	4.000	0.000	162.000	No Ice	2.784	1.187	0.048
			0.000			1/2" Ice	2.992	1.334	0.068
			0.000			1" Ice	3.207	1.490	0.092
WCS RRUS-32-B30 (R)	A	From Leg	4.000	0.000	162.000	No Ice	3.314	2.424	0.077
			0.000			1/2" Ice	3.558	2.638	0.105
			0.000			1" Ice	3.809	2.860	0.136
WCS RRUS-32-B30 (R)	B	From Leg	4.000	0.000	162.000	No Ice	3.314	2.424	0.077
			0.000			1/2" Ice	3.558	2.638	0.105
			0.000			1" Ice	3.809	2.860	0.136
WCS RRUS-32-B30 (R)	C	From Leg	4.000	0.000	162.000	No Ice	3.314	2.424	0.077
			0.000			1/2" Ice	3.558	2.638	0.105
			0.000			1" Ice	3.809	2.860	0.136
(2) LGP21401 (R)	B	From Leg	4.000	0.000	162.000	No Ice	1.104	0.207	0.014
			0.000			1/2" Ice	1.239	0.274	0.021
			-1.000			1" Ice	1.381	0.348	0.030
(2) LGP21401 (R)	C	From Leg	4.000	0.000	162.000	No Ice	1.104	0.207	0.014
			0.000			1/2" Ice	1.239	0.274	0.021
			-1.000			1" Ice	1.381	0.348	0.030
DC6-48-60-18-8F	B	From Leg	4.000	0.000	162.000	No Ice	0.917	0.917	0.019

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 86959.008.01 - PORTLAND WARREN AVE, ME (BU# 878782)	<b>Page</b> 11 of 21
	<b>Project</b>	<b>Date</b> 16:56:16 05/21/16
	<b>Client</b> Crown Castle	<b>Designed by</b> T. Baidur

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz	Vert					
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
(R)			0.000			1/2" Ice	1.458	1.458	0.037
			0.000			1" Ice	1.643	1.643	0.057
Platform Mount [LP 1301-1] (R-4M.P/Sec)	C	None			0.000	No Ice	51.700	51.700	2.262
						1/2" Ice	62.700	62.700	2.935
						1" Ice	73.700	73.700	3.608
*****									
(4) SBNHH-1D65C (P)	A	From Leg	4.000		0.000	No Ice	11.389	7.656	0.050
			0.000			1/2" Ice	12.005	8.246	0.115
			0.000			1" Ice	12.629	8.843	0.188
(2) SBNHH-1D65C (P)	C	From Leg	4.000		0.000	No Ice	11.389	7.656	0.050
			0.000			1/2" Ice	12.005	8.246	0.115
			0.000			1" Ice	12.629	8.843	0.188
(3) B13 RRH 4X30 (P)	A	From Leg	4.000		0.000	No Ice	2.055	1.320	0.056
			0.000			1/2" Ice	2.241	1.475	0.073
			0.000			1" Ice	2.433	1.638	0.093
(2) DB-B1-6C-12AB-0Z (P)	A	From Leg	4.000		0.000	No Ice	3.364	2.192	0.021
			0.000			1/2" Ice	3.597	2.395	0.050
			0.000			1" Ice	3.838	2.606	0.082
(3) RRH2X60-AWS (P)	C	From Leg	4.000		0.000	No Ice	3.500	1.816	0.060
			0.000			1/2" Ice	3.761	2.052	0.083
			0.000			1" Ice	4.029	2.289	0.109
(3) B25 RRH4X30 (P)	C	From Leg	4.000		0.000	No Ice	2.200	1.742	0.055
			0.000			1/2" Ice	2.393	1.920	0.075
			0.000			1" Ice	2.593	2.106	0.099
Platform Mount [LP 1301-1] (P-4M.P/Sec)	C	None			0.000	No Ice	51.700	51.700	2.262
						1/2" Ice	62.700	62.700	2.935
						1" Ice	73.700	73.700	3.608
*****									
Bridge Stiffener (48"x1.25"x11.5") (E)	A	From Leg	0.000		0.000	No Ice	0.833	4.200	0.000
			0.000			1/2" Ice	1.296	4.574	0.000
			0.000			1" Ice	1.596	4.956	0.000
Bridge Stiffener (48"x1.25"x11.5") (E)	B	From Leg	0.000		0.000	No Ice	0.833	4.200	0.000
			0.000			1/2" Ice	1.296	4.574	0.000
			0.000			1" Ice	1.596	4.956	0.000
Bridge Stiffener (48"x1.25"x11.5") (E)	C	From Leg	0.000		0.000	No Ice	0.833	4.200	0.000
			0.000			1/2" Ice	1.296	4.574	0.000
			0.000			1" Ice	1.596	4.956	0.000
*****									

## Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice

<p><b>tnxTower</b></p> <p><b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587-4630 FAX: (918) 295-0265</p>	<p><b>Job</b> 86959.008.01 - PORTLAND WARREN AVE, ME (BU# 878782)</p>	<p><b>Page</b> 12 of 21</p>
	<p><b>Project</b></p>	<p><b>Date</b> 16:56:16 05/21/16</p>
	<p><b>Client</b> Crown Castle</p>	<p><b>Designed by</b> T. Baidur</p>

<i>Comb. No.</i>	<i>Description</i>
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

### Maximum Member Forces

<i>Section No.</i>	<i>Elevation ft</i>	<i>Component Type</i>	<i>Condition</i>	<i>Gov. Load Comb.</i>	<i>Axial K</i>	<i>Major Axis Moment kip-ft</i>	<i>Minor Axis Moment kip-ft</i>
L1	180 - 145.7	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-30.520	-1.968	1.546
			Max. Mx	8	-10.757	-365.882	0.607
			Max. My	2	-10.725	-0.651	369.044
			Max. Vy	20	-17.232	365.406	-0.384
			Max. Vx	2	-17.412	-0.651	369.044
			Max. Torque	11			1.028
L2	145.7 - 140	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-32.393	-2.133	1.911
			Max. Mx	8	-11.965	-465.317	0.733
			Max. My	2	-11.933	-0.734	469.514

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L3	140 - 106.42	Pole	Max. Vy	20	-17.668	464.835	-0.444
			Max. Vx	2	-17.848	-0.734	469.514
			Max. Torque	11			1.329
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-56.217	6.251	13.441
			Max. Mx	20	-23.690	1158.251	-0.862
			Max. My	2	-23.626	0.032	1169.911
			Max. Vy	20	-28.066	1158.251	-0.862
L4	106.42 - 100	Pole	Max. Vx	2	-28.809	0.032	1169.911
			Max. Torque	18			-8.758
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-59.423	6.018	14.002
			Max. Mx	20	-25.988	1340.497	-2.653
			Max. My	2	-25.927	-1.788	1356.954
			Max. Vy	20	-28.727	1340.497	-2.653
			Max. Vx	2	-29.471	-1.788	1356.954
L5	100 - 86.25	Pole	Max. Torque	18			-8.755
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-65.916	5.431	15.299
			Max. Mx	20	-30.085	1745.867	-6.502
			Max. My	2	-30.032	-5.705	1772.621
			Max. Vy	20	-30.237	1745.867	-6.502
			Max. Vx	2	-30.982	-5.705	1772.621
			Max. Torque	18			-8.753
L6	86.25 - 78	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-71.441	5.080	16.050
			Max. Mx	20	-33.612	1999.033	-8.819
			Max. My	2	-33.562	-8.061	2031.970
			Max. Vy	20	-31.151	1999.033	-8.819
			Max. Vx	2	-31.897	-8.061	2031.970
			Max. Torque	18			-8.748
			Max Tension	1	0.000	0.000	0.000
L7	78 - 60	Pole	Max. Compression	26	-85.905	4.327	17.626
			Max. Mx	20	-43.118	2576.933	-13.892
			Max. My	2	-43.078	-13.217	2623.379
			Max. Vy	20	-33.044	2576.933	-13.892
			Max. Vx	2	-33.791	-13.217	2623.379
			Max. Torque	18			-8.746
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-93.999	3.691	18.874
L8	60 - 46.25	Pole	Max. Mx	20	-48.836	3040.681	-17.769
			Max. My	2	-48.805	-17.163	3097.434
			Max. Vy	20	-34.417	3040.681	-17.769
			Max. Vx	2	-35.160	-17.163	3097.434
			Max. Torque	18			-8.741
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-104.467	3.080	19.957
			Max. Mx	20	-56.253	3516.461	-21.591
L9	46.25 - 32.67	Pole	Max. My	2	-56.231	-21.051	3583.348
			Max. Vy	20	-35.664	3516.461	-21.591
			Max. Vx	2	-36.403	-21.051	3583.348
			Max. Torque	18			-8.737
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-115.845	2.539	20.833
			Max. Mx	20	-64.444	3974.533	-25.145
			Max. My	2	-64.430	-24.666	4050.821
L10	32.67 - 20	Pole	Max. Vy	20	-36.657	3974.533	-25.145
			Max. Vx	2	-37.392	-24.666	4050.821
			Max. Torque	18			-8.735
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-121.411	2.157	21.450
			Max. Mx	20	-64.444	3974.533	-25.145
			Max. My	2	-64.430	-24.666	4050.821
			Max. Vy	20	-36.657	3974.533	-25.145
L11	20 - 11.25	Pole	Max. Vx	2	-37.392	-24.666	4050.821
			Max. Torque	18			-8.735
			Max Tension	1	0.000	0.000	0.000



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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L12	11.25 - 9	Pole	Max. Mx	20	-68.544	4297.674	-27.586
			Max. My	2	-68.536	-27.153	4380.414
			Max. Vy	20	-37.236	4297.674	-27.586
			Max. Vx	2	-37.965	-27.153	4380.414
			Max. Torque	18			-8.733
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-123.233	2.065	21.598
			Max. Mx	20	-69.887	4381.578	-28.212
			Max. My	2	-69.881	-27.790	4465.968
			Max. Vy	20	-37.388	4381.578	-28.212
L13	9 - 0	Pole	Max. Vx	2	-38.116	-27.790	4465.968
			Max. Torque	18			-8.732
			Max Tension	1	0.000	0.000	0.000
			Max. Compression	26	-130.925	1.746	22.114
			Max. Mx	20	-75.747	4720.685	-30.704
			Max. My	2	-75.747	-30.330	4811.652
			Max. Vy	20	-37.998	4720.685	-30.704
			Max. Vx	2	-38.720	-30.330	4811.652
			Max. Torque	18			-8.732

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	26	130.925	0.000	0.000
	Max. H <sub>x</sub>	20	75.755	37.981	-0.279
	Max. H <sub>z</sub>	2	75.755	-0.279	38.703
	Max. M <sub>x</sub>	2	4811.652	-0.279	38.703
	Max. M <sub>z</sub>	8	4716.385	-37.981	0.279
	Max. Torsion	6	8.731	-33.031	19.593
	Min. Vert	7	56.817	-33.031	19.593
	Min. H <sub>x</sub>	8	75.755	-37.981	0.279
	Min. H <sub>z</sub>	14	75.755	0.279	-38.703
	Min. M <sub>x</sub>	14	-4808.071	0.279	-38.703
	Min. M <sub>z</sub>	20	-4720.685	37.981	-0.279
	Min. Torsion	18	-8.732	33.031	-19.593

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	63.130	0.000	0.000	-1.423	1.702	0.000
1.2 Dead+1.6 Wind 0 deg - No Ice	75.755	0.279	-38.703	-4811.652	-30.330	-4.993
0.9 Dead+1.6 Wind 0 deg - No Ice	56.817	0.279	-38.703	-4767.407	-30.634	-4.980
1.2 Dead+1.6 Wind 30 deg - No Ice	75.755	19.232	-33.657	-4183.468	-2385.187	-7.923
0.9 Dead+1.6 Wind 30 deg - No Ice	56.817	19.232	-33.657	-4144.967	-2364.016	-7.910
1.2 Dead+1.6 Wind 60 deg - No Ice	75.755	33.031	-19.593	-2434.840	-4100.409	-8.731

