



March 4, 2013

Mr. Steve Tuttle  
Crown Castle  
8 Parkmeadow Drive  
Pittsford, NY 14534  
(585) 899-3445

B+T Group  
1717 S. Boulder, Suite 300  
Tulsa, OK 74119  
(918) 587-4630  
ctuttle@btgrp.com

**Subject:** Structural Modification Report

**Carrier Designation:** *Sprint PCS Co-Locate*  
**Carrier Site Number:** NM03XC066  
**Carrier Site Name:** NM03XC066

**Crown Castle Designation:**  
**Crown Castle BU Number:** 878782  
**Crown Castle Site Name:** 188 Warren Ave  
**Crown Castle JDE Job Number:** 191399  
**Crown Castle Work Order Number:** 580875  
**Crown Castle Application Number:** 164923 Rev. 1

**Engineering Firm Designation:** B+T Group Project Number: 86959.001.01

**Site Data:** 188 Warren Ave, Portland, ME, Cumberland County  
Latitude 43° 41' 15.16", Longitude -70° 18' 14.96"  
180 Foot - Monopole

Dear Mr. Tuttle,

B+T Group is pleased to submit this "Structural Modification Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 525004, in accordance with application 164923, revision 1.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC4: TSA specified load case with proposed modifications **Sufficient Capacity**  
Note: See Table 1 and Table 2 for the proposed and existing/reserved loading, respectively.

The analysis has been performed in accordance with the TIA-222-G standard and the local code requirements based upon a wind speed of 100 mph 3-second gust, exposure category C.

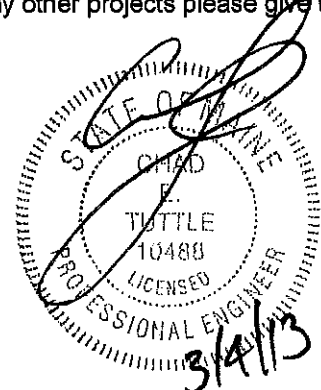
All modifications and equipment proposed in this report shall be installed in accordance with the attached drawings for the determined available structural capacity to be effective.

We at B+T Group appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Respectfully submitted by:  
B+T Engineering, Inc.

Kiran K. Maroju, E.I.  
Project Engineer

Chad E. Tuttle, P.E.  
President



## TABLE OF CONTENTS

### 1) INTRODUCTION

### 2) ANALYSIS CRITERIA

Table 1 - Proposed Antenna and Cable Information

Table 2 - Existing and Reserved Antenna and Cable Information

Table 3 - Design Antenna and Cable Information

### 3) ANALYSIS PROCEDURE

Table 4 - Documents Provided

3.1) Analysis Method

3.2) Assumptions

### 4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

Table 6 - Tower Component Stresses vs. Capacity

4.1) Recommendations

### 5) APPENDIX A

tnxTower Output

### 6) APPENDIX B

Base Level Drawing

### 7) APPENDIX C

Additional Calculations

### 8) APPENDIX D

Tower Modification Drawings

## 1) INTRODUCTION

This tower is a 180 ft. Monopole designed by Pittsburg Monopole in February of 1997. The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-F. This tower has been modified by Crown Castle in 2012 and those modifications were incorporated in this analysis.

## 2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA-222-G Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a 3-second gust wind speed of 100 mph with no ice, 40 mph with 1 inch ice thickness and 60 mph under service loads, exposure category C.

**Table 1 - Proposed Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
177.0	179.0	1	RFS Celwave	APXV9ERR18-C-A20	3	1-1/4	
		2	RFS Celwave	APXVSP18-C-A20			
		3	RFS Celwave	IBC1900BB-1			
		3	RFS Celwave	IBC1900HG-2A			
175.0	176.0	3	Alcatel Lucent	800MHz 2X50W RRH W/FILTER	--	--	--
		6	Alcatel Lucent	PCS 1900MHz 4x45W-65MHz			
	175.0	1	--	Side Arm Mount [SO 102-3]			

**Table 2 - Existing and Reserved Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note	
177.0	179.0	6	Allgon	7184.15	6	1-5/8	3	
	177.0	1	--	Platform Mount [LP 715-1]	--	--	1	
171.0	171.0	6	Dapa	58010	6	1-5/8	1	
		1	--	Platform Mount [LP 401-1]				
161.0	162.0	2	KMW	AM-X-CD-16-65-00T-RET	2	3/4 3/8	2	
		6	Powerwave	7020.00				
		1	Powerwave	P65-17-XLH-RR				
		1	Raycap	DC6-48-60-18-8F				
	161.0	161.0	6	Powerwave	7770.00	12	1-5/8	1
			6	Powerwave	LGP2140X			
			1	--	T-Arm Mount [TA 602-3]			
159.0	160.0	6	Ericsson	RRUS-11	--	--	2	
	159.0	1	--	Side Arm Mount [SO 701-3]				

Notes:

- 1) Existing Equipment
- 2) Reserved Equipment
- 3) Equipment to be Removed

**Table 3 - Design Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
180	180	12	Generic	Antenna ( 4 sq. ft)	--	--
170	170	2	Generic	6' Dish	--	--
160	160	12	Generic	Antenna ( 4 sq. ft)	--	--

### 3) ANALYSIS PROCEDURE

**Table 4 - Documents Provided**

Document	Remarks	Reference	Source
Online Application	Sprint Co-Locate Revision# 1	164923	CCI Sites
Tower Manufacturing Drawing	Pittsburg Monopole Division, Date:2/7/97	1451234	CCI Sites
Tower Modification Drawing	Crown Castle, Date:04/24/12	3160195	CCI Sites
Modification Inspection Report	TEP, Project No:127768	3360128	CCI Sites
Foundation Drawing	Pittsburg Monopole Division, Date:2/7/97	1480918	CCI Sites
Geotech Report	Gemini Geotechnical Associates, Project No.96127ME	1562092	CCI Sites
Antenna Configuration	Previous SA by Crown Castle, Project No:539485	3353442	CCI Sites

#### 3.1) Analysis Method

tnxTower (version 6.0.4.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

#### 3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Mount areas and weights are assumed based on photographs provided.

This analysis may be affected if any assumptions are not valid or have been made in error. B+T Group should be notified to determine the effect on the structural integrity of the tower.

#### 4) ANALYSIS RESULTS

**Table 5 - Section Capacity (Summary) - LC4**

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	180 - 140	Pole	P24x3/8	1	-12.287	901.775	91.2	Pass
L2	140 - 100	Pole	P36x1/2	2	-22.818	1806.730	80.2	Pass
L3	100 - 65	Pole	P42x1/2	3	-33.596	2112.090	99.1	Pass
L4	65 - 60	Pole	P42x.7333	4	-35.759	2891.950	71.9	Pass
L5	60 - 20	Pole	P48x5/8	5	-52.753	3013.870	95.7	Pass
L6	20 - 0	Pole	P54x5/8	6	-62.031	3395.570	90.9	Pass
							Summary	
						Pole (L3)	99.1	Pass
						<b>RATING =</b>	<b>99.1</b>	<b>Pass</b>

**Table 6 - Tower Component Stresses vs. Capacity - LC4**

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Bridge Stiffeners	140	86.1	Pass
1,2	Flange Bolts	100	100.6	Pass
1	Flange Plate	100	42.9	Pass
1	Bridge Stiffeners	60	86.0	Pass
1	Flange Bolts	60	48.1	Pass
1	Flange Plate	60	21.4	Pass
1	Bridge Stiffeners	20	88.3	Pass
1	Flange Bolts	20	61.7	Pass
1	Flange Plate	20	26.3	Pass
1,2	Anchor Rods	Base	101.2	Pass
1	Base Plate	Base	42.3	Pass
1	Base Foundation	Base	50.7	Pass

<b>Structure Rating (max from all components) =</b>	<b>101.2.%</b>
---	----------------

Notes:

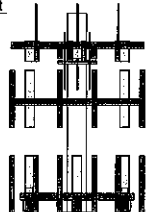
- 1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.
- 2) Capacities up to 105% are considered acceptable based on analysis methods used.

#### 4.1) Recommendations

- 1) All modifications proposed in this report shall be installed in accordance with the attached drawings (Appendix D) for the determined available structural capacity to be effective.

**APPENDIX A**  
**tnxTOWER OUTPUT**

Section	1	P24x3/8	40.000	A36	3.8	180.0 ft
Section	2	P36x1/2	40.000	A36	7.6	140.0 ft
Section	3	P42x1/2	35.000	A36	7.8	100.0 ft
Section	4	P42x7/32	5.000	A36	1.6	65.0 ft
Section	5	P48x5/8	40.000	A36	12.7	60.0 ft
Section	6	P54x5/8	20.000	A36	7.1	20.0 ft
Section					40.6	0.0 ft
Length (ft)						
Grade						
Weight (K)						



**DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
Lighting Rod 3/4" x 5'	183	Side Arm Mount [SO 102-3] (P)	175
APXVSP18-C-A20 w/ Mount Pipe (P)	177	6' x 2" Mount Pipe (E)	175
APXVSP18-C-A20 w/ Mount Pipe (P)	177	6' x 2" Mount Pipe (E)	175
APXVSP18-C-A20 w/ Mount Pipe (P)	177	6' x 2" Mount Pipe (E)	175
APXVSP18-C-A20 w/ Mount Pipe (P)	177	(2) 58010 w/ Mount Pipe (E)	171
APXVSP18-C-A20 w/ Mount Pipe (P)	177	(2) 58010 w/ Mount Pipe (E)	171
APXVSP18-C-A20 w/ Mount Pipe (P)	177	(2) 58010 w/ Mount Pipe (E)	171
IBC1900BB-1 (P)	177	Platform Mount [LP 401-1] (E)	171
IBC1900BB-1 (P)	177	(2) 7770.00 w/ Mount Pipe (E)	161
IBC1900BB-1 (P)	177	(2) 7770.00 w/ Mount Pipe (E)	161
IBC1900HG-2A (P)	177	(2) 7770.00 w/ Mount Pipe (E)	161
IBC1900HG-2A (P)	177	(2) 7770.00 w/ Mount Pipe (E)	161
IBC1900HG-2A (P)	177	(2) LGP2140X (E)	161
IBC1900HG-2A (P)	177	(2) LGP2140X (E)	161
Platform Mount [LP 715-1] (E)	177	(2) LGP2140X (E)	161
4' x 2" Pipe Mount (E)	177	(2) LGP2140X (E)	161
4' x 2" Pipe Mount (E)	177	P65-17-XLH-RR w/ Mount Pipe (R)	161
4' x 2" Pipe Mount (E)	177	AM-X-CD-16-65-00T-RET w/ Mount Pipe (R)	161
800MHz 2X50W RRH W/FILTER (P)	175	AM-X-CD-16-65-00T-RET w/ Mount Pipe (R)	161
800MHz 2X50W RRH W/FILTER (P)	175	(2) 7020.00 (R)	161
800MHz 2X50W RRH W/FILTER (P)	175	(2) 7020.00 (R)	161
(2) PCS 1900MHz 4x45W-65MHz (P)	175	(2) 7020.00 (R)	161
(2) PCS 1900MHz 4x45W-65MHz (P)	175	DC6-48-60-18-8F (R)	161
(2) PCS 1900MHz 4x45W-65MHz (P)	175	T-Arm Mount [TA 602-3] (R)	161
(2) PCS 1900MHz 4x45W-65MHz (P)	175	(2) RRUS 11 (R)	159
(2) PCS 1900MHz 4x45W-65MHz (P)	175	(2) RRUS 11 (R)	159
		Side Arm Mount [SO 701-3] (R)	159
		(2) RRUS 11 (R)	159

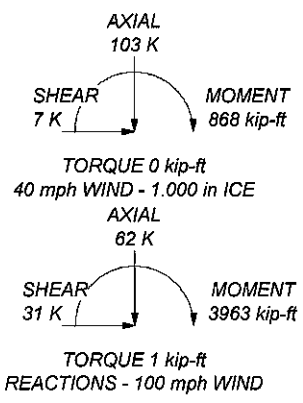
**MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A36	36 ksi	58 ksi	33.8 ksi	34 ksi	65 ksi