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Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Ice						
0.9 Dead+1.6 Wind 60 deg - No Ice	56.817	33.031	-19.593	-2412.275	-4063.586	-8.722
1.2 Dead+1.6 Wind 90 deg - No Ice	75.755	37.981	-0.279	-34.225	-4716.385	-7.201
0.9 Dead+1.6 Wind 90 deg - No Ice	56.817	37.981	-0.279	-33.517	-4673.926	-7.197
1.2 Dead+1.6 Wind 120 deg - No Ice	75.755	35.315	20.590	2533.804	-4342.840	-4.037
0.9 Dead+1.6 Wind 120 deg - No Ice	56.817	35.315	20.590	2511.322	-4304.081	-4.040
1.2 Dead+1.6 Wind 150 deg - No Ice	75.755	18.793	33.455	4152.790	-2332.020	0.725
0.9 Dead+1.6 Wind 150 deg - No Ice	56.817	18.793	33.455	4115.437	-2311.274	0.716
1.2 Dead+1.6 Wind 180 deg - No Ice	75.755	-0.279	38.703	4808.071	34.598	4.995
0.9 Dead+1.6 Wind 180 deg - No Ice	56.817	-0.279	38.703	4764.756	33.792	4.982
1.2 Dead+1.6 Wind 210 deg - No Ice	75.755	-19.232	33.657	4179.917	2389.436	7.925
0.9 Dead+1.6 Wind 210 deg - No Ice	56.817	-19.232	33.657	4142.337	2367.159	7.913
1.2 Dead+1.6 Wind 240 deg - No Ice	75.755	-33.031	19.593	2431.319	4104.674	8.732
0.9 Dead+1.6 Wind 240 deg - No Ice	56.817	-33.031	19.593	2409.667	4066.741	8.723
1.2 Dead+1.6 Wind 270 deg - No Ice	75.755	-37.981	0.279	30.705	4720.685	7.199
0.9 Dead+1.6 Wind 270 deg - No Ice	56.817	-37.981	0.279	30.910	4677.107	7.195
1.2 Dead+1.6 Wind 300 deg - No Ice	75.755	-35.315	-20.590	-2537.346	4347.161	4.034
0.9 Dead+1.6 Wind 300 deg - No Ice	56.817	-35.315	-20.590	-2513.946	4307.277	4.038
1.2 Dead+1.6 Wind 330 deg - No Ice	75.755	-18.793	-33.455	-4156.370	2336.323	-0.726
0.9 Dead+1.6 Wind 330 deg - No Ice	56.817	-18.793	-33.455	-4118.087	2314.457	-0.717
1.2 Dead+1.0 Ice+1.0 Temp	130.925	-0.000	-0.000	-22.114	1.746	-0.001
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	130.925	0.029	-7.446	-964.437	-1.772	-0.726
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp	130.925	3.712	-6.463	-839.986	-467.700	-1.120
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp	130.925	6.401	-3.748	-496.443	-807.835	-1.215
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	130.925	7.497	-0.029	-25.859	-939.873	-0.985
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp	130.925	7.199	4.175	498.587	-895.947	-0.543
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp	130.925	3.760	6.605	801.420	-467.122	0.135
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	130.925	-0.029	7.446	919.795	5.306	0.723
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	130.925	-3.712	6.463	795.345	471.235	1.118
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp	130.925	-6.401	3.748	451.803	811.371	1.213
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	130.925	-7.497	0.029	-18.782	943.410	0.983
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	130.925	-7.199	-4.175	-543.229	899.483	0.540

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Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 330	130.925	-3.760	-6.605	-846.063	470.657	-0.137
deg+1.0 Ice+1.0 Temp						
Dead+Wind 0 deg - Service	63.130	0.056	-7.792	-964.701	-4.725	-1.008
Dead+Wind 30 deg - Service	63.130	3.872	-6.776	-838.906	-476.300	-1.601
Dead+Wind 60 deg - Service	63.130	6.650	-3.944	-488.726	-819.775	-1.765
Dead+Wind 90 deg - Service	63.130	7.646	-0.056	-7.989	-943.114	-1.456
Dead+Wind 120 deg - Service	63.130	7.110	4.145	506.333	-868.420	-0.757
Dead+Wind 150 deg - Service	63.130	3.783	6.735	830.495	-465.645	0.145
Dead+Wind 180 deg - Service	63.130	-0.056	7.792	961.732	8.286	1.008
Dead+Wind 210 deg - Service	63.130	-3.872	6.776	835.938	479.861	1.601
Dead+Wind 240 deg - Service	63.130	-6.650	3.944	485.759	823.336	1.765
Dead+Wind 270 deg - Service	63.130	-7.646	0.056	5.022	946.676	1.456
Dead+Wind 300 deg - Service	63.130	-7.110	-4.145	-509.301	871.983	0.757
Dead+Wind 330 deg - Service	63.130	-3.783	-6.735	-833.464	469.208	-0.145

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.000	-63.130	0.000	0.000	63.130	0.000	0.000%
2	0.279	-75.755	-38.703	-0.279	75.755	38.703	0.000%
3	0.279	-56.817	-38.703	-0.279	56.817	38.703	0.000%
4	19.232	-75.755	-33.657	-19.232	75.755	33.657	0.000%
5	19.232	-56.817	-33.657	-19.232	56.817	33.657	0.000%
6	33.031	-75.755	-19.593	-33.031	75.755	19.593	0.000%
7	33.031	-56.817	-19.593	-33.031	56.817	19.593	0.000%
8	37.981	-75.755	-0.279	-37.981	75.755	0.279	0.000%
9	37.981	-56.817	-0.279	-37.981	56.817	0.279	0.000%
10	35.315	-75.755	20.590	-35.315	75.755	-20.590	0.000%
11	35.315	-56.817	20.590	-35.315	56.817	-20.590	0.000%
12	18.793	-75.755	33.455	-18.793	75.755	-33.455	0.000%
13	18.793	-56.817	33.455	-18.793	56.817	-33.455	0.000%
14	-0.279	-75.755	38.703	0.279	75.755	-38.703	0.000%
15	-0.279	-56.817	38.703	0.279	56.817	-38.703	0.000%
16	-19.232	-75.755	33.657	19.232	75.755	-33.657	0.000%
17	-19.232	-56.817	33.657	19.232	56.817	-33.657	0.000%
18	-33.031	-75.755	19.593	33.031	75.755	-19.593	0.000%
19	-33.031	-56.817	19.593	33.031	56.817	-19.593	0.000%
20	-37.981	-75.755	0.279	37.981	75.755	-0.279	0.000%
21	-37.981	-56.817	0.279	37.981	56.817	-0.279	0.000%
22	-35.315	-75.755	-20.590	35.315	75.755	20.590	0.000%
23	-35.315	-56.817	-20.590	35.315	56.817	20.590	0.000%
24	-18.793	-75.755	-33.455	18.793	75.755	33.455	0.000%
25	-18.793	-56.817	-33.455	18.793	56.817	33.455	0.000%
26	0.000	-130.925	0.000	0.000	130.925	0.000	0.000%
27	0.029	-130.925	-7.446	-0.029	130.925	7.446	0.000%
28	3.712	-130.925	-6.463	-3.712	130.925	6.463	0.000%
29	6.401	-130.925	-3.748	-6.401	130.925	3.748	0.000%
30	7.497	-130.925	-0.029	-7.497	130.925	0.029	0.000%
31	7.199	-130.925	4.175	-7.199	130.925	-4.175	0.000%
32	3.760	-130.925	6.605	-3.760	130.925	-6.605	0.000%
33	-0.029	-130.925	7.446	0.029	130.925	-7.446	0.000%
34	-3.712	-130.925	6.463	3.712	130.925	-6.463	0.000%
35	-6.401	-130.925	3.748	6.401	130.925	-3.748	0.000%
36	-7.497	-130.925	0.029	7.497	130.925	-0.029	0.000%
37	-7.199	-130.925	-4.175	7.199	130.925	4.175	0.000%

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Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
38	-3.760	-130.925	-6.605	3.760	130.925	6.605	0.000%
39	0.056	-63.130	-7.792	-0.056	63.130	7.792	0.000%
40	3.872	-63.130	-6.776	-3.872	63.130	6.776	0.000%
41	6.650	-63.130	-3.944	-6.650	63.130	3.944	0.000%
42	7.646	-63.130	-0.056	-7.646	63.130	0.056	0.000%
43	7.110	-63.130	4.145	-7.110	63.130	-4.145	0.000%
44	3.783	-63.130	6.735	-3.783	63.130	-6.735	0.000%
45	-0.056	-63.130	7.792	0.056	63.130	-7.792	0.000%
46	-3.872	-63.130	6.776	3.872	63.130	-6.776	0.000%
47	-6.650	-63.130	3.944	6.650	63.130	-3.944	0.000%
48	-7.646	-63.130	0.056	7.646	63.130	-0.056	0.000%
49	-7.110	-63.130	-4.145	7.110	63.130	4.145	0.000%
50	-3.783	-63.130	-6.735	3.783	63.130	6.735	0.000%

## Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.0000001	0.0000001
2	Yes	5	0.0000001	0.00011332
3	Yes	5	0.0000001	0.00005450
4	Yes	5	0.0000001	0.00097734
5	Yes	5	0.0000001	0.00045184
6	Yes	6	0.0000001	0.00004895
7	Yes	5	0.0000001	0.00055840
8	Yes	5	0.0000001	0.00020073
9	Yes	5	0.0000001	0.00009741
10	Yes	6	0.0000001	0.00004522
11	Yes	5	0.0000001	0.00051217
12	Yes	6	0.0000001	0.00004197
13	Yes	5	0.0000001	0.00047792
14	Yes	5	0.0000001	0.00014472
15	Yes	5	0.0000001	0.00006953
16	Yes	6	0.0000001	0.00004868
17	Yes	5	0.0000001	0.00055440
18	Yes	5	0.0000001	0.00097415
19	Yes	5	0.0000001	0.00045109
20	Yes	5	0.0000001	0.00016976
21	Yes	5	0.0000001	0.00008256
22	Yes	6	0.0000001	0.00005011
23	Yes	5	0.0000001	0.00056762
24	Yes	6	0.0000001	0.00004290
25	Yes	5	0.0000001	0.00048793
26	Yes	4	0.0000001	0.00025725
27	Yes	5	0.0000001	0.00083304
28	Yes	5	0.0000001	0.00087481
29	Yes	5	0.0000001	0.00086769
30	Yes	5	0.0000001	0.00080122
31	Yes	5	0.0000001	0.00091124
32	Yes	5	0.0000001	0.00082538
33	Yes	5	0.0000001	0.00078143
34	Yes	5	0.0000001	0.00083411
35	Yes	5	0.0000001	0.00083587
36	Yes	5	0.0000001	0.00080857
37	Yes	5	0.0000001	0.00095863
38	Yes	5	0.0000001	0.00088050

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39	Yes	4	0.00000001	0.00015660
40	Yes	4	0.00000001	0.00028623
41	Yes	4	0.00000001	0.00043320
42	Yes	4	0.00000001	0.00021117
43	Yes	4	0.00000001	0.00029947
44	Yes	4	0.00000001	0.00027717
45	Yes	4	0.00000001	0.00016139
46	Yes	4	0.00000001	0.00042233
47	Yes	4	0.00000001	0.00029756
48	Yes	4	0.00000001	0.00020654
49	Yes	4	0.00000001	0.00038341
50	Yes	4	0.00000001	0.00029573