**TOWER DESIGN NOTES**

1. Tower is located in Cumberland County, Maine.
2. Tower designed for Exposure C to the TIA-222-G Standard.
3. Tower designed for a 100 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 40 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.000 ft
8. TOWER RATING: 99.1%

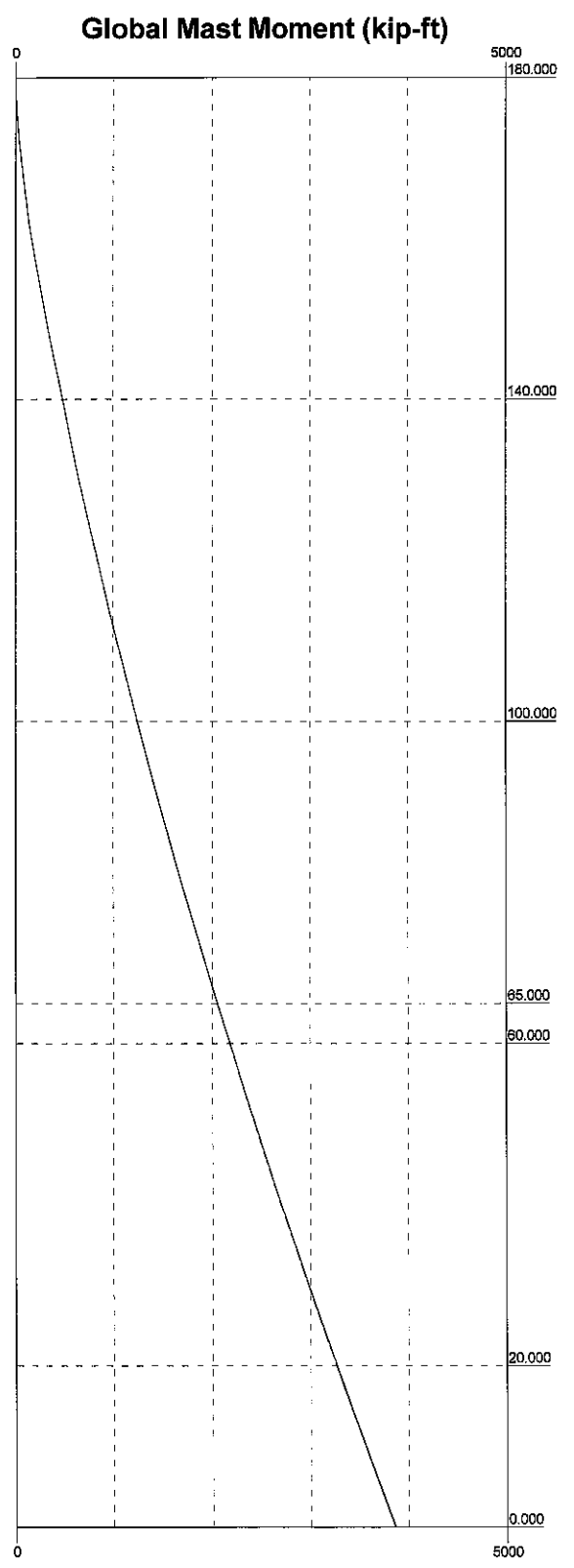
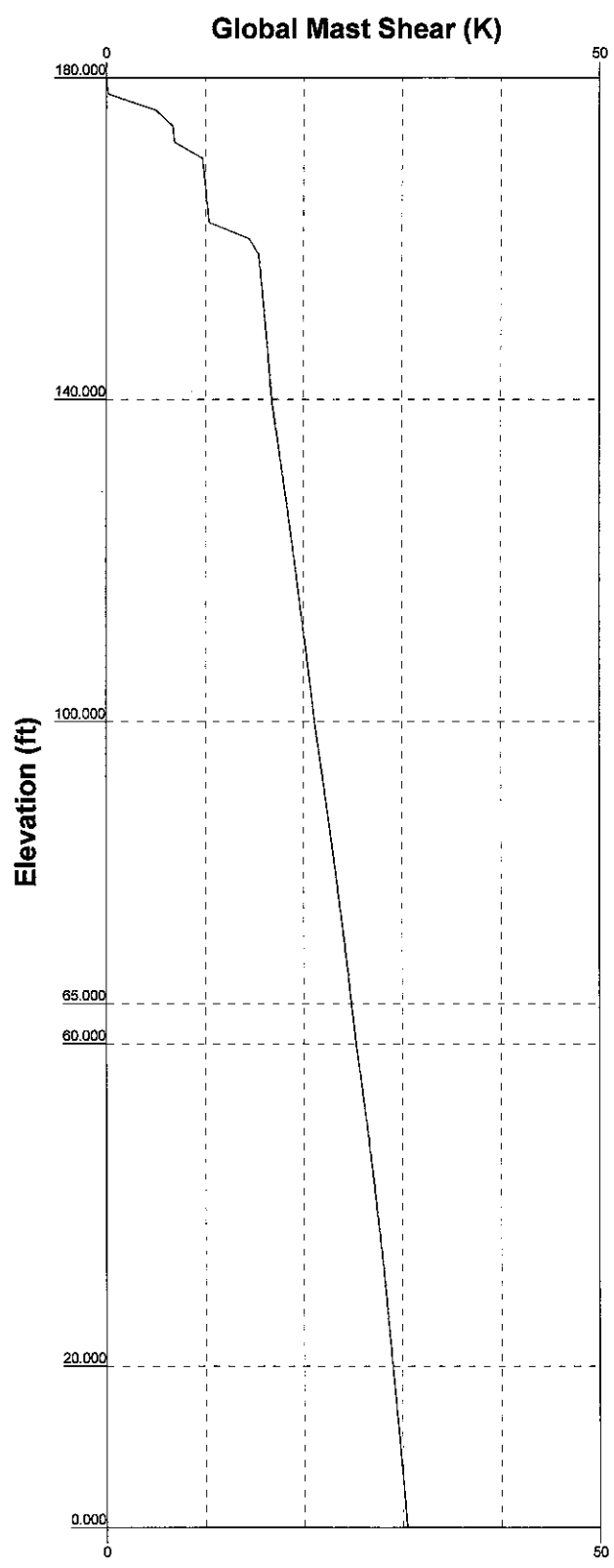
ALL REACTIONS ARE FACTORED




<p><b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265</p>	Job: <b>86959.001.01 - Portland Warren Ave, ME(BU# 878)</b>
	Project: <b>180' Monopole / App Id:164923 Rev: 1</b>
	Client: Crown Castle    Drawn by: HKarande    App'd:
	Code: TIA-222-G    Date: 03/01/13    Scale: NTS
	Path:    Dwg No E-1