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	180 - 145.7	19.987	49	0.982	0.004
L2	145.7 - 140	13.179	49	0.851	0.003
L3	140 - 106.42	12.186	49	0.810	0.003
L4	106.42 - 100	7.020	49	0.632	0.003
L5	100 - 86.25	6.194	49	0.596	0.002
L6	86.25 - 78	4.604	49	0.505	0.002
L7	78 - 60	3.770	49	0.459	0.002
L8	60 - 46.25	2.219	49	0.360	0.001
L9	46.25 - 32.67	1.309	49	0.270	0.001
L10	32.67 - 20	0.651	49	0.191	0.001
L11	20 - 11.25	0.237	49	0.119	0.000
L12	11.25 - 9	0.071	49	0.061	0.000
L13	9 - 0	0.046	49	0.048	0.000

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
184.000	Lighting Rod 5/8" x 8"	49	19.987	0.982	0.004	46268
177.000	APXVSPP18-C-A20 w/ Mount Pipe	49	19.362	0.975	0.004	46268
175.000	PCS 1900MHz 4x45W-65MHz	49	18.945	0.970	0.004	46268
162.000	7770.00	49	16.282	0.932	0.003	12852
140.000	Bridge Stiffener (48"x1.25"x11.5")	49	12.186	0.810	0.003	12437
110.000	(4) SBNHH-1D65C	49	7.506	0.651	0.003	8683

### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	180 - 145.7	99.536	22	4.899	0.017
L2	145.7 - 140	65.636	22	4.242	0.016

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Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L3	140 - 106.42	60.695	22	4.040	0.015
L4	106.42 - 100	34.980	22	3.151	0.014
L5	100 - 86.25	30.867	22	2.968	0.012
L6	86.25 - 78	22.946	22	2.517	0.009
L7	78 - 60	18.793	22	2.288	0.008
L8	60 - 46.25	11.064	22	1.792	0.005
L9	46.25 - 32.67	6.527	22	1.347	0.004
L10	32.67 - 20	3.244	22	0.953	0.002
L11	20 - 11.25	1.180	22	0.595	0.001
L12	11.25 - 9	0.355	22	0.302	0.001
L13	9 - 0	0.228	22	0.239	0.001

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
184.000	Lighting Rod 5/8" x 8'	22	99.536	4.899	0.018	9421
177.000	APXVSPP18-C-A20 w/ Mount Pipe	22	96.421	4.864	0.018	9421
175.000	PCS 1900MHz 4x45W-65MHz	22	94.348	4.840	0.018	9421
162.000	7770.00	22	81.088	4.651	0.017	2615
140.000	Bridge Stiffener (48"x1.25"x11.5")	22	60.695	4.040	0.016	2525
110.000	(4) SBNHH-1D65C	22	37.398	3.243	0.015	1755

### Compression Checks

### Pole Design Data

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio P <sub>u</sub> / φP <sub>n</sub>
L1	180 - 145.7 (1)	P24x3/8	34.300	0.000	0.0	27.833	-10.679	901.775	0.012
L2	145.7 - 140 (2)	P24x3/8 [0.677164]	5.700	0.000	0.0	49.616	-11.840	2026.420	0.006
L3	140 - 106.42 (3)	P36x1/2	33.580	0.000	0.0	55.763	-23.518	1806.730	0.013
L4	106.42 - 100 (4)	P36x1/2 [0.759201]	6.420	0.000	0.0	84.053	-25.816	3354.020	0.008
L5	100 - 86.25 (5)	P42x1/2	13.750	0.000	0.0	65.188	-29.923	2112.090	0.014
L6	86.25 - 78 (6)	P42x1/2 [0.732342]	8.250	0.000	0.0	94.945	-33.456	3686.900	0.009
L7	78 - 60 (7)	P42x1/2 [0.914993]	18.000	0.000	0.0	118.100	-42.981	4586.050	0.009
L8	60 - 46.25 (8)	P48x5/8	13.750	0.000	0.0	93.021	-48.727	3013.870	0.016
L9	46.25 - 32.67 (9)	P48x5/8 [0.826841]	13.580	0.000	0.0	122.537	-56.171	3753.930	0.015
L10	32.67 - 20 (10)	P48x5/8 [0.983981]	12.670	0.000	0.0	145.339	-64.391	5731.410	0.011
L11	20 - 11.25 (11)	P54x5/8 4.8.2 (1.05 CR) - 11	8.750	0.000	0.0	104.802	-68.515	3395.570	0.020
L12	11.25 - 9 (12)	P54x5/8 [0.793292]	2.250	0.000	0.0	132.602	-69.864	4116.960	0.017
L13	9 - 0 (13)	P54x5/8 [0.884318]	9.000	0.000	0.0	147.564	-75.746	4480.350	0.017

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### Pole Bending Design Data

Section No.	Elevation ft	Size	$M_{ux}$ kip-ft	$\phi M_{ux}$ kip-ft	Ratio $\frac{M_{ux}}{\phi M_{ux}}$	$M_{uy}$ kip-ft	$\phi M_{uy}$ kip-ft	Ratio $\frac{M_{uy}}{\phi M_{uy}}$
L1	180 - 145.7 (1)	P24x3/8	370.271	550.881	0.672	0.000	550.881	0.000
L2	145.7 - 140 (2)	P24x3/8 [0.677164]	473.074	1254.008	0.377	0.000	1254.008	0.000
L3	140 - 106.42 (3)	P36x1/2	1210.858	1623.158	0.746	0.000	1623.158	0.000
L4	106.42 - 100 (4)	P36x1/2 [0.759201]	1404.142	3100.258	0.453	0.000	3100.258	0.000
L5	100 - 86.25 (5)	P42x1/2	1835.808	2162.842	0.849	0.000	2162.842	0.000
L6	86.25 - 78 (6)	P42x1/2 [0.732342]	2106.308	3871.308	0.544	0.000	3871.308	0.000
L7	78 - 60 (7)	P42x1/2 [0.914993]	2725.933	4998.758	0.545	0.000	4998.758	0.000
L8	60 - 46.25 (8)	P48x5/8	3224.542	3573.958	0.902	0.000	3573.958	0.000
L9	46.25 - 32.67 (9)	P48x5/8 [0.826841]	3736.575	4697.800	0.795	0.000	4697.800	0.000
L10	32.67 - 20 (10)	P48x5/8 [0.983981]	4229.942	7046.283	0.600	0.000	7046.283	0.000
L11	20 - 11.25 (11)	P54x5/8	4578.033	4453.000	1.028	0.000	4453.000	0.000
L12	11.25 - 9 (12)	P54x5/8 [0.793292]	4668.392	5647.225	0.827	0.000	5647.225	0.000
L13	9 - 0 (13)	P54x5/8 [0.884318]	5033.483	6313.117	0.797	0.000	6313.117	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual $V_u$ K	$\phi V_n$ K	Ratio $\frac{V_u}{\phi V_n}$	Actual $T_u$ kip-ft	$\phi T_n$ kip-ft	Ratio $\frac{T_u}{\phi T_n}$
L1	180 - 145.7 (1)	P24x3/8	17.490	450.887	0.039	1.026	874.033	0.001
L2	145.7 - 140 (2)	P24x3/8 [0.677164]	18.591	1013.210	0.018	1.327	1915.292	0.001
L3	140 - 106.42 (3)	P36x1/2	29.711	903.365	0.033	4.046	2635.858	0.002
L4	106.42 - 100 (4)	P36x1/2 [0.759201]	30.519	1677.010	0.018	4.045	4823.308	0.001
L5	100 - 86.25 (5)	P42x1/2	32.267	1056.050	0.031	4.043	3609.208	0.001
L6	86.25 - 78 (6)	P42x1/2 [0.732342]	33.321	1843.450	0.018	4.041	6230.983	0.001
L7	78 - 60 (7)	P42x1/2 [0.914993]	35.507	2293.020	0.015	4.039	7683.517	0.001
L8	60 - 46.25 (8)	P48x5/8	37.020	1506.930	0.025	4.037	5872.808	0.001
L9	46.25 - 32.67 (9)	P48x5/8 [0.826841]	38.396	1876.970	0.020	4.036	7253.658	0.001
L10	32.67 - 20 (10)	P48x5/8 [0.983981]	39.494	2865.710	0.014	4.035	11002.500	0.000
L11	20 - 11.25 (11)	P54x5/8	40.100	1697.790	0.024	4.035	7465.225	0.001
L12	11.25 - 9 (12)	P54x5/8 [0.793292]	40.259	2058.480	0.020	4.034	8995.000	0.000
L13	9 - 0 (13)	P54x5/8 [0.884318]	40.897	2240.180	0.018	4.034	9756.000	0.000

### Pole Interaction Design Data

Section No.	Elevation ft	Ratio $\frac{P_u}{\phi P_n}$	Ratio $\frac{M_{ux}}{\phi M_{ux}}$	Ratio $\frac{M_{uy}}{\phi M_{uy}}$	Ratio $\frac{V_u}{\phi V_n}$	Ratio $\frac{T_u}{\phi T_n}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	180 - 145.7 (1)	0.012	0.672	0.000	0.039	0.001	0.686	1.000	4.8.2 ✓
L2	145.7 - 140 (2)	0.006	0.377	0.000	0.018	0.001	0.383	1.000	4.8.2 ✓

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Section No.	Elevation ft	Ratio $P_u$	Ratio $M_{ux}$	Ratio $M_{uy}$	Ratio $V_u$	Ratio $T_u$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
		$\phi P_n$	$\phi M_{nx}$	$\phi M_{ny}$	$\phi V_n$	$\phi T_n$			
L3	140 - 106.42 (3)	0.013	0.746	0.000	0.033	0.002	0.760	1.000	4.8.2 ✓
L4	106.42 - 100 (4)	0.008	0.453	0.000	0.018	0.001	0.461	1.000	4.8.2 ✓
L5	100 - 86.25 (5)	0.014	0.849	0.000	0.031	0.001	0.864	1.000	4.8.2 ✓
L6	86.25 - 78 (6)	0.009	0.544	0.000	0.018	0.001	0.554	1.000	4.8.2 ✓
L7	78 - 60 (7)	0.009	0.545	0.000	0.015	0.001	0.555	1.000	4.8.2 ✓
L8	60 - 46.25 (8)	0.016	0.902	0.000	0.025	0.001	0.919	1.000	4.8.2 ✓
L9	46.25 - 32.67 (9)	0.015	0.795	0.000	0.020	0.001	0.811	1.000	4.8.2 ✓
L10	32.67 - 20 (10)	0.011	0.600	0.000	0.014	0.000	0.612	1.000	4.8.2 ✓
L11	20 - 11.25 (11)	0.020	1.028	0.000	0.024	0.001	1.049	1.000	4.8.2 ✓
L12	11.25 - 9 (12)	0.017	0.827	0.000	0.020	0.000	0.844	1.000	4.8.2 ✓
L13	9 - 0 (13)	0.017	0.797	0.000	0.018	0.000	0.815	1.000	4.8.2 ✓

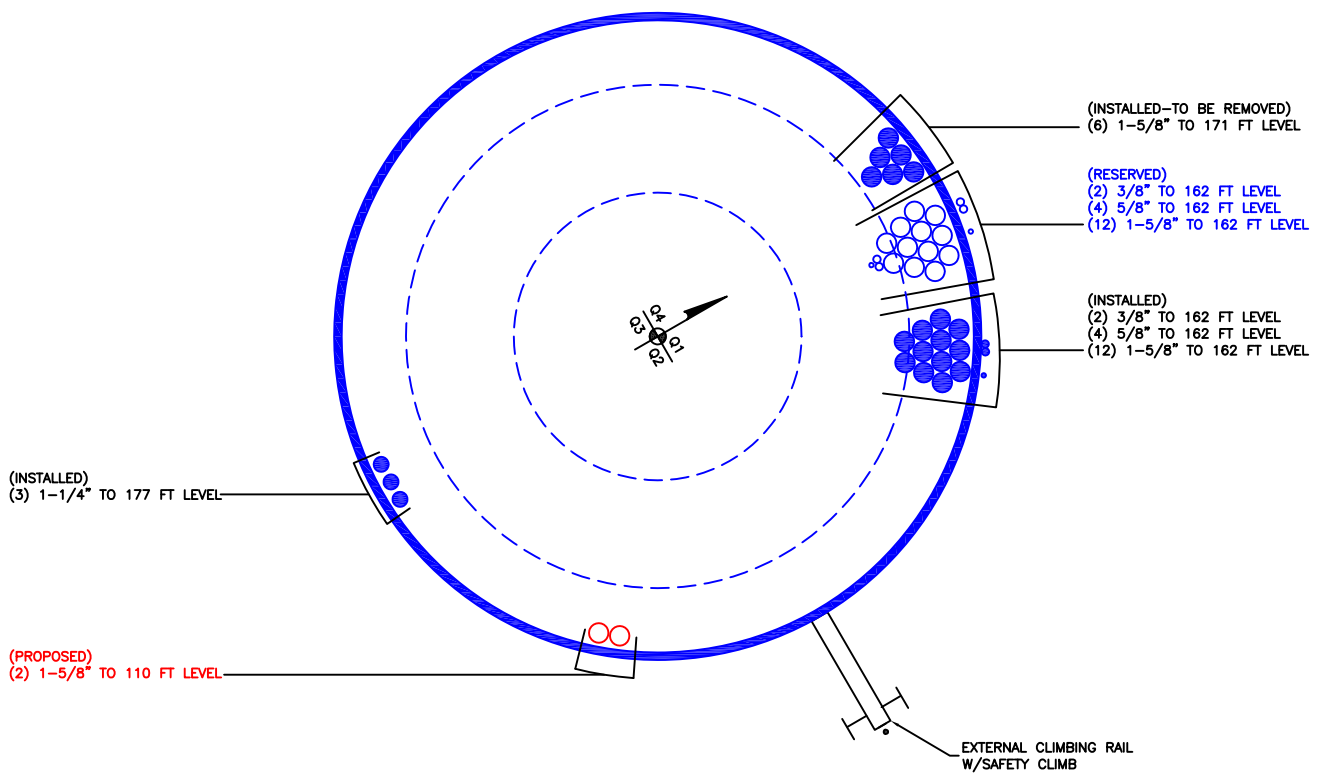
### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow}$ K	% Capacity	Pass Fail
L1	180 - 145.7	Pole	P24x3/8	1	-10.679	901.775	**	**
L2	145.7 - 140	Pole	P24x3/8 [0.677164]	2	-11.840	2026.420	**	**
L3	140 - 106.42	Pole	P36x1/2	3	-23.518	1806.730	**	**
L4	106.42 - 100	Pole	P36x1/2 [0.759201]	4	-25.816	3354.020	**	**
L5	100 - 86.25	Pole	P42x1/2	5	-29.923	2112.090	**	**
L6	86.25 - 78	Pole	P42x1/2 [0.732342]	6	-33.456	3686.900	**	**
L7	78 - 60	Pole	P42x1/2 [0.914993]	7	-42.981	4586.050	**	**
L8	60 - 46.25	Pole	P48x5/8	8	-48.727	3013.870	**	**
L9	46.25 - 32.67	Pole	P48x5/8 [0.826841]	9	-56.171	3753.930	**	**
L10	32.67 - 20	Pole	P48x5/8 [0.983981]	10	-64.391	5731.410	**	**
L11	20 - 11.25	Pole	P54x5/8	11	-68.515	3395.570	**	**
L12	11.25 - 9	Pole	P54x5/8 [0.793292]	12	-69.864	4116.960	**	**
L13	9 - 0	Pole	P54x5/8 [0.884318]	13	-75.746	4480.350	**	**
						Summary		
						Pole (L11)	**	**
						<b>RATING =</b>	**	**

\*\* See additional Calc in Appendix C



**APPENDIX B**  
**BASE LEVEL DRAWING**



BUSINESS UNIT:878782

**APPENDIX C**  
**ADDITIONAL CALCULATIONS**







Reinforcement Capacity



5500 Flatirons Parkway, Suite 100  
Boulder, CO 80301  
720-304-6882

Dimensions and Properties														Compression				Axial				
Model	Weight (lb/ft)	Area (in <sup>2</sup> )	Moment of Inertia (in <sup>4</sup> )	Moment of Inertia (in <sup>4</sup> )	Centroid from Mating Edge (in)	Centroid from Bolt Hole Center (in)	Web Thickness (in)	Width (in)	Flange Width (in)	Flange Thickness (in)	Hole Diameter (in)	Yield Stress (ksi)	Ultimate Stress (ksi)	Slender. Ratio Coefficient	Unbraced Length (in)	Slender. Ratio Coefficient	Unbraced Length (in)	ASD-9			LRFD	
																		Allowable Axial (kip)	Allowable Axial w/ increase (kip)	Governing Axial	Design Axial Strength (kip)	Governing Axial
<i>Model</i>	<i>Wt</i>	<i>A</i>	<i>Ix</i>	<i>Iy</i>	<i>Y</i>	<i>X</i>	<i>Tw</i>	<i>W</i>	<i>Wf</i>	<i>Tf</i>	<i>Dh</i>	<i>Fy</i>	<i>Fu</i>	<i>Kx</i>	<i>Lx</i>	<i>Ky</i>	<i>Ly</i>	<i>PAII</i>	<i>Pall.inc</i>	<i>Ptype.ASD</i>	<i>phiPn</i>	<i>Ptype.LRFD</i>
CCI-1x4.5	15.3	4.50	0.38	7.59	0.5	0	1	4.5	0	0	1.21875	65	80	0.80	20	1.00	20	128.8	171.7	Rupture	193.1	Rupture
CCI-1x6	20.4	6.00	0.50	18.00	0.5	0	1	6	0	0	1.21875	65	80	0.80	16	1.00	16	188.8	251.7	Rupture	283.1	Rupture
CCI-1.25x6.5	27.6	8.13	1.06	28.61	0.625	0	1.25	6.5	0	0	1.21875	65	80	0.80	19	1.00	19	260.4	347.2	Compress.	391.4	Rupture
CCI-1.25x8.5	36.2	10.63	1.38	63.97	0.625	0	1.25	8.5	0	0	1.21875	65	80	0.80	17	1.00	17	350.9	467.9	Compress.	541.4	Rupture

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SUBJECT	Welded Existing Bridge Stiffener @ 140 ft		
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Rev. Type: G

**Determine Load to Bridge Stiffener:**

M	=	<u>473.07</u>	k-ft	From tnx Model
I	=	<u>8416.89</u>	in <sup>4</sup>	From AutoCAD Sketch
$\bar{y}_{bar}$	=	<u>21.00</u>	in	
S	=	<u>400.804</u>	in <sup>3</sup>	I/y
f <sub>c</sub>	=	<u>14.164</u>	ksi	M/S
A <sub>g</sub>	=	<u>6.250</u>	in <sup>2</sup>	
P <sub>u</sub>	=	<u>88.523</u>	k	f <sub>c</sub> x A <sub>g</sub>

Stiffener Width	=	<u>5.000</u>	in
Stiffener Thickness	=	<u>1.250</u>	in
Stiffener Height	=	<u>48.000</u>	in
F <sub>y</sub>	=	<u>65</u>	ksi
Step Width	=	<u>6.00</u>	in
Fillet Weld to Pole	=	<u>3/8</u>	in
Bolt Circle	=	<u>29.50</u>	in
Number of Bolts	=	<u>24</u>	
Bolt Size	=	<u>3/4</u>	in
Bolt Area	=	<u>0.44</u>	in <sup>2</sup>
Notch	=	<u>2.000</u>	in

**Determine  $\Phi P_n$  (Allowable Axial Load):**

$P_n = F_{cr} \times A_g$			Eqn E3-1, AISC 13th Edition, Section E3.
K	=	<u>1</u>	
I	=	<u>8.000</u>	in
I <sub>y</sub>	=	<u>0.814</u>	in <sup>4</sup>
A <sub>g</sub>	=	<u>6.250</u>	in <sup>2</sup>
r <sub>y</sub>	=	<u>0.361</u>	in
kl/r	=	<u>22.170</u>	

$4.71 \times \sqrt{E/F_y} = 99.49$       Limit State Equation for Flexural Buckling - AISC 13th Edition, Section E3.

F <sub>e</sub>	=	<u>582.31</u>	ksi	Eqn E3-4 - AISC 13th Edition, Section E3. Elastic Critical Buckling Stress
F <sub>cr</sub>	=	<u>62.03</u>	ksi	Eqn E3-2, AISC 13th Edition, Section E3 Critical Buckling Stress
P <sub>n</sub>	=	<u>387.71</u>	k	Nominal Compressive Strength
$\Phi P_n$	=	<u>348.94</u>	k	Allowable Compressive Strength

**Unity% = 25.4 %**

**Determine  $\Phi M_n$  (Allowable Strong Axis Moment on Bridge Stiffener):**

P <sub>u</sub>	=	<u>88.52</u>	k	From Above
e	=	<u>5.50</u>	in	Eccentricity
M <sub>u</sub>	=	<u>486.88</u>	k-in	Moment Due to Eccentric Load on Bridge Stiffener
M <sub>p</sub>	=	<u>23400.00</u>	k-in	Plastic Moment - Eqn F11-1, AISC 13th Edition, Section F11.
L <sub>b</sub> d/t <sup>2</sup>	=	<u>76.80</u>		For All Bridge Stiffeners, Eqn F11-2 Will Control.
M <sub>y</sub>	=	<u>31200.00</u>	k-in	Moment at Yield
M <sub>n</sub>	=	<u>45952.43</u>	k-in	Nominal moment - Eqn F11-2, AISC 13th Edition, Section F11.
$\Phi M_n$	=	<u>41357.18</u>	k-in	Allowable Strong Axis Moment

**Unity% = 2.1 %**

**Moment to Existing Bolt Group:**

I(Bolts)	=	1153.4 in <sup>4</sup>
I(Total)	=	8416.89

$\frac{I(\text{Bolts})}{I(\text{Total})} = \frac{1153.39}{8416.89} = 0.137$

**Meq = 64.83 k-ft** <-----Insert into Flange Spreadsheet



PROJECT	<b>86959.008.01 - PORTLAND WARREN AVE, ME</b>		
SUBJECT	<b>Welded Existing Bridge Stiffener @ 140 ft</b>		
DATE	<b>05/21/16</b>	PAGE	2 OF 2



**Check for Welded Connection**

Weld Size = **3/8**      D = 6 in  
 Weld grade = **70 ksi**  
 Plate Dia = **36 in**

	<b>Upper pole</b>	<b>Lower Pole</b>
Pole dia	<b>24 in</b>	<b>36 in</b>
Weld Length	<b>20 in</b>	<b>20 in</b>
Eccentricity	10.500 in	4.5
a	0.53	0.23
C1	1	1
K	0	0
C	2.211	3.413
P(Allowable)	198.96 K	307.14 K
Unity (%)	<b>44.5%</b>	<b>28.8%</b>

<b>Unity% =</b>	<b>44.5%</b>
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PROJECT	86959.008.01 - Portland Warren Ave, ME		
SUBJECT	Existing Flat Plate Bridge Stiffeners @ 140'		
DATE	05/21/16	PAGE	1 OF 1