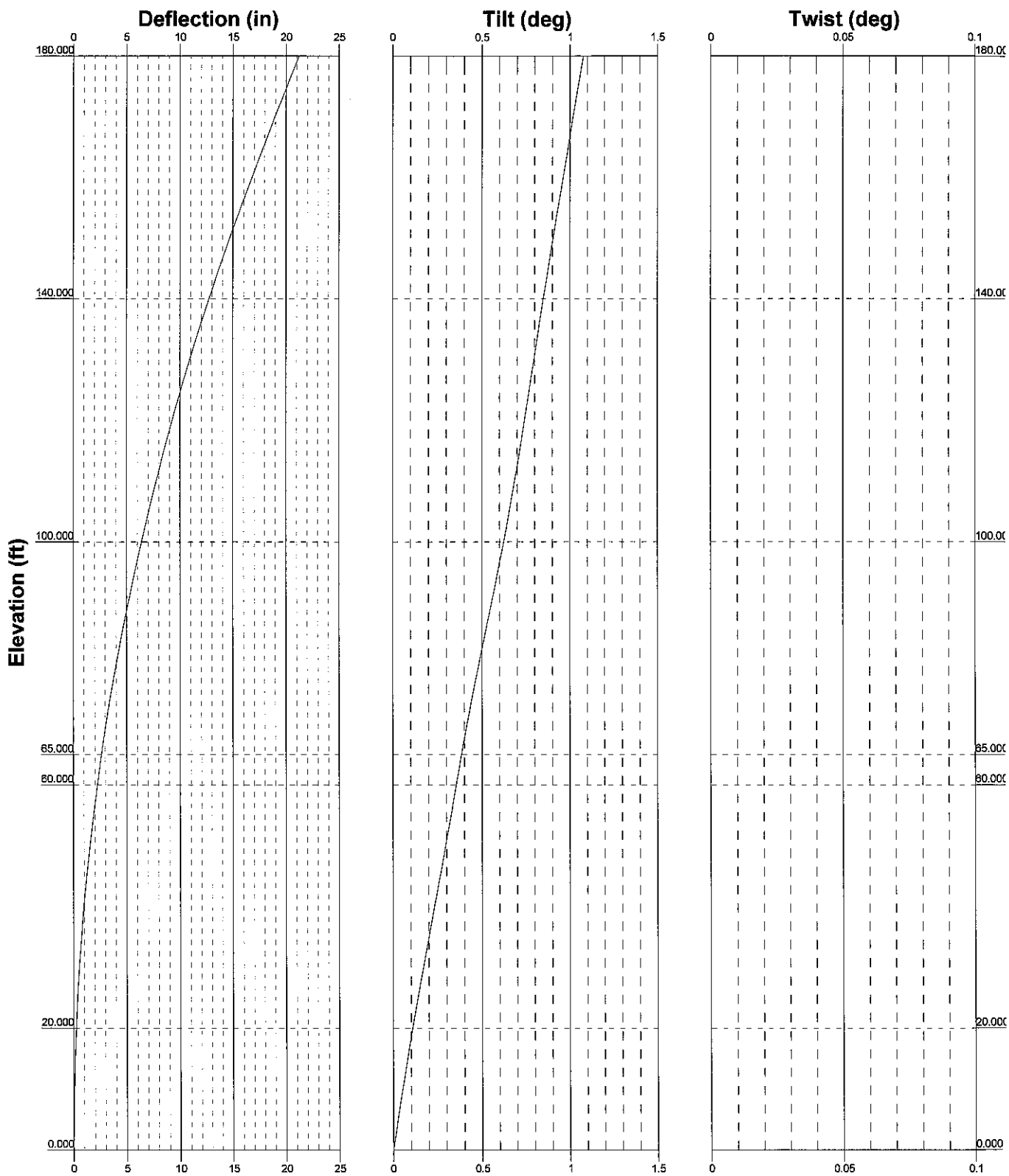
—— Vx      - - - - Vz


—— Mx      - - - - Mz

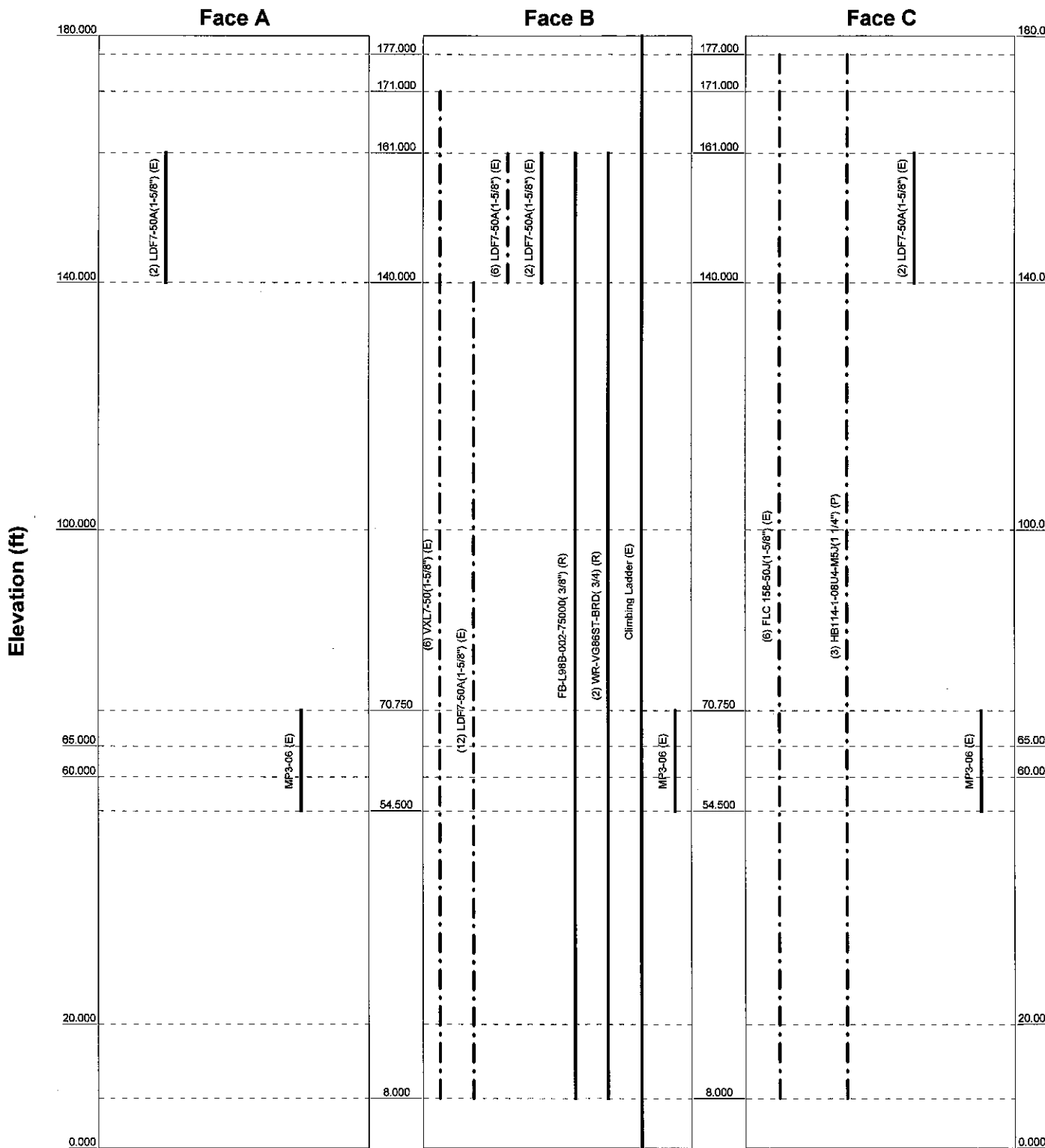



 <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job: 86959.001.01 - Portland Warren Ave, ME/BU# 878</b>		
	<b>Project: 180' Monopole / App Id:164923 Rev: 1</b>		
	Client: Crown Castle	Drawn by: HKarande	App'd:
	Code: TIA-222-G	Date: 03/01/13	Scale: NTS
	Path:	Dwg No. E-4	





 <p><b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265</p>	Job: <b>86959.001.01 - Portland Warren Ave, ME(BU# 878)</b>		
	Project: <b>180' Monopole / App Id:164923 Rev: 1</b>		
	Client: <b>Crown Castle</b>	Drawn by: <b>HKarande</b>	App'd:
	Code: <b>TIA-222-G</b>	Date: <b>03/01/13</b>	Scale: <b>NTS</b>
Path:	Dwg No. <b>E-5</b>		



 <p><b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265</p>	<b>Job: 86959.001.01 - Portland Warren Ave, ME(BU# 878)</b>		
	<b>Project: 180' Monopole / App Id:164923 Rev: 1</b>		
	Client: Crown Castle	Drawn by: HKarande	App'd:
	Code: TIA-222-G	Date: 03/01/13	Scale: NTS
	Path:	Dwg No. E-7	

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 86959.001.01 - Portland Warren Ave, ME(BU# 878782)	<b>Page</b> 1 of 10
	<b>Project</b> 180' Monopole / App Id:164923 Rev: 1	<b>Date</b> 10:45:15 03/01/13
	<b>Client</b> Crown Castle	<b>Designed by</b> HKarande

**Tower Input Data**

There is a pole section.  
This tower is designed using the TIA-222-G standard.  
The following design criteria apply:  
Tower is located in Cumberland County, Maine.  
Basic wind speed of 100 mph.  
Structure Class II.  
Exposure Category C.  
Topographic Category 1.  
Crest Height 0.000 ft.  
Nominal ice thickness of 1.000 in.  
Ice thickness is considered to increase with height.  
Ice density of 56.000 pcf.  
A wind speed of 40 mph is used in combination with ice.  
Temperature drop of 50.000 °F.  
Deflections calculated using a wind speed of 60 mph.  
A non-linear (P-delta) analysis was used.  
Pressures are calculated at each section.  
Stress ratio used in pole design is 1.  
Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

**Pole Section Geometry**

Section	Elevation ft	Section Length ft	Pole Size	Pole Grade	Socket Length ft
L1	180.000-140.000	40.000	P24x3/8	A36 (36 ksi)	
L2	140.000-100.000	40.000	P36x1/2	A36 (36 ksi)	
L3	100.000-65.000	35.000	P42x1/2	A36 (36 ksi)	
L4	65.000-60.000	5.000	P42x.7333	33.8 ksi (34 ksi)	
L5	60.000-20.000	40.000	P48x5/8	A36 (36 ksi)	
L6	20.000-0.000	20.000	P54x5/8	A36 (36 ksi)	

Tower Elevation ft	Gusset Area (per face) ft <sup>2</sup>	Gusset Thickness in	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in
L1 180.000-140.000				1	1	1		
L2 140.000-100.000				1	1	1		
L3 100.000-65.000				1	1	1		
L4 65.000-60.000				1	1	1		



<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 86959.001.01 - Portland Warren Ave, ME(BU# 878782)	<b>Page</b> 3 of 10
	<b>Project</b> 180' Monopole / App Id:164923 Rev: 1	<b>Date</b> 10:45:15 03/01/13
	<b>Client</b> Crown Castle	<b>Designed by</b> HKarande

**Feed Line/Linear Appurtenances Section Areas**

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
L1	180.000-140.000	A	0.000	0.000	8.316	0.000	0.034
		B	0.000	0.000	24.394	0.000	0.423
		C	0.000	0.000	8.316	0.000	0.359
L2	140.000-100.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	19.767	0.000	0.743
		C	0.000	0.000	0.000	0.000	0.350
L3	100.000-65.000	A	0.000	0.000	6.603	0.000	0.000
		B	0.000	0.000	23.899	0.000	0.650
		C	0.000	0.000	6.603	0.000	0.307
L4	65.000-60.000	A	0.000	0.000	5.742	0.000	0.000
		B	0.000	0.000	8.213	0.000	0.093
		C	0.000	0.000	5.742	0.000	0.044
L5	60.000-20.000	A	0.000	0.000	6.316	0.000	0.000
		B	0.000	0.000	26.083	0.000	0.743
		C	0.000	0.000	6.316	0.000	0.350
L6	20.000-0.000	A	0.000	0.000	0.000	0.000	0.000
		B	0.000	0.000	8.330	0.000	0.247
		C	0.000	0.000	0.000	0.000	0.105

**Feed Line/Linear Appurtenances Section Areas - With Ice**

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
L1	180.000-140.000	A	2.342	0.000	0.000	22.692	0.000	0.377
		B		0.000	0.000	80.453	0.000	1.759
		C		0.000	0.000	22.692	0.000	0.701
L2	140.000-100.000	A	2.276	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	80.489	0.000	2.023
		C		0.000	0.000	0.000	0.000	0.350
L3	100.000-65.000	A	2.192	0.000	0.000	8.200	0.000	0.134
		B		0.000	0.000	76.728	0.000	1.839
		C		0.000	0.000	8.200	0.000	0.440
L4	65.000-60.000	A	2.132	0.000	0.000	7.102	0.000	0.112
		B		0.000	0.000	16.695	0.000	0.349
		C		0.000	0.000	7.102	0.000	0.156
L5	60.000-20.000	A	2.042	0.000	0.000	7.765	0.000	0.117
		B		0.000	0.000	82.160	0.000	1.938
		C		0.000	0.000	7.765	0.000	0.467
L6	20.000-0.000	A	1.775	0.000	0.000	0.000	0.000	0.000
		B		0.000	0.000	25.479	0.000	0.590
		C		0.000	0.000	0.000	0.000	0.105

**Feed Line Center of Pressure**

Section	Elevation ft	CP <sub>X</sub> in	CP <sub>Z</sub> in	CP <sub>X</sub> Ice in	CP <sub>Z</sub> Ice in
L1	180.000-140.000	0.305	-0.256	0.336	-0.451
L2	140.000-100.000	0.389	-0.444	0.592	-1.224
L3	100.000-65.000	0.344	-0.395	0.564	-1.167

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 86959.001.01 - Portland Warren Ave, ME(BU# 878782)	<b>Page</b> 4 of 10
	<b>Project</b> 180' Monopole / App Id:164923 Rev: 1	<b>Date</b> 10:45:15 03/01/13
	<b>Client</b> Crown Castle	<b>Designed by</b> HKarande

Section	Elevation	CP <sub>x</sub>	CP <sub>z</sub>	CP <sub>x</sub> Ice	CP <sub>z</sub> Ice
	ft	in	in	in	in
L4	65.000-60.000	0.211	-0.242	0.373	-0.769
L5	60.000-20.000	0.358	-0.412	0.595	-1.223
L6	20.000-0.000	0.398	-0.359	0.686	-0.991

### Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>a</sub> No Ice	K <sub>a</sub> Ice
L1	8	LDF7-50A(1-5/8")	140.00 - 161.00	1.0000	1.0000
L1	9	LDF7-50A(1-5/8")	140.00 - 161.00	1.0000	1.0000
L1	10	LDF7-50A(1-5/8")	140.00 - 161.00	1.0000	1.0000
L1	11	FB-L98B-002-75000( 3/8")	140.00 - 161.00	1.0000	1.0000
L1	12	WR-VG86ST-BRD( 3/4)	140.00 - 161.00	1.0000	1.0000
L1	14	Climbing Ladder	140.00 - 180.00	1.0000	1.0000
L2	11	FB-L98B-002-75000( 3/8")	100.00 - 140.00	1.0000	1.0000
L2	12	WR-VG86ST-BRD( 3/4)	100.00 - 140.00	1.0000	1.0000
L2	14	Climbing Ladder	100.00 - 140.00	1.0000	1.0000
L3	11	FB-L98B-002-75000( 3/8")	65.00 - 100.00	1.0000	1.0000
L3	12	WR-VG86ST-BRD( 3/4)	65.00 - 100.00	1.0000	1.0000
L3	14	Climbing Ladder	65.00 - 100.00	1.0000	1.0000
L3	16	MP3-06	65.00 - 70.75	1.0000	1.0000
L3	17	MP3-06	65.00 - 70.75	1.0000	1.0000
L3	18	MP3-06	65.00 - 70.75	1.0000	1.0000
L4	11	FB-L98B-002-75000( 3/8")	60.00 - 65.00	1.0000	1.0000
L4	12	WR-VG86ST-BRD( 3/4)	60.00 - 65.00	1.0000	1.0000
L4	14	Climbing Ladder	60.00 - 65.00	1.0000	1.0000
L4	16	MP3-06	60.00 - 65.00	1.0000	1.0000
L4	17	MP3-06	60.00 - 65.00	1.0000	1.0000
L4	18	MP3-06	60.00 - 65.00	1.0000	1.0000
L5	11	FB-L98B-002-75000( 3/8")	20.00 - 60.00	1.0000	1.0000
L5	12	WR-VG86ST-BRD( 3/4)	20.00 - 60.00	1.0000	1.0000
L5	14	Climbing Ladder	20.00 - 60.00	1.0000	1.0000
L5	16	MP3-06	54.50 - 60.00	1.0000	1.0000
L5	17	MP3-06	54.50 - 60.00	1.0000	1.0000
L5	18	MP3-06	54.50 - 60.00	1.0000	1.0000
L6	11	FB-L98B-002-75000( 3/8")	8.00 - 20.00	1.0000	1.0000
L6	12	WR-VG86ST-BRD( 3/4)	8.00 - 20.00	1.0000	1.0000
L6	14	Climbing Ladder	0.00 - 20.00	1.0000	1.0000

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 86959.001.01 - Portland Warren Ave, ME(BU# 878782)	<b>Page</b> 5 of 10
	<b>Project</b> 180' Monopole / App Id:164923 Rev: 1	<b>Date</b> 10:45:15 03/01/13
	<b>Client</b> Crown Castle	<b>Designed by</b> HKarande

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>i</sub>		Weight
			Horz Lateral	Vert			Front	Side	
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
Lighting Rod 3/4" x 5'	C	None			0.000	183.000	No Ice 0.375	0.375	0.030
							1/2" Ice 0.890	0.890	0.034
							1" Ice 1.356	1.356	0.041
**/**									
APXVSP18-C-A20 w/ Mount Pipe (P)	A	From Leg	4.000		0.000	177.000	No Ice 8.498	6.946	0.083
			0.000				1/2" Ice 9.149	8.127	0.148
			2.000				1" Ice 9.767	9.021	0.225
APXV9ERR18-C-A20 w/ Mount Pipe (P)	B	From Leg	4.000		0.000	177.000	No Ice 8.498	7.471	0.088
			0.000				1/2" Ice 9.149	8.656	0.155
			2.000				1" Ice 9.767	9.556	0.235
APXVSP18-C-A20 w/ Mount Pipe (P)	C	From Leg	4.000		0.000	177.000	No Ice 8.498	6.946	0.083
			0.000				1/2" Ice 9.149	8.127	0.148
			2.000				1" Ice 9.767	9.021	0.225
IBC1900BB-1 (P)	A	From Leg	4.000		0.000	177.000	No Ice 1.127	0.533	0.020
			0.000				1/2" Ice 1.273	0.647	0.030
			2.000				1" Ice 1.427	0.770	0.039
IBC1900BB-1 (P)	B	From Leg	4.000		0.000	177.000	No Ice 1.127	0.533	0.020
			0.000				1/2" Ice 1.273	0.647	0.030
			2.000				1" Ice 1.427	0.770	0.039
IBC1900BB-1 (P)	C	From Leg	4.000		0.000	177.000	No Ice 1.127	0.533	0.020
			0.000				1/2" Ice 1.273	0.647	0.030
			2.000				1" Ice 1.427	0.770	0.039
IBC1900HG-2A (P)	A	From Leg	4.000		0.000	177.000	No Ice 1.127	0.533	0.020
			0.000				1/2" Ice 1.273	0.647	0.030
			2.000				1" Ice 1.427	0.770	0.039
IBC1900HG-2A (P)	B	From Leg	4.000		0.000	177.000	No Ice 1.127	0.533	0.020
			0.000				1/2" Ice 1.273	0.647	0.030
			2.000				1" Ice 1.427	0.770	0.039
IBC1900HG-2A (P)	C	From Leg	4.000		0.000	177.000	No Ice 1.127	0.533	0.020
			0.000				1/2" Ice 1.273	0.647	0.030
			2.000				1" Ice 1.427	0.770	0.039
Platform Mount {LP 715-1} (E)	C	None			0.000	177.000	No Ice 44.210	44.210	1.775
							1/2" Ice 53.970	53.970	2.323
							1" Ice 63.730	63.730	2.871
4' x 2" Pipe Mount (E)	A	From Leg	4.000		0.000	177.000	No Ice 0.866	0.866	0.015
			0.000				1/2" Ice 1.111	1.111	0.022
			2.000				1" Ice 1.365	1.365	0.032
4' x 2" Pipe Mount (E)	B	From Leg	4.000		0.000	177.000	No Ice 0.866	0.866	0.015
			0.000				1/2" Ice 1.111	1.111	0.022
			2.000				1" Ice 1.365	1.365	0.032
4' x 2" Pipe Mount (E)	C	From Leg	4.000		0.000	177.000	No Ice 0.866	0.866	0.015
			0.000				1/2" Ice 1.111	1.111	0.022
			2.000				1" Ice 1.365	1.365	0.032
**/**									
800MHz 2X50W RRH W/FILTER (P)	A	From Leg	1.000		0.000	175.000	No Ice 2.401	2.254	0.064
			0.000				1/2" Ice 2.613	2.460	0.086
			1.000				1" Ice 2.833	2.675	0.111
800MHz 2X50W RRH W/FILTER (P)	B	From Leg	1.000		0.000	175.000	No Ice 2.401	2.254	0.064
			0.000				1/2" Ice 2.613	2.460	0.086
			1.000				1" Ice 2.833	2.675	0.111
800MHz 2X50W RRH W/FILTER (P)	C	From Leg	1.000		0.000	175.000	No Ice 2.401	2.254	0.064
			0.000				1/2" Ice 2.613	2.460	0.086
			1.000				1" Ice 2.833	2.675	0.111

**tnxTower**

**B+T Group**  
 1717 S. Boulder, Suite 300  
 Tulsa, OK  
 Phone: (918) 587-4630  
 FAX: (918) 295-0265

**Job**  
 86959.001.01 - Portland Warren Ave, ME(BU# 878782)

**Page**  
 6 of 10

**Project**  
 180' Monopole / App Id:164923 Rev: 1

**Date**  
 10:45:15 03/01/13

**Client**  
 Crown Castle

**Designed by**  
 HKarande

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>A</sub> A <sub>A</sub>		Weight
			Horz Lateral	Vert			Front	Side	
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
(2) PCS 1900MHz 4x45W-65MHz (P)	A	From Leg	1.000 0.000 1.000		0.000	175.000	No Ice 2.709 1/2" Ice 2.948 1" Ice 3.195	2.611 2.847 3.092	0.060 0.083 0.110
(2) PCS 1900MHz 4x45W-65MHz (P)	B	From Leg	1.000 0.000 1.000		0.000	175.000	No Ice 2.709 1/2" Ice 2.948 1" Ice 3.195	2.611 2.847 3.092	0.060 0.083 0.110
(2) PCS 1900MHz 4x45W-65MHz (P)	C	From Leg	1.000 0.000 1.000		0.000	175.000	No Ice 2.709 1/2" Ice 2.948 1" Ice 3.195	2.611 2.847 3.092	0.060 0.083 0.110
Side Arm Mount [SO 102-3] (P)	C	None			0.000	175.000	No Ice 3.000 1/2" Ice 3.480 1" Ice 3.960	3.000 3.480 3.960	0.081 0.111 0.141
6' x 2" Mount Pipe (E)	A	From Leg	0.500 0.000 0.000		0.000	175.000	No Ice 1.425 1/2" Ice 1.925 1" Ice 2.294	1.425 1.925 2.294	0.022 0.033 0.048
6' x 2" Mount Pipe (E)	B	From Leg	0.500 0.000 0.000		0.000	175.000	No Ice 1.425 1/2" Ice 1.925 1" Ice 2.294	1.425 1.925 2.294	0.022 0.033 0.048
6' x 2" Mount Pipe (E)	C	From Leg	0.500 0.000 0.000		0.000	175.000	No Ice 1.425 1/2" Ice 1.925 1" Ice 2.294	1.425 1.925 2.294	0.022 0.033 0.048
****									
(2) 58010 w/ Mount Pipe (E)	A	From Leg	4.000 0.000 0.000		0.000	171.000	No Ice 3.616 1/2" Ice 4.029 1" Ice 4.440	3.116 3.826 4.493	0.031 0.061 0.101
(2) 58010 w/ Mount Pipe (E)	B	From Leg	4.000 0.000 0.000		0.000	171.000	No Ice 3.616 1/2" Ice 4.029 1" Ice 4.440	3.116 3.826 4.493	0.031 0.061 0.101
(2) 58010 w/ Mount Pipe (E)	C	From Leg	4.000 0.000 0.000		0.000	171.000	No Ice 3.616 1/2" Ice 4.029 1" Ice 4.440	3.116 3.826 4.493	0.031 0.061 0.101
Platform Mount [LP 401-1] (E)	C	None			0.000	171.000	No Ice 24.330 1/2" Ice 30.220 1" Ice 36.110	24.330 30.220 36.110	1.645 2.030 2.415
****									
(2) 7770.00 w/ Mount Pipe (E)	A	From Leg	4.000 0.000 1.000		0.000	161.000	No Ice 6.119 1/2" Ice 6.626 1" Ice 7.128	4.254 5.014 5.711	0.055 0.101 0.155
(2) 7770.00 w/ Mount Pipe (E)	B	From Leg	4.000 0.000 1.000		0.000	161.000	No Ice 6.119 1/2" Ice 6.626 1" Ice 7.128	4.254 5.014 5.711	0.055 0.101 0.155
(2) 7770.00 w/ Mount Pipe (E)	C	From Leg	4.000 0.000 1.000		0.000	161.000	No Ice 6.119 1/2" Ice 6.626 1" Ice 7.128	4.254 5.014 5.711	0.055 0.101 0.155
(2) LGP2140X (E)	A	From Leg	4.000 0.000 0.000		0.000	161.000	No Ice 1.260 1/2" Ice 1.416 1" Ice 1.581	0.378 0.493 0.617	0.014 0.021 0.030
(2) LGP2140X (E)	B	From Leg	4.000 0.000 0.000		0.000	161.000	No Ice 1.260 1/2" Ice 1.416 1" Ice 1.581	0.378 0.493 0.617	0.014 0.021 0.030
(2) LGP2140X (E)	C	From Leg	4.000 0.000 0.000		0.000	161.000	No Ice 1.260 1/2" Ice 1.416 1" Ice 1.581	0.378 0.493 0.617	0.014 0.021 0.030
P65-17-XLH-RR w/ Mount Pipe (R)	A	From Leg	4.000 0.000 1.000		0.000	161.000	No Ice 11.704 1/2" Ice 12.424 1" Ice 13.153	8.938 10.450 11.986	0.092 0.174 0.271
AM-X-CD-16-65-00T-RET	B	From Leg	4.000		0.000	161.000	No Ice 8.498	6.304	0.074



Description	Face or Leg	Offset Type	Offsets: Horiz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>A</sub> A <sub>Front</sub> ft <sup>2</sup>	C <sub>A</sub> A <sub>Side</sub> ft <sup>2</sup>	Weight K
w/ Mount Pipe (R)			0.000			1/2" Ice 9.149	7.479	0.136
AM-X-CD-16-65-00T-RET	C	From Leg	1.000			1" Ice 9.767	8.368	0.210
w/ Mount Pipe (R)			4.000	0.000	161.000	No Ice 8.498	6.304	0.074
(2) 7020.00 (R)	A	From Leg	0.000			1/2" Ice 9.149	7.479	0.136
(R)			1.000			1" Ice 9.767	8.368	0.210
(2) 7020.00 (R)	B	From Leg	4.000	0.000	161.000	No Ice 0.119	0.204	0.002
(R)			0.000			1/2" Ice 0.171	0.279	0.005
(2) 7020.00 (R)	C	From Leg	1.000			1" Ice 0.232	0.363	0.009
(R)			4.000	0.000	161.000	No Ice 0.119	0.204	0.002
(2) 7020.00 (R)	A	From Leg	0.000			1/2" Ice 0.171	0.279	0.005
(R)			1.000			1" Ice 0.232	0.363	0.009
DC6-48-60-18-8F (R)	A	From Leg	4.000	0.000	161.000	No Ice 1.266	1.266	0.020
(2) RRUS 11 (R)	A	From Leg	0.000			1/2" Ice 1.456	1.456	0.035
(R)			1.000			1" Ice 1.658	1.658	0.053
(2) RRUS 11 (R)	B	From Leg	2.000	0.000	159.000	No Ice 3.249	1.373	0.048
(R)			0.000			1/2" Ice 3.491	1.551	0.068
(2) RRUS 11 (R)	C	From Leg	1.000			1" Ice 3.741	1.738	0.092
(R)			2.000	0.000	159.000	No Ice 3.249	1.373	0.048
(2) RRUS 11 (R)	A	From Leg	0.000			1/2" Ice 3.491	1.551	0.068
(R)			1.000			1" Ice 3.741	1.738	0.092
Side Arm Mount [SO 701-3] (R)	C	None	2.000	0.000	159.000	No Ice 3.249	1.373	0.048
(R)			0.000			1/2" Ice 3.491	1.551	0.068
T-Arm Mount [TA 602-3] (R)	C	None	1.000			1" Ice 3.741	1.738	0.092
(R)			0.000	0.000	161.000	No Ice 2.830	2.830	0.195
(R)						1/2" Ice 3.920	3.920	0.237
(R)						1" Ice 5.010	5.010	0.279
(R)						No Ice 11.590	11.590	0.774
(R)						1/2" Ice 15.440	15.440	0.990
(R)						1" Ice 19.290	19.290	1.206