**Determine Load to Bridge Stiffener:**

<b>M =</b>	473.1 k-ft	From Risa Model	<b>Stiffener Width</b>	6.000 in
<b>I =</b>	8416.9 in <sup>4</sup>	From AutoCAD Sketch	<b>Stiffener Thickness</b>	1.000 in
<b>ybar =</b>	18.500 in			
<b>S =</b>	454.97 in <sup>3</sup>	I/y	<b>Fy</b>	65 ksi
<b>fc =</b>	12.48 ksi	M/S	<b>Fu</b>	80 ksi
<b>Ag =</b>	6.000 in <sup>2</sup>			
<b>Pu =</b>	74.87 k	fc x Ag	<b>Bolt Circle</b>	29.50 in
			<b>Number of Bolts</b>	24
			<b>Bolt Size</b>	3/4
			<b>Gap @ Flange</b>	6.00 in

**Determine  $\Phi P_n$  (Allowable Axial Load):**

<b>Pn = Fcr x Ag</b>		Eqn E3-1, AISC 13th Edition, Section E3.		
<b>K =</b>	1			
<b>I =</b>	16.000 in	Unsupported Length		
<b>Iy =</b>	.500 in <sup>4</sup>	Local Weak Axis Moment of Intertia		
<b>Ag =</b>	6.000 in <sup>2</sup>	Stiffener Cross Sectional Area		
<b>ry =</b>	.289 in	Radius of Gyration (Weak Axis)		
<b>kl/r =</b>	55.43			
<b>4.71 x <math>\sqrt{E/Fy}</math> =</b>	99.49	Limit State Equation for Flexural Buckling - AISC 13th Edition, Section E3.		
<b>Fe =</b>	93.17 ksi	Eqn E3-4 - AISC 13th Edition, Section E3.		
		Elastic Critical Buckling Stress		
<b>Fcr =</b>	48.54 ksi	Eqn E3-2, AISC 13th Edition, Section E3		
		Critical Buckling Stress		
<b>Pn =</b>	291.24 k	Nominal Compressive Strength		
<b><math>\Phi P_n</math> =</b>	262.12 k	Allowable Compressive Strength	<b>Unity% =</b>	28.6 %

**Tension Rupture Check:**

AISC 13th Edition, Chapter J4.1

<b>Hole Size</b>	1.25			
<b>U =</b>	1			
<b>Ag =</b>	6.000 in <sup>2</sup>		Shear Lag Factor - Table D3.1 and TIA222-G	
<b>An =</b>	4.750 in <sup>2</sup>		Gross Area	
<b>Ae =</b>	4.750 in <sup>2</sup>		Net Area	
<b><math>\Phi R_n</math> =</b>	351.00 k		Effective Area	
			Tension Yielding: Eqn J4-1	
<b><math>\Phi R_n</math> =</b>	285.00 k		Tension Rupture: Eqn J4-2	
<b><math>\Phi R_n</math>(Equiv)</b>	285.00 ksi			
			<b>Unity%</b>	26.3 %

**Moment to Existing Bolt Group:**

<b>S<sub>BG</sub> =</b>	570.64 in <sup>3</sup>	<b># Bolts Acting</b>	6
<b>ft =</b>	9.95 ksi		
<b>Ab =</b>	.442 in <sup>2</sup>		
<b>T =</b>	26.37 k		
<b>Arm =</b>	29.50 ksi		
<b>M<sub>EQ</sub> =</b>	64.8 k-ft		

←-----Insert into Crown Spreadsheet

# Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 321952 Revision # 13

Reactions		
Mu	64.83	ft-kips
Axial, Pu:	11.84	kips
Shear, Vu:	18.59	kips
Elevation:	140	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
21.87

Pole Manufacturer: Other

Bolt Data		
Qty:	24	
Diameter (in.):	0.75	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:		<-- Disregard
N/A:		<-- Disregard
Circle (in.):	29.5	

Plate Data		
Diam:	34.75	in
Thick, t:	1.875	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	3.14	in

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

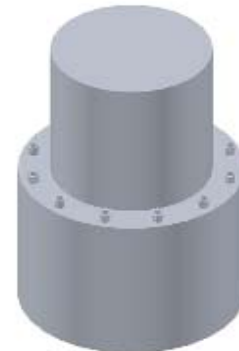
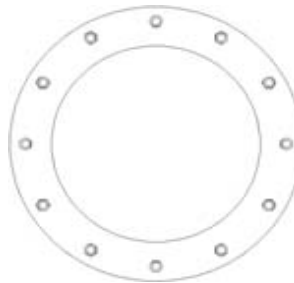
Pole Data		
Diam:	24	in
Thick:	0.375	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi
Reinf. Fillet Weld	0	"0" if None

If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Flange Bolt Results		Rigid
Bolt Tension Capacity, $\phi^* T_n, B1$ :	30.06 kips	$\phi^* T_n$
Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$ ), B:	30.04 kips	$\phi T_n [(1 - (V_u / \phi V_n)^2)^{0.5}]$
Max Bolt directly applied Tu:	3.90 Kips	
Min. PL "tc" for B cap. w/o Pry:	1.319 in	
Min PL "treq" for actual T w/ Pry:	0.360 in	
Min PL "t1" for actual T w/o Pry:	0.475 in	
T allowable w/o Prying:	30.06 kips	$\alpha < 0$ case
Prying Force, q:	0.00 kips	
Total Bolt Tension = Tu + q:	3.90 kips	
Non-Prying Bolt Stress Ratio, Tu/B:	13.0% Pass	

Exterior Flange Plate Results		Flexural Check	Rigid
Compression Side Plate Stress:	2.7 ksi		TIA G
Allowable Plate Stress:	32.4 ksi		$\phi^* F_y$
Compression Plate Stress Ratio:	8.5% Pass		Comp. Y.L. Length:
			17.15
<b>No Prying</b>			
Tension Side Stress Ratio, $(treq/t)^2$ :	3.7% Pass		

n/a  
**Stiffener Results**  
 Horizontal Weld : n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a  
**Pole Results**  
 Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

# Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 321952 Revision # 13

Manufacturer: Other

## Bolt Data

Qty:	24	Bolt Fu:	120
Diam:	0.75	Bolt Fy:	92
Bolt Material:	A325		
N/A:		<-- Disregard	
N/A:		<-- Disregard	
Circle:	29.5	in	

## Plate Data

Plate Outer Diam:	35	in
Plate Inner Diam:	24.25	in (Hole @ Ctr)
Thick:	1.875	in
Grade:	36	ksi
<b>Effective Width:</b>	4.58	in

## Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

## Pole Data

Pole OuterDiam:	36	in
Thick:	0.5	in
Pole Inner Diam:	35	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi

## Reactions

Moment:	64.83	ft-kips
Axial:	11.84	kips
Shear:	18.59	kips
Exterior Flange Run, T+q:	3.9	kips

## Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi V_n$ (kips):
21.87

Elevation: 140 feet

## Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 3.9 Kips, Ext. Tu=Interior Tu  
 Adjusted  $\phi T_n$  (due to  $V_u = V_u / Q_t$ ): 30.0 Kips  
 Bolt Stress Ratio: 13.0% **Pass**

## Interior Flange Plate Results

Controlling Bolt Axial Force: 4.9 Kips, Ext. Cu=Interior Cu  
 Plate Stress: 3.3 ksi  
 Allowable Plate Stress,  $\phi F_y$ : 32.4 ksi  
 Plate Stress Ratio: 10.3% **Pass**

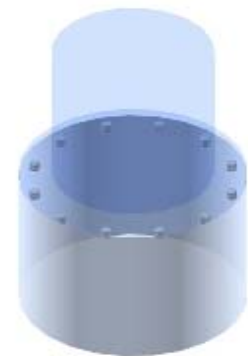
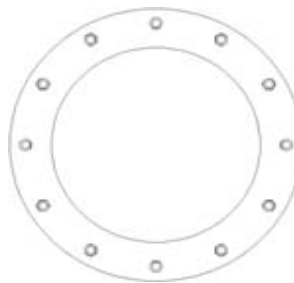
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## Stiffener Results

Horizontal Weld : n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a

## Pole Results

Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

PROJECT	86959.008.01 - Portland Warren Ave, ME		
SUBJECT	Existing Flat Plate Bridge Stiffeners @ 100'		
DATE	05/21/16	PAGE	1 OF 1



0

### Determine Load to Bridge Stiffener:

M =	1404.1 k-ft	From Risa Model	Stiffener Width	6.500 in
I =	10001.1 in <sup>4</sup>	From AutoCAD Sketch	Stiffener Thickness	1.250 in
ybar =	21.625 in			
S =	462.48 in <sup>3</sup>	I/y	Fy	65 ksi
fc =	36.43 ksi	M/S	Fu	80 ksi
Ag =	8.125 in <sup>2</sup>			
Pu =	296.02 k	fc x Ag	Bolt Circle	38.50 in
			Number of Bolts	52
			Bolt Size	3/4
			Gap @ Flange	6.00 in

### Determine $\Phi P_n$ (Allowable Axial Load):

$P_n = F_{cr} \times A_g$		Eqn E3-1, AISC 13th Edition, Section E3.		
K =	1			
I =	16.000 in	Unsupported Length		
$I_y =$	1.058 in <sup>4</sup>	Local Weak Axis Moment of Intertia		
$A_g =$	8.125 in <sup>2</sup>	Stiffener Cross Sectional Area		
$r_y =$	.361 in	Radius of Gyration (Weak Axis)		
$kl/r =$	44.34			
$4.71 \times \sqrt{E/F_y} =$	99.49	Limit State Equation for Flexural Buckling - AISC 13th Edition, Section E3.		
$F_e =$	145.58 ksi	Eqn E3-4 - AISC 13th Edition, Section E3.		
		Elastic Critical Buckling Stress		
$F_{cr} =$	53.92 ksi	Eqn E3-2, AISC 13th Edition, Section E3		
		Critical Buckling Stress		
$P_n =$	438.10 k	Nominal Compressive Strength		
$\Phi P_n =$	394.29 k	Allowable Compressive Strength	Unity% =	75.1 %

### Tension Rupture Check:

AISC 13th Edition, Chapter J4.1

Hole Size	1.25			
U =	1		Shear Lag Factor - Table D3.1 and TIA222-G	
$A_g =$	8.125 in <sup>2</sup>		Gross Area	
$A_n =$	6.563 in <sup>2</sup>		Net Area	
$A_e =$	6.563 in <sup>2</sup>		Effective Area	
$\Phi R_n =$	475.31 k		Tension Yielding: Eqn J4-1	
$\Phi R_n =$	393.75 k		Tension Rupture: Eqn J4-2	
$\Phi R_n(\text{Equiv})$	393.75 ksi			
			Unity%	75.2 %

### Moment to Existing Bolt Group:

$S_{BG} =$	519.54 in <sup>3</sup>	# Bolts Acting	13
ft =	32.43 ksi		
$A_b =$	.442 in <sup>2</sup>		
T =	186.26 k		
Arm =	38.50 ksi		
$M_{EQ} =$	597.6 k-ft		

←-----Insert into Crown Spreadsheet

# Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 321952 Revision # 13

Reactions		
Mu	597.6	ft-kips
Axial, Pu:	25.816	kips
Shear, Vu:	30.519	kips
Elevation:	100	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
21.87

Pole Manufacturer: Other

Bolt Data		
Qty:	52	
Diameter (in.):	0.75	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:		<-- Disregard
N/A:		<-- Disregard
Circle (in.):	38.5	

Plate Data		
Diam:	40.75	in
Thick, t:	2.125	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	2.17	in