\*\*\*

**Load Combinations**

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 86959.001.01 - Portland Warren Ave, ME(BU# 878782)	<b>Page</b> 8 of 10
	<b>Project</b> 180' Monopole / App Id:164923 Rev: 1	<b>Date</b> 10:45:15 03/01/13
	<b>Client</b> Crown Castle	<b>Designed by</b> HKarande

Comb. No.	Description
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	180 - 140	21.207	50	1.076	0.001
L2	140 - 100	12.718	50	0.849	0.001
L3	100 - 65	6.410	50	0.623	0.000
L4	65 - 60	2.645	50	0.385	0.000
L5	60 - 20	2.258	50	0.354	0.000
L6	20 - 0	0.240	50	0.112	0.000

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
183.000	Lighting Rod 3/4" x 5'	50	21.207	1.076	0.001	54546
177.000	APXVSP18-C-A20 w/ Mount Pipe	50	20.536	1.059	0.001	54546
175.000	800MHz 2X50W RRH W/FILTER	50	20.088	1.047	0.001	54546
171.000	(2) 58010 w/ Mount Pipe	50	19.197	1.024	0.001	30303
161.000	(2) 7770.00 w/ Mount Pipe	50	17.002	0.966	0.001	14354
159.000	(2) RRUS 11	50	16.572	0.955	0.001	12987

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 86959.001.01 - Portland Warren Ave, ME(BU# 878782)	<b>Page</b> 9 of 10
	<b>Project</b> 180' Monopole / App Id:164923 Rev: 1	<b>Date</b> 10:45:15 03/01/13
	<b>Client</b> Crown Castle	<b>Designed by</b> HKarande

### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	180 - 140	105.954	24	5.382	0.006
L2	140 - 100	63.582	24	4.248	0.003
L3	100 - 65	32.056	24	3.118	0.002
L4	65 - 60	13.229	24	1.924	0.001
L5	60 - 20	11.294	24	1.771	0.001
L6	20 - 0	1.200	24	0.557	0.000

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
183.000	Lighting Rod 3/4" x 5'	24	105.954	5.382	0.006	11117
177.000	APXVSPP18-C-A20 w/ Mount Pipe	24	102.602	5.295	0.006	11117
175.000	800MHz 2X50W RRH W/FILTER	24	100.370	5.237	0.006	11117
171.000	(2) 58010 w/ Mount Pipe	24	95.922	5.121	0.005	6175
161.000	(2) 7770.00 w/ Mount Pipe	24	84.969	4.834	0.004	2923
159.000	(2) RRUS 11	24	82.821	4.777	0.004	2644

### Compression Checks

### Pole Design Data

Section No.	Elevation ft	Size	L ft	L <sub>n</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	φP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
L1	180 - 140 (1)	P24x3/8	40.000	0.000	0.0	27.833	-12.287	901.775	0.014
L2	140 - 100 (2)	P36x1/2	40.000	0.000	0.0	55.763	-22.818	1806.730	0.013
L3	100 - 65 (3)	P42x1/2	35.000	0.000	0.0	65.188	-33.596	2112.090	0.016
L4	65 - 60 (4)	P42x.7333	5.000	0.000	0.0	95.067	-35.759	2891.950	0.012
L5	60 - 20 (5)	P48x5/8	40.000	0.000	0.0	93.021	-52.753	3013.870	0.018
L6	20 - 0 (6)	P54x5/8	20.000	0.000	0.0	104.802	-62.031	3395.570	0.018

### Pole Bending Design Data

Section No.	Elevation ft	Size	M <sub>ux</sub> kip-ft	φM <sub>ux</sub> kip-ft	Ratio $\frac{M_{ux}}{\phi M_{ux}}$	M <sub>uy</sub> kip-ft	φM <sub>uy</sub> kip-ft	Ratio $\frac{M_{uy}}{\phi M_{uy}}$
L1	180 - 140 (1)	P24x3/8	493.927	550.881	0.897	0.000	550.881	0.000
L2	140 - 100 (2)	P36x1/2	1279.750	1623.158	0.788	0.000	1623.158	0.000
L3	100 - 65 (3)	P42x1/2	2108.458	2162.842	0.975	0.000	2162.842	0.000
L4	65 - 60 (4)	P42x.7333	2237.017	3165.958	0.707	0.000	3165.958	0.000
L5	60 - 20 (5)	P48x5/8	3355.450	3573.958	0.939	0.000	3573.958	0.000
L6	20 - 0 (6)	P54x5/8	3963.267	4453.000	0.890	0.000	4453.000	0.000

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK Phone: (918) 587-4630 FAX: (918) 295-0265	<b>Job</b> 86959.001.01 - Portland Warren Ave, ME(BU# 878782)	<b>Page</b> 10 of 10
	<b>Project</b> 180' Monopole / App Id:164923 Rev: 1	<b>Date</b> 10:45:15 03/01/13
	<b>Client</b> Crown Castle	<b>Designed by</b> HKarande

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual $V_u$ K	$\phi V_n$ K	Ratio $\frac{V_u}{\phi V_n}$	Actual $T_u$ kip-ft	$\phi T_n$ kip-ft	Ratio $\frac{T_u}{\phi T_n}$
L1	180 - 140 (1)	P24x3/8	17.399	450.887	0.039	0.530	874.033	0.001
L2	140 - 100 (2)	P36x1/2	21.765	903.365	0.024	0.529	2635.858	0.000
L3	100 - 65 (3)	P42x1/2	25.459	1056.050	0.024	0.528	3609.208	0.000
L4	65 - 60 (4)	P42x.7333	25.990	1445.970	0.018	0.528	4887.275	0.000
L5	60 - 20 (5)	P48x5/8	29.675	1506.930	0.020	0.527	5872.808	0.000
L6	20 - 0 (6)	P54x5/8	31.108	1697.790	0.018	0.527	7465.225	0.000

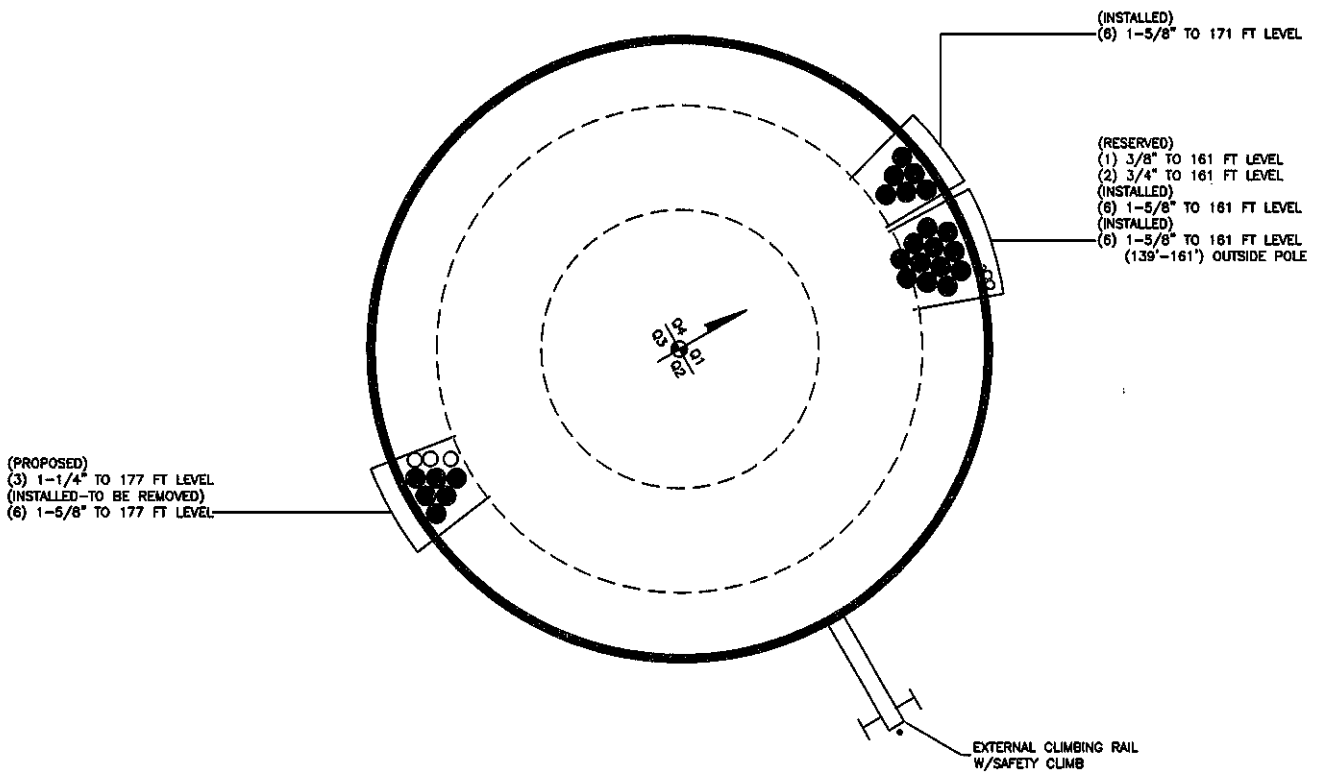
### Pole Interaction Design Data

Section No.	Elevation ft	Ratio $\frac{P_u}{\phi P_n}$	Ratio $\frac{M_{ux}}{\phi M_{nx}}$	Ratio $\frac{M_{uy}}{\phi M_{ny}}$	Ratio $\frac{V_u}{\phi V_n}$	Ratio $\frac{T_u}{\phi T_n}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	180 - 140 (1)	0.014	0.897	0.000	0.039	0.001	0.912 ✓	1.000	4.8.2 ✓
L2	140 - 100 (2)	0.013	0.788	0.000	0.024	0.000	0.802 ✓	1.000	4.8.2 ✓
L3	100 - 65 (3)	0.016	0.975	0.000	0.024	0.000	0.991 ✓	1.000	4.8.2 ✓
L4	65 - 60 (4)	0.012	0.707	0.000	0.018	0.000	0.719 ✓	1.000	4.8.2 ✓
L5	60 - 20 (5)	0.018	0.939	0.000	0.020	0.000	0.957 ✓	1.000	4.8.2 ✓
L6	20 - 0 (6)	0.018	0.890	0.000	0.018	0.000	0.909 ✓	1.000	4.8.2 ✓

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow}$ K	% Capacity	Pass Fail
L1	180 - 140	Pole	P24x3/8	1	-12.287	901.775	91.2	Pass
L2	140 - 100	Pole	P36x1/2	2	-22.818	1806.730	80.2	Pass
L3	100 - 65	Pole	P42x1/2	3	-33.596	2112.090	99.1	Pass
L4	65 - 60	Pole	P42x.7333	4	-35.759	2891.950	71.9	Pass
L5	60 - 20	Pole	P48x5/8	5	-52.753	3013.870	95.7	Pass
L6	20 - 0	Pole	P54x5/8	6	-62.031	3395.570	90.9	Pass
Summary								
Pole (L3)							99.1	Pass
<b>RATING =</b>							<b>99.1</b>	<b>Pass</b>

**APPENDIX B**  
**BASE LEVEL DRAWING**



BUSINESS UNIT: 878782 TOWER ID: C\_BASELEVEL

**APPENDIX C**  
**ADDITIONAL CALCULATIONS**

PROJECT **86959.001.01 - Portland, ME - Crown Castle**SUBJECT **Bridge Stiffeners @ 140'**DATE **03/01/13** PAGE **1** OF **2****B&T Engineering, Inc.**

1325 E. 15th St., Suite 202

Tulsa, OK 74120

(918) 587-4630

SSC

**Global Section Properties:****Assumes Moment to Pole Face**

Top Pole t	0.38 in
Bottom Pole t	0.38 in
Top Pole Dia.	24.00 in
Bottom Pole Dia.	36.00 in
Pole Grade	36.00 ksi
BS Material Grade	65.00 ksi
BS Width	5.50 in
BS Thickness	1.25 in
BS Height	48.00 in
Weld Size	3/8 in
Weld Grade	70 exx
Gap	8.00 in
I	4467.52 in <sup>4</sup>
Mu	493.93 k-ft
Step Width	6.00 in
Ybar	22.00 in
S	203.07 in <sup>3</sup>
fb	29.19 ksi
Area	6.88 in <sup>2</sup>
Pu (BS)	200.67 k

Axial Load	12.29 k
Number of BS	3
Bolted Plate t	1.25

Width of Bottom Section of BS  
Plate Thickness of BSDistance Between BS Welded Sections  
Global MOI, Taken from AutoCAD  
Moment at Flange Under ConsiderationDist. CL Pole to CL BS  
Global Section Modulus; I/Ybar  
M/S  
BS Cross Sectional Area Below Flange  
Load to BS**Bottom Bridge Stiffener Section:**

V = P	204.76 k
Arm	2.75 in
Incidental Moment	563.09 k-in
Lb	2.75 in
d	20.00 in
Lbd/t <sup>2</sup>	35.2
Phi*Mn	7304.61 k-in

Shear to BS  
Incidental Moment Arm (BS Plate)  
Moment at Pole Face

(BS Height - Gap)/2

AISC 13th, F11

**Unity% = 7.71%**

kv	5
Cv	1
Phi*Vn	877.5

AISC 13th, G2

**Unity% = 23.33%**



PROJECT **86959.001.01 - Portland, ME - Crown Castle**

SUBJECT **Bridge Stiffeners @ 140'**

DATE **03/01/13** PAGE **2** OF **2**



**B&T Engineering, Inc.**

1325 E. 15th St., Suite 202

Tulsa, OK 74120

(918) 587-4630

SSC

**Top Bridge Stiffener Section:**

V = P	204.76 k		
Arm	8.75 in		
Incidental Moment	1791.66 k-in		
Lb	8.75 in		
d	20.00 in		
Lbd/t <sup>2</sup>	112.00		
Phi*Mn	7074.68 k-in	AISC 13th, F11	
		<b>Unity% =</b>	<b>25.33%</b>
kv	5	AISC 13th, G2	
Cv	1		
Phi*Vn	877.5	<b>Unity% =</b>	<b>23.33%</b>

**Check Weld Between BS and Connection Plate:**

Leg Size	3/8 in		
Aw/in	0.53 in <sup>2</sup>		
Load From Moment	26.87 k/in		
Load From Shear	10.24 k/in		
Resultant Load	14.38 k/in	Load to one inch of one weld	
Phi*Rn	16.70 ksi		
		<b>Unity% =</b>	<b>86.09%</b>

**Check Bridge Stiffener Span:**

Lu	37.00 in		
b/t	4.4		
Qs	1		
ry	0.3608 in		
Kl/r	66.65	AISC 13th, E3 and E7	
4.71*sqrt(E/QFy)	99.49		
Fe	64.43 ksi		
Fcr	42.61 ksi		
Phi*Rn	263.6657562		
		<b>Unity% =</b>	<b>77.66%</b>

# Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782

Site Name: Portland Warren Ave, ME

App #: 164923, Rev 1

## Reactions

Mu	1279.75	ft-kips
Axial, Pu:	22.818	kips
Shear, Vu:	21.765	kips
Elevation:	100	feet

## Bolt Threads:

X-Excluded	
$\phi V_n = \phi(0.55 \cdot A_b \cdot F_u)$	
$\phi = 0.75, \phi \cdot V_n$ (kips):	21.87

Pole Manufacturer: Other

If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

## Bolt Data

Qty:	52	
Diameter (in.):	0.75	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:		<-- Disregard
N/A:		<-- Disregard
Circle (in.):	38.5	

Flange Bolt Results

Bolt Tension Capacity,  $\phi \cdot T_n, B1$ : 30.06 kips  
 Adjusted  $\phi \cdot T_n$  (due to  $V_u = V_u / Q_t$ ), B: 30.05 kips  
 Max Bolt directly applied  $T_u$ : 30.24 Kips  
 Min. PL "tc" for B cap. **w/o Pry**:  $T_u > B$  N/A in  
 Min PL "treq" for actual T **w/ Pry**: 0.965 in  
 Min PL "t1" for actual T **w/o Pry**:  $T_u > B$  N/A in  
 T allowable w/o Prying: 30.06 kips  
 Prying Force, q: 0.00 kips  $T > B$  Case  
 Total Bolt Tension =  $T_u + q$ : 30.24 kips  
 Non-Prying Bolt Stress Ratio,  $T_u / B$ : 100.6% Pass

Rigid

$\phi \cdot T_n$
$\phi T_n \{1 - (V_u / \phi V_n)^2\}^{0.5}$

## Plate Data

Diam:	40.75	in
Thick, t:	2.125	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	2.17	in

## Exterior Flange Plate Results

Flexural Check  
 Compression Side Plate Stress: 10.1 ksi  
 Allowable Plate Stress: 32.4 ksi  
 Compression Plate Stress Ratio: 31.1% Pass  
**No Prying Check for  $T_u > B$**   
 Tension Side Stress Ratio,  $(treq/t)^2$ : 20.6% Pass

Flexural Check

Rigid

TIA G
$\phi \cdot F_y$
Comp. Y.L. Length: 13.65

## Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

n/a

## Stiffener Results

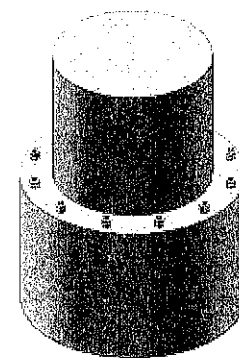
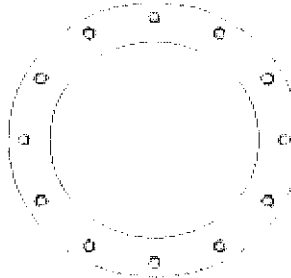
Horizontal Weld: n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a

## Pole Results

Pole Punching Shear Check: n/a

## Pole Data

Diam:	36	in
Thick:	0.5	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi
Reinf. Fillet Weld	0	"0" if None



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

# Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

Site Data	
BU#:	878782
Site Name:	Portland Warren Ave, ME
App #:	164923, Rev 1

Manufacturer:	Other
---------------	-------

Bolt Data		
Qty:	52	
Diam:	0.75	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:		<-- Disregard
N/A:		<-- Disregard
Circle:	38.5	in

Plate Data		
Plate Outer Diam:	41	in
Plate Inner Diam:	36.25	in (Hole @ Ctr)
Thick:	2.125	in
Grade:	36	ksi
Effective Width:	2.48	in

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

Pole Data		
Pole OuterDiam:	42	in
Thick:	0.5	in
Pole Inner Diam:	41	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi

Reactions		
Moment:	1279.75	ft-kips
Axial:	22.818	kips
Shear:	21.765	kips
Exterior Flange Run, T+q:	30.24	kips

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 \cdot A_b \cdot F_u)$
$\phi = 0.75, \phi \cdot V_n$ (kips):
21.87

Elevation: 100 feet

### Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 30.2 Kips, Ext. Tu=Interior Tu  
 Adjusted  $\phi \cdot T_n$  (due to  $V_u = V_u / Q_t$ ): 30.1 Kips  
 Bolt Stress Ratio: 100.6% Pass

### Interior Flange Plate Results

Controlling Bolt Axial Force: 31.1 Kips, Ext. Cu=Interior Cu  
 Plate Stress: 13.9 ksi  
 Allowable Plate Stress,  $\phi \cdot F_y$ : 32.4 ksi  
 Plate Stress Ratio: 42.9% Pass

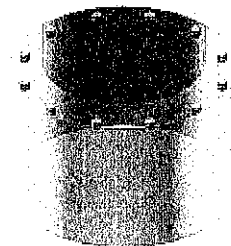
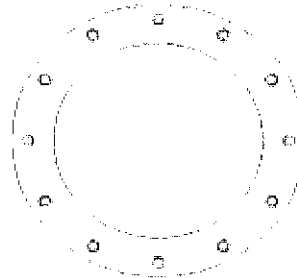
n/a

### Stiffener Results

Horizontal Weld: n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a

### Pole Results

Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

PROJECT **86959.001.01 - Portland Warren Ave, ME**  
 SUBJECT **Sabre Bridge Stiffeners @ 60'**  
 DATE **03/01/13** PAGE 1 OF 1



**B&T Engineering, Inc.**  
 1325 E. 15th St., Suite 202  
 Tulsa, OK 74120  
 (918) 587-4630

SSC

**Determine Load to Bridge Stiffener:**

<b>M =</b>	2239.2 k-ft	From Risa Model	<b>Stiffener Width</b>	<b>8.500 in</b>
<b>I =</b>	15852.8 in <sup>4</sup>	From AutoCAD Sketch	<b>Stiffener Thickness</b>	<b>1.250 in</b>
<b>ybar =</b>	24.625 in		<b>Stiffener Height</b>	<b>48.000 in</b>
<b>S =</b>	643.77 in <sup>3</sup>	I/y	<b>Fy</b>	<b>65 ksi</b>
<b>fc =</b>	41.74 ksi	M/S	<b>Step Width</b>	<b>3.00 in</b>
<b>Ag =</b>	10.625 in <sup>2</sup>			
<b>Pu =</b>	443.49 k	fc x Ag	<b>Bolt Circle</b>	<b>44.38 in</b>

**Determine  $\Phi P_n$  (Allowable Axial Load):**

<b>Pn = Fcr x Ag</b>		Eqn E3-1, AISC 13th Edition, Section E3.		
<b>K =</b>	1			
<b>l =</b>	16.000 in	Unsupported Length		
<b>Iy =</b>	1.383 in <sup>4</sup>	Local Weak Axis Moment of Inertia		
<b>Ag =</b>	10.625 in <sup>2</sup>	Stiffener Cross Sectional Area		
<b>ry =</b>	.361 in	Radius of Gyration (Weak Axis)		
<b>kl/r =</b>	44.34			
<b>4.71 x <math>\sqrt{E/Fy}</math> =</b>	99.49	Limit State Equation for Flexural Buckling - AISC 13th Edition, Section E3.		
<b>Fe =</b>	145.58 ksi	Eqn E3-4 - AISC 13th Edition, Section E3.		
		Elastic Critical Buckling Stress		
<b>Fcr =</b>	53.92 ksi	Eqn E3-2, AISC 13th Edition, Section E3		
		Critical Buckling Stress		
<b>Pn =</b>	572.90 k	Nominal Compressive Strength		
<b><math>\Phi P_n</math> =</b>	515.61 k	Allowable Compressive Strength	<b>Unity% =</b>	<b>86.0 %</b>