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

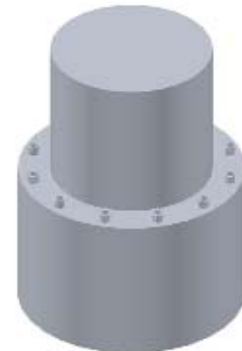
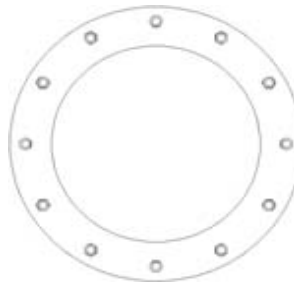
Pole Data		
Diam:	36	in
Thick:	0.5	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi
Reinf. Fillet Weld	0	"0" if None

If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Flange Bolt Results		Rigid
Bolt Tension Capacity, $\phi^* T_n, B1$ :	30.06 kips	$\phi^* T_n$
Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$ ), B:	30.05 kips	$\phi T_n [(1 - (V_u / \phi V_n)^2)^{0.5}]$
Max Bolt directly applied Tu:	13.83 Kips	
Min. PL "tc" for B cap. w/o Pry:	0.962 in	
Min PL "treq" for actual T w/ Pry:	0.512 in	
Min PL "t1" for actual T w/o Pry:	0.653 in	
T allowable w/o Prying:	30.06 kips	$\alpha < 0$ case
Prying Force, q:	0.00 kips	
Total Bolt Tension = Tu + q:	13.83 kips	
Non-Prying Bolt Stress Ratio, Tu/B:	46.0% Pass	

Exterior Flange Plate Results		Flexural Check	Rigid
Compression Side Plate Stress:	4.8 ksi		TIA G
Allowable Plate Stress:	32.4 ksi		$\phi^* F_y$
Compression Plate Stress Ratio:	14.8% Pass		Comp. Y.L. Length:
			13.65
<b>No Prying</b>			
Tension Side Stress Ratio, $(treq/t)^2$ :	5.8% Pass		

n/a  
**Stiffener Results**  
 Horizontal Weld : n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a  
**Pole Results**  
 Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

# Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 321952 Revision # 13

Manufacturer: Other

## Bolt Data

Qty:	52	Bolt Fu:	120
Diam:	0.75	Bolt Fy:	92
Bolt Material:	A325		
N/A:		<-- Disregard	
N/A:		<-- Disregard	
Circle:	38.5	in	

## Plate Data

Plate Outer Diam:	41	in
Plate Inner Diam:	36.25	in (Hole @ Ctr)
Thick:	2.125	in
Grade:	36	ksi
<b>Effective Width:</b>	2.48	in

## Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

## Pole Data

Pole OuterDiam:	42	in
Thick:	0.5	in
Pole Inner Diam:	41	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi

## Reactions

Moment:	597.6	ft-kips
Axial:	25.816	kips
Shear:	30.519	kips
Exterior Flange Run, T+q:	13.83	kips

## Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi V_n$ (kips):
21.87

Elevation: 100 feet

## Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 13.8 Kips, Ext. Tu=Interior Tu  
 Adjusted  $\phi T_n$  (due to  $V_u = V_u / Q_t$ ): 30.0 Kips  
 Bolt Stress Ratio: 46.0% **Pass**

## Interior Flange Plate Results

Controlling Bolt Axial Force: 14.8 Kips, Ext. Cu=Interior Cu  
 Plate Stress: 6.6 ksi  
 Allowable Plate Stress,  $\phi F_y$ : 32.4 ksi  
 Plate Stress Ratio: 20.5% **Pass**

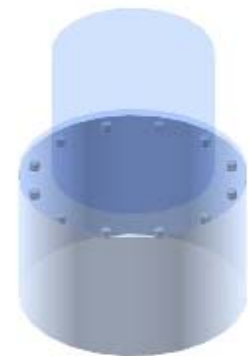
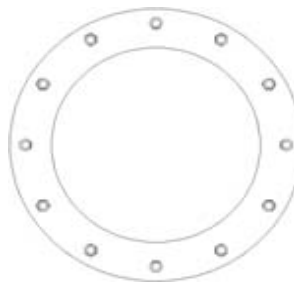
n/a

## Stiffener Results

Horizontal Weld : n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a

## Pole Results

Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

PROJECT	<b>86959.008.01 - Portland Warren Ave, ME</b>		
SUBJECT	<b>Existing Flat Plate Bridge Stiffeners @ 60'</b>		
DATE	<b>05/21/16</b>	PAGE	1 OF 1



**Determine Load to Bridge Stiffener:**

<b>M =</b>	2725.9 k-ft	From Risa Model	<b>Stiffener Width</b>	6.500 in
<b>I =</b>	20174.7 in <sup>4</sup>	From AutoCAD Sketch	<b>Stiffener Thickness</b>	1.250 in
<b>ybar =</b>	24.625 in			
<b>S =</b>	819.28 in <sup>3</sup>	I/y	<b>Fy</b>	65 ksi
<b>fc =</b>	39.93 ksi	M/S	<b>Fu</b>	80 ksi
<b>Ag =</b>	8.125 in <sup>2</sup>			
<b>Pu =</b>	324.41 k	fc x Ag	<b>Bolt Circle</b>	44.38 in
			<b>Number of Bolts</b>	56
			<b>Bolt Size</b>	3/4
			<b>Gap @ Flange</b>	6.00 in

**Determine  $\Phi P_n$  (Allowable Axial Load):**

<b>Pn = Fcr x Ag</b>		Eqn E3-1, AISC 13th Edition, Section E3.		
<b>K =</b>	1			
<b>I =</b>	16.000 in	Unsupported Length		
<b>Iy =</b>	1.058 in <sup>4</sup>	Local Weak Axis Moment of Intertia		
<b>Ag =</b>	8.125 in <sup>2</sup>	Stiffener Cross Sectional Area		
<b>ry =</b>	.361 in	Radius of Gyration (Weak Axis)		
<b>kl/r =</b>	44.34			
<b>4.71 x <math>\sqrt{E/Fy}</math> =</b>	99.49	Limit State Equation for Flexural Buckling - AISC 13th Edition, Section E3.		
<b>Fe =</b>	145.58 ksi	Eqn E3-4 - AISC 13th Edition, Section E3.		
		Elastic Critical Buckling Stress		
<b>Fcr =</b>	53.92 ksi	Eqn E3-2, AISC 13th Edition, Section E3		
		Critical Buckling Stress		
<b>Pn =</b>	438.10 k	Nominal Compressive Strength		
<b><math>\Phi P_n</math> =</b>	394.29 k	Allowable Compressive Strength	<b>Unity% =</b>	<b>82.3 %</b>

**Tension Rupture Check:**

AISC 13th Edition, Chapter J4.1

<b>Hole Size</b>	1.25			
<b>U =</b>	1			
<b>Ag =</b>	8.125 in <sup>2</sup>		Shear Lag Factor - Table D3.1 and TIA222-G	
<b>An =</b>	6.563 in <sup>2</sup>		Gross Area	
<b>Ae =</b>	6.563 in <sup>2</sup>		Net Area	
<b><math>\Phi R_n</math> =</b>	475.31 k		Effective Area	
			Tension Yielding: Eqn J4-1	
<b><math>\Phi R_n</math> =</b>	393.75 k		Tension Rupture: Eqn J4-2	
<b><math>\Phi R_n</math>(Equiv)</b>	393.75 ksi			
			<b>Unity%</b>	<b>82.4 %</b>

**Moment to Existing Bolt Group:**

<b>S<sub>BG</sub> =</b>	909.28 in <sup>3</sup>	<b># Bolts Acting</b>	14
<b>ft =</b>	35.97 ksi		
<b>Ab =</b>	.442 in <sup>2</sup>		
<b>T =</b>	222.50 k		
<b>Arm =</b>	44.38 ksi		
<b>M<sub>EQ</sub> =</b>	822.8 k-ft		

←-----Insert into Crown Spreadsheet



# Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 321952 Revision # 13

Reactions		
Mu	822.8	ft-kips
Axial, Pu:	42.981	kips
Shear, Vu:	35.507	kips
Elevation:	60	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
27.34

Pole Manufacturer: Other

Bolt Data		
Qty:	56	
Diameter (in.):	0.75	Bolt Fu: 150
Bolt Material:	A490	Bolt Fy: 130
N/A:		<-- Disregard
N/A:		<-- Disregard
Circle (in.):	44.375	

Plate Data		
Diam:	46.5	in
Thick, t:	2.25	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	2.36	in

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

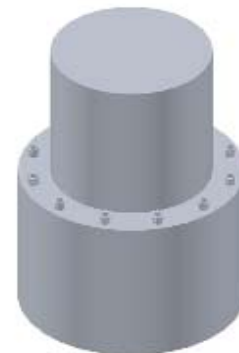
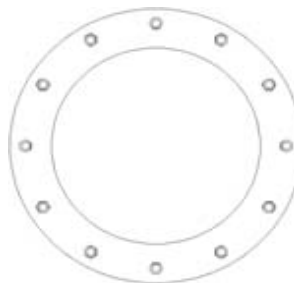
Pole Data		
Diam:	42	in
Thick:	0.5	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi
Reinf. Fillet Weld	0	"0" if None

If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Flange Bolt Results		Rigid
Bolt Tension Capacity, $\phi^* T_n, B1$ :	37.58 kips	$\phi^* T_n$
Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$ ), B:	37.56 kips	$\phi T_n [(1 - (V_u / \phi V_n)^2)^{0.5}]$
Max Bolt directly applied Tu:	15.13 Kips	
Min. PL "tc" for B cap. w/o Pry:	0.996 in	
Min PL "treq" for actual T w/ Pry:	0.491 in	
Min PL "t1" for actual T w/o Pry:	0.632 in	
T allowable w/o Prying:	37.58 kips	$\alpha < 0$ case
Prying Force, q:	0.00 kips	
Total Bolt Tension = Tu + q:	15.13 kips	
Non-Prying Bolt Stress Ratio, Tu/B:	40.3% Pass	

Exterior Flange Plate Results		Flexural Check	Rigid
Compression Side Plate Stress:	4.3 ksi		TIA G
Allowable Plate Stress:	32.4 ksi		$\phi^* F_y$
Compression Plate Stress Ratio:	13.2% Pass		Comp. Y.L. Length:
			14.32
<b>No Prying</b>			
Tension Side Stress Ratio, $(treq/t)^2$ :	4.8% Pass		

n/a  
**Stiffener Results**  
 Horizontal Weld : n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a  
**Pole Results**  
 Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

# Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 321952 Revision # 13

Manufacturer: Other

## Bolt Data

Qty:	56	Bolt Fu:	150
Diam:	0.75	Bolt Fy:	130
Bolt Material:	A490		
N/A:		<-- Disregard	
N/A:		<-- Disregard	
Circle:	44.375	in	

## Plate Data

Plate Outer Diam:	46.75	in
Plate Inner Diam:	42.25	in (Hole @ Ctr)
Thick:	2.25	in
Grade:	36	ksi
<b>Effective Width:</b>	2.62	in

## Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

## Pole Data

Pole OuterDiam:	48	in
Thick:	0.625	in
Pole Inner Diam:	46.75	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi

## Reactions

Moment:	822.8	ft-kips
Axial:	42.981	kips
Shear:	35.507	kips
Exterior Flange Run, T+q:	15.13	kips

## Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
27.34

Elevation: 60 feet

## Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 15.1 Kips, Ext. Flange Tu+q  
 Adjusted  $\phi^* T_n$  (due to  $V_u = V_u / Q_t$ ): 37.6 Kips  
 Bolt Stress Ratio: 40.3% **Pass**

## Interior Flange Plate Results

Controlling Bolt Axial Force: 16.7 Kips, Ext. Cu=Interior Cu  
 Plate Stress: 6.0 ksi  
 Allowable Plate Stress,  $\phi^* F_y$ : 32.4 ksi  
 Plate Stress Ratio: 18.4% **Pass**