**Moment to Existing Bolt Group:**

<b>S<sub>BG</sub> =</b>	714.49 in <sup>3</sup>	<b># Bolts Acting</b>	14
<b>ft =</b>	37.61 ksi		
<b>Ab =</b>	.442 in <sup>2</sup>		
<b>T =</b>	232.61 k		
<b>Arm =</b>	44.38 ksi		
<b>M<sub>EQ</sub> =</b>	860.2 k-ft		

<-----Insert into Crown Spreadsheet

PROJECT **86959.001.01 - Portland Warren Ave, ISSC**  
 SUBJECT **AeroSolutions Bridge Stiffeners @ 60'**  
 DATE **03/01/13** PAGE 1 OF 1



**B&T Engineering, Inc.**  
 1325 E. 15th St., Suite 202  
 Tulsa, OK 74120  
 (918) 587-4630

**Determine Load to Bridge Stiffener:**

M =	2239.2 k-ft	From Risa Model	<b>MP3 Type</b>	<b>MP3-06</b>
I =	14086.1 in <sup>4</sup>	From AutoCAD Sketch		
ybar =	24.930 in			
S =	565.03 in <sup>3</sup>	I/y	<b>Fy</b>	<b>65 ksi</b>
fc =	47.56 ksi	M/S	<b>Step Width</b>	<b>3.00 in</b>
Ag =	8.570 in <sup>2</sup>			
Pu =	407.56 k	fc x Ag	<b>Bolt Circle</b>	<b>44.38 in</b>

**Determine  $\Phi P_n$  (Allowable Axial Load):**

$P_n = F_{cr} \times A_g$		Eqn E3-1, AISC 13th Edition, Section E3.		
K =	1			
l =	18.000 in	Unsupported Length		
Iy =	4.950 in <sup>2</sup>	Local Weak Axis Moment of Intertia		
Ag =	8.570 in <sup>2</sup>	Stiffener Cross Sectional Area		
ry =	.760 in	Radius of Gyration (Weak Axis)		
kl/r =	23.68			
$4.71 \times \sqrt{E/F_y} =$	99.49	Limit State Equation for Flexural Buckling - AISC 13th Edition, Section E3.		
Fe =	510.25 ksi	Eqn E3-4 - AISC 13th Edition, Section E3.		
Fcr =	61.63 ksi	Elastic Critical Buckling Stress		
		Eqn E3-2, AISC 13th Edition, Section E3		
		Critical Buckling Stress		
Pn =	528.13 k	Nominal Compressive Strength		
$\Phi P_n =$	475.31 k	Allowable Compressive Strength	<b>Unity% =</b>	<b>85.7 %</b>

**Moment to Existing Bolt Group:**

$S_{BG} =$	634.87 in <sup>3</sup>	# Bolts Acting	14
ft =	42.33 ksi		
Ab =	.442 in <sup>2</sup>		
T =	261.78 k		
Arm =	44.38 ksi		
$M_{EQ} =$	968.0 k-ft		

<-----Insert into Crown Spreadsheet

# Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782

Site Name: Portland Warren Ave, ME

App #: 164923, Rev 1

Reactions		
Mu	968	ft-kips
Axial, Pu:	35.759	kips
Shear, Vu:	25.99	kips
Elevation:	60	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 \cdot A_b \cdot F_u)$
$\phi = 0.75, \phi \cdot V_n$ (kips):
27.34

Pole Manufacturer:	Other
--------------------	-------

If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Bolt Data		
Qty:	56	
Diameter (in.):	0.75	Bolt Fu: 150
Bolt Material:	A490	Bolt Fy: 130
N/A:		<-- Disregard
N/A:		<-- Disregard
Circle (in.):	44.375	

Flange Bolt Results

Bolt Tension Capacity, $\phi \cdot T_n, B1$ :	37.58 kips
Adjusted $\phi \cdot T_n$ (due to $V_u = V_u / Q_t$ ), B:	37.57 kips
Max Bolt directly applied Tu:	18.06 Kips
Min. PL "tc" for B cap. w/o Pry:	0.996 in
Min PL "treq" for actual T w/ Pry:	0.537 in
Min PL "t1" for actual T w/o Pry:	0.690 in
T allowable w/o Prying:	37.58 kips $\alpha' < 0$ case
Prying Force, q:	0.00 kips
Total Bolt Tension = Tu + q:	18.06 kips
Non-Prying Bolt Stress Ratio, Tu/B:	48.1% Pass

Rigid
$\phi \cdot T_n$
$\phi T_n [(1 - (V_u / \phi V_n)^2)^{0.5}]$

Plate Data		
Diam:	46.5	in
Thick, t:	2.25	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	2.36	in

Exterior Flange Plate Results

Flexural Check	5.0 ksi
Compression Side Plate Stress:	32.4 ksi
Allowable Plate Stress:	15.3% Pass
Compression Plate Stress Ratio:	
No Prying	
Tension Side Stress Ratio, $(treq/t)^2$ :	5.7% Pass

Rigid
TIA G
$\phi \cdot F_y$
Comp. Y.L. Length:
14.32

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

n/a

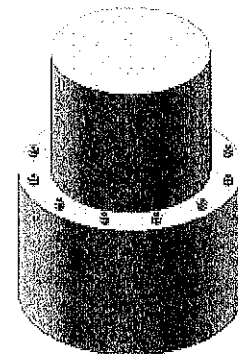
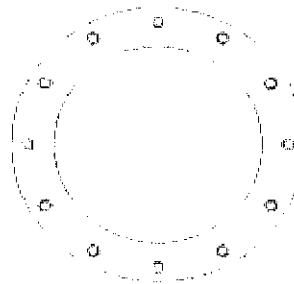
Stiffener Results

Horizontal Weld :	n/a
Vertical Weld:	n/a
Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$ :	n/a
Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$ :	n/a
Plate Comp. (AISC Bracket):	n/a

Pole Results

Pole Punching Shear Check: n/a

Pole Data		
Diam:	42	in
Thick:	0.5	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi
Reinf. Fillet Weld	0	"0" if None



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

# Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 164923, Rev 1

Manufacturer:	Other
---------------	-------

Bolt Data		
Qty:	56	
Diam:	0.75	Bolt Fu: 150
Bolt Material:	A490	Bolt Fy: 130
N/A:		<-- Disregard
N/A:		<-- Disregard
Circle:	44.375	in

Plate Data		
Plate Outer Diam:	46.75	in
Plate Inner Diam:	42.25	in (Hole @ Ctr)
Thick:	2.25	in
Grade:	36	ksi
Effective Width:	2.62	in

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

Pole Data		
Pole OuterDiam:	48	in
Thick:	0.625	in
Pole Inner Diam:	46.75	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi

## Reactions

Moment:	968	ft-kips
Axial:	35.759	kips
Shear:	25.99	kips
Exterior Flange Run, T+q:	18.06	kips

## Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
27.34

Elevation: 60 feet

## Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 18.1 Kips, Ext. Flange Tu+q  
 Adjusted  $\phi^* T_n$  (due to  $V_u = V_u / Q_t$ ), 37.6 Kips  
 Bolt Stress Ratio: 48.1% Pass

## Interior Flange Plate Results

Controlling Bolt Axial Force: 19.3 Kips, Ext. Cu=Interior Cu  
 Plate Stress: 6.9 ksi  
 Allowable Plate Stress,  $\phi^* F_y$ : 32.4 ksi  
 Plate Stress Ratio: 21.4% Pass

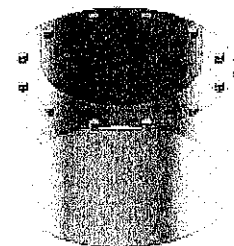
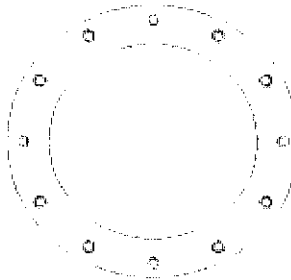
## n/a

## Stiffener Results

Horizontal Weld : n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a

## Pole Results

Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

PROJECT **86959.001.01 - Portland Warren Ave, ME**  
 SUBJECT **Sabre Bridge Stiffeners @ 20'**  
 DATE **03/01/13** PAGE 1 OF 1



**B&T Engineering, Inc.**  
 1325 E. 15th St., Suite 202  
 Tulsa, OK 74120  
 (918) 587-4630

SSC

**Determine Load to Bridge Stiffener:**

M =	3355.1 k-ft	From Risa Model	Stiffener Width	8.500 in
I =	25218.0 in <sup>4</sup>	From AutoCAD Sketch	Stiffener Thickness	1.250 in
ybar =	24.625 in		Stiffener Height	48.000 in
S =	1024.08 in <sup>3</sup>	I/y	Fy	65 ksi
fc =	39.31 ksi	M/S	Step Width	3.00 in
Ag =	10.625 in <sup>2</sup>			
Pu =	417.72 k	fc x Ag	Bolt Circle	50.38 in

**Determine  $\phi P_n$  (Allowable Axial Load):**

Pn = Fcr x Ag		Eqn E3-1, AISC 13th Edition, Section E3.		
K =	1			
l =	16.000 in	Unsupported Length		
Iy =	1.383 in <sup>4</sup>	Local Weak Axis Moment of Inertia		
Ag =	10.625 in <sup>2</sup>	Stiffener Cross Sectional Area		
ry =	.361 in	Radius of Gyration (Weak Axis)		
kl/r =	44.34			
4.71 x $\sqrt{E/F_y}$ =	99.49	Limit State Equation for Flexural Buckling - AISC 13th Edition, Section E3.		
Fe =	145.58 ksi	Eqn E3-4 - AISC 13th Edition, Section E3.		
Fcr =	53.92 ksi	Elastic Critical Buckling Stress		
		Eqn E3-2, AISC 13th Edition, Section E3		
		Critical Buckling Stress		
Pn =	572.90 k	Nominal Compressive Strength		
$\phi P_n$ =	515.61 k	Allowable Compressive Strength	Unity% =	81.0 %

**Moment to Existing Bolt Group:**

S <sub>BG</sub> =	1001.21 in <sup>3</sup>	# Bolts Acting	13
ft =	40.21 ksi		
Ab =	.785 in <sup>2</sup>		
T =	410.58 k		
Arm =	50.38 ksi		
M <sub>EQ</sub> =	1723.6 k-ft		

<-----Insert into Crown Spreadsheet



PROJECT **86959.001.01 - Portland Warren Ave, ISSC**  
 SUBJECT **AeroSolutions Bridge Stiffeners @ 20'**  
 DATE **03/01/13** PAGE 1 OF 1



**B&T Engineering, Inc.**  
 1325 E. 15th St., Suite 202  
 Tulsa, OK 74120  
 (918) 587-4630

**Determine Load to Bridge Stiffener:**

<b>M =</b>	3355.1 k-ft	From Risa Model	<b>MP3 Type</b>	<b>MP3-06</b>
<b>I =</b>	22971.6 in <sup>4</sup>	From AutoCAD Sketch		
<b>ybar =</b>	27.930 in			
<b>S =</b>	822.47 in <sup>3</sup>	I/y	<b>Fy</b>	<b>65 ksi</b>
<b>fc =</b>	48.95 ksi	M/S	<b>Step Width</b>	<b>3.00 in</b>
<b>Ag =</b>	8.570 in <sup>2</sup>			
<b>Pu =</b>	419.52 k	fc x Ag	<b>Bolt Circle</b>	<b>50.38 in</b>