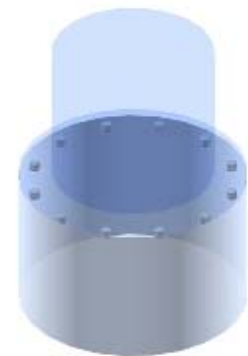
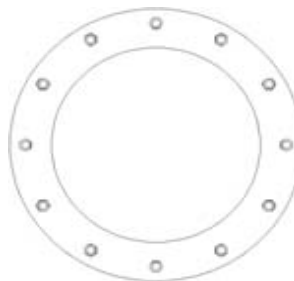
n/a

## Stiffener Results

Horizontal Weld : n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a

## Pole Results

Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

PROJECT	<b>86959.008.01 - Portland Warren Ave, ME</b>		
SUBJECT	<b>Exist/Prop Flat Plate Bridge Stiffeners @ 20'</b>		
DATE	<b>05/21/16</b>	PAGE	1 OF 1



0

**Determine Load to Bridge Stiffener:**

<b>M =</b>	<b>4229.9 k-ft</b>	From Risa Model	<b>Stiffener Width</b>	<b>6.500 in</b>
<b>I =</b>	<b>46471.2 in^4</b>	From AutoCAD Sketch	<b>Stiffener Thickness</b>	<b>1.250 in</b>
<b>ybar =</b>	<b>27.625 in</b>			
<b>S =</b>	<b>1682.22 in^3</b>	I/y	<b>Fy</b>	<b>65 ksi</b>
<b>fc =</b>	<b>30.17 ksi</b>	M/S	<b>Fu</b>	<b>80 ksi</b>
<b>Ag =</b>	<b>8.125 in^2</b>			
<b>Pu =</b>	<b>245.16 k</b>	fc x Ag	<b>Bolt Circle</b>	<b>50.38 in</b>
			<b>Number of Bolts</b>	<b>52</b>
			<b>Bolt Size</b>	<b>1</b>
			<b>Gap @ Flange</b>	<b>6.00 in</b>

**Determine  $\Phi P_n$  (Allowable Axial Load):**

<b>Pn = Fcr x Ag</b>		Eqn E3-1, AISC 13th Edition, Section E3.	
<b>K =</b>	<b>1</b>		
<b>I =</b>	<b>16.000 in</b>	Unsupported Length	
<b>Iy =</b>	<b>1.058 in^4</b>	Local Weak Axis Moment of Inertia	
<b>Ag =</b>	<b>8.125 in^2</b>	Stiffener Cross Sectional Area	
<b>ry =</b>	<b>.361 in</b>	Radius of Gyration (Weak Axis)	
<b>k/r =</b>	<b>44.34</b>		
<b>4.71 x <math>\sqrt{E/Fy}</math> =</b>	<b>99.49</b>	Limit State Equation for Flexural Buckling - AISC 13th Edition, Section E3.	
<b>Fe =</b>	<b>145.58 ksi</b>	Eqn E3-4 - AISC 13th Edition, Section E3.	
		Elastic Critical Buckling Stress	
<b>Fcr =</b>	<b>53.92 ksi</b>	Eqn E3-2, AISC 13th Edition, Section E3	
		Critical Buckling Stress	
<b>Pn =</b>	<b>438.10 k</b>	Nominal Compressive Strength	
<b><math>\Phi P_n</math> =</b>	<b>394.29 k</b>	Allowable Compressive Strength	<b>Unity% = 62.2 %</b>

**Tension Rupture Check:**

AISC 13th Edition, Chapter J4.1

<b>Hole Size</b>	<b>1.25</b>		
<b>U =</b>	<b>1</b>	Shear Lag Factor - Table D3.1 and TIA222-G	
<b>Ag =</b>	<b>8.125 in^2</b>	Gross Area	
<b>An =</b>	<b>6.563 in^2</b>	Net Area	
<b>Ae =</b>	<b>6.563 in^2</b>	Effective Area	
<b><math>\Phi R_n</math> =</b>	<b>475.31 k</b>	Tension Yielding: Eqn J4-1	
<b><math>\Phi R_n</math> =</b>	<b>393.75 k</b>	Tension Rupture: Eqn J4-2	
<b><math>\Phi R_n</math>(Equiv)</b>	<b>393.75 ksi</b>		<b>Unity% 62.3 %</b>

**Moment to Existing Bolt Group:**

<b>S<sub>BG</sub> =</b>	<b>1845.01 in^3</b>	<b># Bolts Acting</b>	<b>13</b>
<b>ft =</b>	<b>27.51 ksi</b>		
<b>Ab =</b>	<b>.785 in^2</b>		
<b>T =</b>	<b>280.90 k</b>		
<b>Arm =</b>	<b>50.38 ksi</b>		
<b>M<sub>EQ</sub> =</b>	<b>1179.2 k-ft</b>	<b>&lt;-----Insert into Crown Spreadsheet</b>	

# Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 321952 Revision # 13

Reactions		
Mu	1179.2	ft-kips
Axial, Pu:	64.391	kips
Shear, Vu:	39.494	kips
Elevation:	20	feet

Bolt Threads:	
X-Excluded	
$\phi V_n = \phi(0.55 A_b F_u)$	
$\phi = 0.75, \phi V_n$ (kips):	
38.88	

Pole Manufacturer: Other

If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Bolt Data		
Qty:	52	
Diameter (in.):	1	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:		<-- Disregard
N/A:		<-- Disregard
Circle (in.):	50.375	

Flange Bolt Results		Rigid	
Bolt Tension Capacity, $\phi T_n, B1$ :	54.54 kips	$\phi T_n$	
Adjusted $\phi T_n$ (due to $V_u = V_u / Q_t$ ), <b>B</b> :	54.53 kips	$\phi T_n [(1 - (V_u / \phi V_n)^2)^{0.5}]$	
Max Bolt directly applied $T_u$ :	20.37 Kips		
Min. PL "tc" for <b>B</b> cap. <b>w/o</b> Pry:	0.995 in		
Min PL "treq" for actual <b>T w/</b> Pry:	0.476 in		
Min PL "t1" for actual <b>T w/o</b> Pry:	0.608 in		
T allowable w/o Prying:	54.54 kips	$\alpha < 0$ case	
Prying Force, q:	0.00 kips		
Total Bolt Tension = $T_u + q$ :	20.37 kips		
Non-Prying Bolt Stress Ratio, $T_u / B$ :	37.4% <b>Pass</b>		

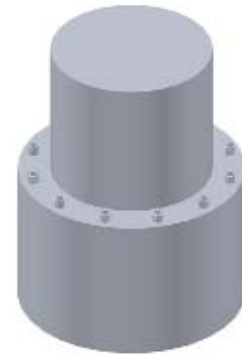
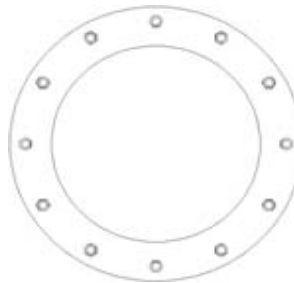
Plate Data		
Diam:	52.5	in
Thick, t:	2.5	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	2.90	in

Exterior Flange Plate Results		Flexural Check		Rigid	
Compression Side Plate Stress:	3.9 ksi			TIA G	
Allowable Plate Stress:	32.4 ksi			$\phi F_y$	
Compression Plate Stress Ratio:	12.0% <b>Pass</b>			Comp. Y.L. Length:	
				15.29	
<b>No Prying</b>					
Tension Side Stress Ratio, $(treq/t)^2$ :	3.6% <b>Pass</b>				

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

**n/a**  
**Stiffener Results**  
 Horizontal Weld : n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a  
**Pole Results**  
 Pole Punching Shear Check: n/a

Pole Data		
Diam:	48	in
Thick:	0.625	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi
Reinf. Fillet Weld	0	"0" if None



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

# Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 321952 Revision # 13

Manufacturer: Other

## Bolt Data

Qty:	52	Bolt Fu:	120
Diam:	1	Bolt Fy:	92
Bolt Material:	A325		
N/A:		<-- Disregard	
N/A:		<-- Disregard	
Circle:	50.375	in	

## Plate Data

Plate Outer Diam:	52.75	in
Plate Inner Diam:	48.25	in (Hole @ Ctr)
Thick:	2.5	in
Grade:	36	ksi
<b>Effective Width:</b>	3.19	in

## Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

## Pole Data

Pole OuterDiam:	54	in
Thick:	0.625	in
Pole Inner Diam:	52.75	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi

## Reactions

Moment:	1179.2	ft-kips
Axial:	64.391	kips
Shear:	39.494	kips
Exterior Flange Run, T+q:	20.37	kips

## Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi V_n$ (kips):
38.88

Elevation: 20 feet

## Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 20.4 Kips, Ext. Flange Tu+q  
 Adjusted  $\phi T_n$  (due to  $V_u = V_u / Q_t$ ): 54.5 Kips  
 Bolt Stress Ratio: 37.4% **Pass**

## Interior Flange Plate Results

Controlling Bolt Axial Force: 22.8 Kips, Ext. Cu=Interior Cu  
 Plate Stress: 5.4 ksi  
 Allowable Plate Stress,  $\phi F_y$ : 32.4 ksi  
 Plate Stress Ratio: 16.8% **Pass**

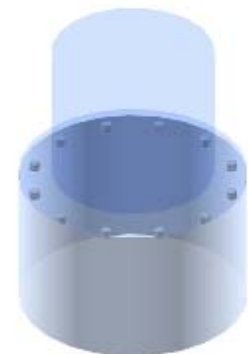
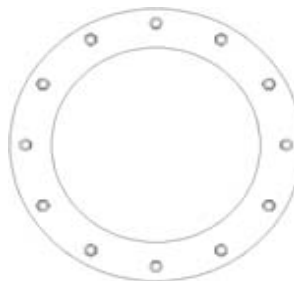
n/a

## Stiffener Results

Horizontal Weld : n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a

## Pole Results

Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

## Anchor Rod Information for TIA/EIA-222-F and TIA-222-G-2



Site Information	
ID:	878782
Name:	PORTLAND WARREN AVE
App. #:	321952 Revision # 13

Base Reactions	
Moment:	5033 ft-kip
Axial:	76 kip
Shear:	41 kip
Base Plate Type:	Circular

Design Information	
TIA Code:	G
ASIF:	1.000
Failure:	105%
eta Factor:	0.50

Original Anchor Rod Data	
Quantity:	28
Diameter:	2.00 in
Material:	A36
Bolt Circle:	60.1 in
Bolt Spacing:	in
Bolt Group Area:	87.96 in <sup>2</sup>
Bolt Group MOIx:	39749 in <sup>4</sup>

Reactions Seen by Original AR Group	
Moment:	4020.0 kip-ft
Axial:	75.7 kip
Shear:	40.9 kip

Original AR Capacity Check	
Combined Load:	120.2 kip
Allowable load:	115.9 kip
AR Capacity:	103.7% <span style="color: green;">Pass</span>

First Added Anchor Rod Data	
Quantity:	4
Diameter:	2.25 in
Material:	F1554 GR 105
Bolt Circle:	71.0 in
Bolt Group Area:	15.90 in <sup>2</sup>
Bolt Group MOIx:	10022 in <sup>4</sup>

Reactions Seen by First Added AR Group	
Moment:	1013.5 kip-ft
Axial:	0.0 kip
Shear:	0.0 kip

First Added AR Capacity Check	
Combined Load:	170.2 kip
Allowable load:	324.8 kip
AR Capacity:	52.4% <span style="color: green;">Pass</span>

Second Added Anchor Rod Data	
Quantity:	
Diameter:	in
Material:	
Bolt Circle:	in
Bolt Group Area:	0.00 in <sup>2</sup>
Bolt Group MOIx:	0 in <sup>4</sup>

Reactions Seen by Second Added AR Group	
Moment:	0.0 kip-ft
Axial:	0.0 kip
Shear:	0.0 kip

Second Added AR Capacity Check	
Combined Load:	0.0 kip
Allowable load:	0.0 kip
AR Capacity:	0.0%

Third Added Anchor Rod Data	
Quantity:	
Diameter:	in
Material:	
Bolt Circle:	in
Bolt Group Area:	0.00 in <sup>2</sup>
Bolt Group MOIx:	0 in <sup>4</sup>

Reactions Seen by Second Added AR Group	
Moment:	0.0 kip-ft
Axial:	0.0 kip
Shear:	0.0 kip

Second Added AR Capacity Check	
Combined Load:	0.0 kip
Allowable load:	0.0 kip
AR Capacity:	0.0%

# Stiffened or Unstiffened, UngROUTED, Circular Base Plate - Any Rod Mater

**TIA Rev G** Assumption: Clear space between bottom of leveling nut and top of concrete **not** exceeding (1)\*(l

## Site Data

BU#: 878782
Site Name: PORTLAND WARREN AV
App #: 321952 Revision # 13
Pole Manufacturer: Other

## Anchor Rod Data

Qty:	28	
Diam:	2	in
Rod Material:	Other	
Strength (Fu):	58	ksi
Yield (Fy):	36	ksi
Bolt Circle:	60.125	in

## Plate Data

Diam:	66	in
Thick:	3.25	in
Grade:	36	ksi
Single-Rod B-eff:	6.06	in

## Stiffener Data (Welding at both sides)

Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

## Pole Data

Diam:	54	in
Thick:	0.625	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi
Reinf. Fillet Weld	0	"0" if None

## Reactions

Mu:	4019.9554	ft-kips
Axial, Pu:	75.7457	kips
Shear, Vu:	40.897139	kips
Eta Factor, η	0.5	TIA G (Fig. 4-4)

If No stiffeners, Criteria: AISC LRFD <-Only Applicable to Unstiffene

## Anchor Rod Results

Max Rod (Cu+ Vu/η):	120.2 Kips
Allowable Axial, Φ*Fu*Anet:	116.0 Kips
Anchor Rod Stress Ratio:	103.7% <b>Pass</b>

## Base Plate Results

	Flexural Check
Base Plate Stress:	14.0 ksi
Allowable Plate Stress:	32.4 ksi
Base Plate Stress Ratio:	43.1% <b>Pass</b>

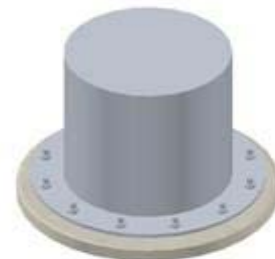
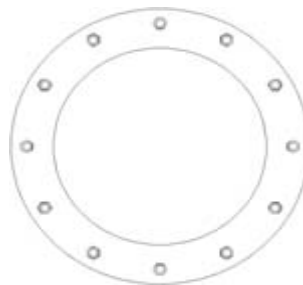
n/a

## Stiffener Results

Horizontal Weld :	n/a
Vertical Weld:	n/a
Plate Flex+Shear, fb/Fb+(fv/Fv)^2:	n/a
Plate Tension+Shear, ft/Ft+(fv/Fv)^2:	n/a
Plate Comp. (AISC Bracket):	n/a

## Pole Results

Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Proj. Number 86959.008.01  
Proj. Name PORTLAND WARREN AVE, ME  
Code Rev. G

**Proposed Anchor Rods**

Diameter	2.25	in
Grade	F1554-105	
Quantity	4	
Bolt Circle	71	in
AR Capacity	325	kips

**Tower Properties**

F <sub>y pole</sub>	36	ksi
F <sub>u pole</sub>	58	ksi
F <sub>y base</sub>	36	ksi
F <sub>u base</sub>	58	ksi

**Existing Anchor Rods**

Diameter	2	in
Quantity	28	
Bolt Circle	60.125	in

**Foundation Properties**

Type	Pad	
Pad Thickness	5	ft
f' <sub>c</sub>	4000	psi
Clear Cover	3	inch
Pad Width	12	ft
	10	
	18	
	3	
	60	
Seismic controlled?	<input type="checkbox"/>	

Summary Output	
<b>- Anchor Rod Checks</b>	
Specified Embedment Depth:	AR is too large for existing pad thickness
Min. Pull Test Value:	190
6 inch Tape Length	No Good
<b>- Anchor Rod Bracket Checks</b>	
Tube Stress:	99.6%
Bracket Plate Check:	OK
Max. Weld Stress:	72.0%

**Anchor Rod Bracket Properties**

**Gusset Properties**

Thickness	1.25	inch
Pole to Tube CL	8.5	inch
Height	36	inch
Width at Tube	6	inch
F <sub>y plate</sub>	65	ksi
F <sub>u plate</sub>	80	ksi
Gap	0	inch
Notch	0.75	inch

**Pipe /Tube Properties**

Size	HSS5x5x1/2	
L <sub>pipe</sub>	33	inch
F <sub>y pipe</sub>	46	ksi
D <sub>pipe</sub>	5	inch
t <sub>pipe</sub>	0.5	inch
A <sub>pipe</sub>	7.88	inch <sup>2</sup>
I <sub>pipe</sub>	26	inch <sup>4</sup>
r <sub>pipe</sub>	1.82	inch

**Weld Properties**

F <sub>EXX</sub>	70	ksi	Weld Material Grade
<b>- Bracket to Tube Weld</b>			
D <sub>v pipe</sub>	6		Vertical fillet weld size in sixteenths
l <sub>weld pipe</sub>	33	inch	Length of Vertical Weld to Pipe
<b>- Bracket to Pole Weld</b>			
D <sub>v pole</sub>	6		Vertical fillet weld size in sixteenths
H	36	inch	Height of vertical weld from base plate
<b>- Base Plate Welds</b>			
D <sub>Hbp</sub>	0.5625	inch	Gusset Bevel Size
D <sub>Hp</sub>	8		Pipe to Baseplate weld in sixteenths

**Additional Variables**

C <sub>1</sub>	1.00	Electrode Strength Coefficient
k <sub>rt</sub>	0	Transverse Reinforcement Index :
ψ <sub>t</sub>	1	Rebar Location Factor :
ψ <sub>e</sub>	1	Rebar Coatig Factor :
ψ <sub>s</sub>	1	Rebar Size Factor :
λ	1	Concrete Weight Factor :
S <sub>b</sub>	1325	psi Epoxy Bond Strength:



PROJECT **86959.008.01 - Portland Warren Ave, ME**  
 SUBJECT **Foundation Analysis**  
 DATE **05/21/16**

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**B+T GRP**  
 1717 S. Boulder, Suite 300  
 Tulsa, OK 74119  
 (918) 587-4630

**Weight of Concrete**

$$W_c = \gamma * w_1 * w_2 * D$$

$$= .15 * 12 * 12 * 5$$

$$= 108 \text{ kips}$$

**MOI of Anchor Group**

$$I/A = \Sigma n * d^2$$

$$= [2 * 14 * 5.6'^2 + 2 * (4.7'^2 + 3.9'^2 + 3.0'^2 + 2.15'^2 + 1.3'^2 + 0.43'^2)] * 144$$

$$= 156854.82 \text{ in}^4/\text{in}^2$$

**Effective Moment at Anchors**

$$M_e = M + V * D$$

$$= 5033 + 41 * 5$$

$$= 5238 \text{ k-ft}$$

**Max Comp. in Anchor**

$$C_u = (P + \phi W_c) / N + M_e * c / (I/A)$$

$$= (71k + 1 * 108k) / 52 + (5148 * 12)k\text{-in} * (7.95 * 12)\text{in} / (156854 \text{in}^4/\text{in}^2)$$

$$= 41.8 \text{ kips}$$

**Max Tension in Anchor**

$$T_u = (-P + \phi W_c) / N + M_e * c / (I/A)$$

$$= (-71k + 9 * 108k) / 52 + (5148 * 12)k\text{-in} * (7.95 * 12)\text{in} / (156854 \text{in}^4/\text{in}^2)$$

$$= 38.6 \text{ kips}$$

**Axial Capacity of Anchor**

$$\phi P_n = \phi F_y * A_y$$

$$= 0.9 * 60 \text{ksi} * 1.0 \text{in}^2$$

$$= 54.0 \text{ kips}$$

**% Capacity**

$$= \underline{\underline{77.3\%}}$$

**Rock to Grout Bond**

$$P_{RG} = \phi * S_A * F_b$$

$$= 0.5 * 2.5 \text{in} * \pi * (45 \text{ksi} * 8 \text{ft} * 12)$$

$$= 169.6 \text{ kips}$$

Ultimate Bond Strength  
 450 psi

**% Capacity**

$$= \underline{\underline{22.8\%}}$$

**Factored Loads**

M	5033 k-ft
P	76 k
V	41 k

**Block**

W1	12 ft
W2	12 ft
D	5 ft

**Anchor**

Size	1.128
Qty	14 per face
Spacing	10.77 in
Grade	60 ksi
Hole Size	2.5 in

### Steel to Grout Bond

$$\begin{aligned}
 P_{RG} &= \phi * SA * F_b \\
 &= 0.5 * 1.125 \text{ in} * \pi * (.32 \text{ ksi} * 8 \text{ ft} * 12) \\
 &= 54.4 \text{ kips}
 \end{aligned}$$

### Steel-to-Grout Bond

$$\begin{aligned}
 &4.2 * \text{sqrt}(f'_c) \\
 &- f'_c \text{ of SikaGrout 212 } \geq 5800 \text{ psi} \\
 &= 320 \text{ psi}
 \end{aligned}$$

### % Capacity

$$= \underline{\underline{99.2\%}}$$

### Rock Group Forces

Moment Resistance from Concrete Weighth

$$\begin{aligned}
 \phi M_c &= 0.9 * 108 \text{ k} * 2.8284 \text{ ft} \\
 &= 274.9 \text{ k-ft (Diagonal)}
 \end{aligned}$$

$$\begin{aligned}
 \phi M_c &= 0.9 * 108 \text{ k} * 6 \text{ ft} \\
 &= 583.2 \text{ k-ft (Orthogonal)}
 \end{aligned}$$

Group Uplift Force

$$\begin{aligned}
 &\text{Diagonal} \\
 U_{gd} &= 560.8 \text{ kips}
 \end{aligned}$$

$$\begin{aligned}
 &\text{Orthogonal} \\
 U_{go} &= 455.5 \text{ kips}
 \end{aligned}$$

### Rock Group Weight

$$\begin{aligned}
 \phi R_w &= \phi * Vol * \gamma_{rock} \\
 &= 0.75 * 581.6 \text{ ft}^3 * 0.16 \text{ kcf} \\
 &= 69.8 \text{ kips}
 \end{aligned}$$

### Rock Shear Strength

$$\begin{aligned}
 \phi R_s &= \phi * SA * v_{rock} * \cos(30) \\
 &= 576.8 \text{ kips}
 \end{aligned}
 \quad
 \begin{aligned}
 \phi & 0.75 \\
 SA & 222 \text{ ft}^2 \\
 v_{rock} & 4 \text{ ksf}
 \end{aligned}$$

### % Capacity

$$= \underline{\underline{86.7\%}}$$

### Soil Bearing

$$\begin{aligned}
 \sigma &= P/A + M/S \\
 &= 76 / 12^2 + 5033 / 203.6 \\
 &= 25.2 \text{ ksf}
 \end{aligned}$$

$$\begin{aligned}
 q_{all} &= 30 \text{ ksf} \\
 &= \frac{S = (12^3 / 6 / \text{sqrt}(2))}{203.6} \text{ ft}^3
 \end{aligned}$$

### % Capacity

$$= \underline{\underline{84.1\%}}$$