**Determine  $\Phi P_n$  (Allowable Axial Load):**

<b>Pn = Fcr x Ag</b>		Eqn E3-1, AISC 13th Edition, Section E3.		
<b>K =</b>	1			
<b>I =</b>	18.000 in	Unsupported Length		
<b>Iy =</b>	4.950 in <sup>2</sup>	Local Weak Axis Moment of Inertia		
<b>Ag =</b>	8.570 in <sup>2</sup>	Stiffener Cross Sectional Area		
<b>ry =</b>	.760 in	Radius of Gyration (Weak Axis)		
<b>kl/r =</b>	23.68			
<b>4.71 x <math>\sqrt{E/Fy}</math> =</b>	99.49	Limit State Equation for Flexural Buckling - AISC 13th Edition, Section E3.		
<b>Fe =</b>	510.25 ksi	Eqn E3-4 - AISC 13th Edition, Section E3.		
		Elastic Critical Buckling Stress		
<b>Fcr =</b>	61.63 ksi	Eqn E3-2, AISC 13th Edition, Section E3		
		Critical Buckling Stress		
<b>Pn =</b>	528.13 k	Nominal Compressive Strength		
<b><math>\Phi P_n</math> =</b>	475.31 k	Allowable Compressive Strength	<b>Unity% =</b>	<b>88.3 %</b>

**Moment to Existing Bolt Group:**

<b>S<sub>BG</sub> =</b>	912.02 in <sup>3</sup>	<b># Bolts Acting</b>	13
<b>ft =</b>	44.15 ksi		
<b>Ab =</b>	.785 in <sup>2</sup>		
<b>T =</b>	450.73 k		
<b>Arm =</b>	50.38 ksi		
<b>M<sub>EQ</sub> =</b>	1892.1 k-ft	<b>&lt;-----Insert into Crown Spreadsheet</b>	

# Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

### Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 164923, Rev 1

Reactions		
Mu	1892.1	ft-kips
Axial, Pu:	52.753	kips
Shear, Vu:	29.675	kips
Elevation:	20	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 \cdot A_b \cdot F_u)$
$\phi = 0.75, \phi \cdot V_n$ (kips):
38.88

Pole Manufacturer:	Other
--------------------	-------

If No stiffeners, Criteria:	TIA G	<-Only Applicable to Unstiffened Cases
<b>Flange Bolt Results</b>		
Bolt Tension Capacity, $\phi \cdot T_n, B1$ :	54.54 kips	<b>Rigid</b>
Adjusted $\phi \cdot T_n$ (due to $V_u = V_u / Q_t$ ), B:	54.53 kips	$\phi \cdot T_n$
Max Bolt directly applied Tu:	33.66 Kips	$\phi T_n [(1 - (V_u / \phi V_n)^2)^{0.5}]$
Min. PL "tc" for B cap. w/o Pry:	0.995 in	
Min PL "treq" for actual T w/ Pry:	0.611 in	
Min PL "t1" for actual T w/o Pry:	0.782 in	
T allowable w/o Prying:	54.54 kips	$\alpha' < 0$ case
Prying Force, q:	0.00 kips	
Total Bolt Tension = Tu + q:	33.66 kips	
Non-Prying Bolt Stress Ratio, Tu/B:	61.7% Pass	

Bolt Data		
Qty:	52	
Diameter (in.):	1	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:		<-- Disregard
N/A:		<-- Disregard
Circle (in.):	50.375	

Plate Data		
Diam:	52.5	in
Thick, t:	2.5	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	2.90	in

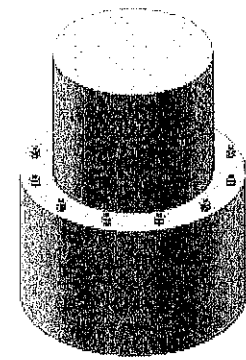
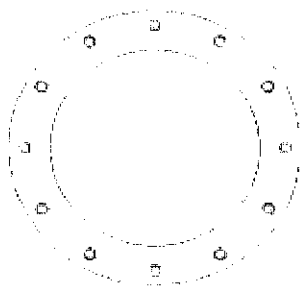
Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

Pole Data		
Diam:	48	in
Thick:	0.625	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi
Reinf. Fillet Weld	0	"0" if None

Exterior Flange Plate Results		Flexural Check
Compression Side Plate Stress:	6.1 ksi	<b>Rigid</b>
Allowable Plate Stress:	32.4 ksi	TIA G
Compression Plate Stress Ratio:	18.8% Pass	$\phi \cdot F_y$
<b>No Prying</b>		Comp. Y.L. Length:
Tension Side Stress Ratio, $(treq/t)^2$ :	6.0% Pass	15.29

Stiffener Results	
Horizontal Weld :	n/a
Vertical Weld:	n/a
Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$ :	n/a
Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$ :	n/a
Plate Comp. (AISC Bracket):	n/a

**Pole Results**  
 Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt  
 \*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

# Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 878782  
 Site Name: Portland Warren Ave, ME  
 App #: 164923, Rev 1

## Reactions

Moment:	1892.1	ft-kips
Axial:	52.753	kips
Shear:	29.675	kips
Exterior Flange Run, T+q:	33.6	kips

## Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 \cdot A_b \cdot F_u)$
$\phi = 0.75, \phi \cdot V_n$ (kips):
38.88

Manufacturer: Other

Elevation: 20 feet

## Bolt Data

Qty:	52		
Diam:	1	Bolt Fu:	120
Bolt Material:	A325	Bolt Fy:	92
N/A:		<-- Disregard	
N/A:		<-- Disregard	
Circle:	50.375	in	

## Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 33.7 Kips, Ext. Tu=Interior Tu  
 Adjusted  $\phi \cdot T_n$  (due to  $V_u = V_u / Q_{ty}$ ), 54.5 Kips  
 Bolt Stress Ratio: 61.7% Pass

## Plate Data

Plate Outer Diam:	52.75	in
Plate Inner Diam:	48.25	in (Hole @ Ctr)
Thick:	2.5	in
Grade:	36	ksi
Effective Width:	3.19	in

## Interior Flange Plate Results

Controlling Bolt Axial Force: 35.7 Kips, Ext. Cu=Interior Cu  
 Plate Stress: 8.5 ksi  
 Allowable Plate Stress,  $\phi \cdot F_y$ : 32.4 ksi  
 Plate Stress Ratio: 26.3% Pass

## Flexural Check

## Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

n/a

## Stiffener Results

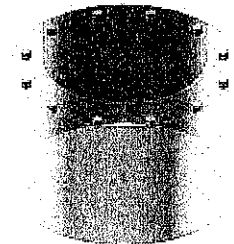
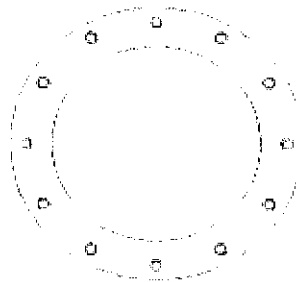
Horizontal Weld: n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a

## Pole Results

Pole Punching Shear Check: n/a

## Pole Data

Pole OuterDiam:	54	in
Thick:	0.625	in
Pole Inner Diam:	52.75	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

# Stiffened or Unstiffened, Ungrouted, Circular Base Plate - Any Rod Material

**TIA Rev G** Assumption: Clear space between bottom of leveling nut and top of concrete not exceeding (1)\*(Rod Diameter)

## Site Data

BU#:	878782
Site Name:	Portland Warren Ave, ME
App #:	164923, Rev 1
Pole Manufacturer:	Other

## Anchor Rod Data

Qty:	28	
Diam:	2	in
Rod Material:	Other	
Strength (Fu):	58	ksi
Yield (Fy):	36	ksi
Bolt Circle:	60.125	in

## Plate Data

Diam:	66	in
Thick:	3.25	in
Grade:	36	ksi
Single-Rod B-eff:	6.06	in

## Stiffener Data (Welding at both sides)

Config:	0	*
Weld Type:		
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

## Pole Data

Diam:	54	in
Thick:	0.625	in
Grade:	36	ksi
# of Sides:	0	"0" IF Round
Fu	58	ksi
Reinf. Fillet Weld	0	"0" if None

## Reactions

Mu:	3963	ft-kips
Axial, Pu:	62	kips
Shear, Vu:	31	kips
Eta Factor, η	0.5	TIA G (Fig. 4-4)

If No stiffeners, Criteria: AISC LRFD <-Only Applicable to Unstiffened Cases

## Anchor Rod Results

Max Rod (Cu+ Vu/η):	117.4 Kips
Allowable Axial, $\phi^*Fu^*Anet$ :	116.0 Kips
Anchor Rod Stress Ratio:	101.2% Pass

Rigid
AISC LRFD
$\phi^*Tn$

## Base Plate Results

Base Plate Stress:	13.7 ksi
Allowable Plate Stress:	32.4 ksi
Base Plate Stress Ratio:	42.3% Pass

## Flexural Check

Rigid
AISC LRFD
$\phi^*Fy$
Y.L. Length:
26.44

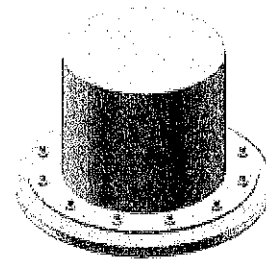
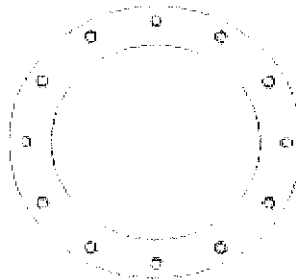
n/a

## Stiffener Results

Horizontal Weld :	n/a
Vertical Weld:	n/a
Plate Flex+Shear, $f_b/F_b+(f_v/F_v)^2$ :	n/a
Plate Tension+Shear, $f_t/F_t+(f_v/F_v)^2$ :	n/a
Plate Comp. (AISC Bracket):	n/a

## Pole Results

Pole Punching Shear Check:	n/a
----------------------------	-----



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

**(Bearing and Stability Checks) Tool for TIA Rev F or G - Application (MP, SST with unitbase)**

**Site Data**

BU#: 878782
Site Name: Portland Waren Ave, ME
App #: 164923, Rev 1
(14)#9, 2.5" dia holes, rock anchors x8'

Rock anchor uplift capacity @75psi for 5' & 150psi for below 5' bond=  
 Moment capacity of Rock anchors

Loads Already Factored		
For P (DL)	1.2	<----Disregard
For P,V, and M (WL)	1.35	<----Disregard

Pad & Pier Data		
Base PL Dist. Above Pier:	0	in
Pier Dist. Above Grade:	0	in
Pad Bearing Depth, D:	5	ft
Pad Thickness, T:	5	ft
Pad Width=Length, L:	12	ft
Pier Cross Section Shape:	Round	<--Pull Down
Enter Pier Diameter:	3	ft
Concrete Density:	150.0	pcf
Pier Cross Section Area:	7.07	ft^2
Pier Height:	0.00	ft
Soil (above pad) Height:	0.00	ft

Soil Parameters		
Unit Weight, $\gamma$ :	125.0	pcf
Ultimate Bearing Capacity, $q_n$ :	40.00	ksf
Strength Reduct. factor, $\phi$ :	0.75	
Angle of Friction, $\phi$ :	30.0	degrees
Undrained Shear Strength, $C_u$ :	0.00	ksf
Allowable Bearing: $\phi * q_n$ :	30.00	ksf
Passive Pres. Coeff., $K_p$ :	3.00	

Forces/Moments due to Wind and Lateral Soil		
Minimum of ( $\phi * \text{Ultimate Pad Passive Force, } V_u$ ):	31.0	kips
Pad Force Location Above D:	1.67	ft
$\phi$ (Passive Pressure Moment):	51.67	ft-kips
Factored O.T. M(WL), "1.6W":	525.7	ft-kips
Factored OT (MW-Msoil), M1	474.08	ft-kips

Resistance due to Foundation Gravity		
Soil Wedge Projection grade, a:	0.00	ft
Sum of Soil Wedges Wt:	0.00	kips
Soil Wedges ecc, K1:	0.00	ft
Ftg+Soil above Pad wt:	108.0	kips
Unfactored (Total ftg-soil Wt):	108.00	kips
1.2D. <b>No Soil Wedges.</b>	191.60	kips
0.9D. <b>With Soil Wedges</b>	143.70	kips

Resistance due to Cohesion (Vertical)		
$\phi * (1/2 * C_u)$ (Total Vert. Planes)	0.00	kips

Monopole Base Reaction Forces		
TIA Revision:	G	<--Pull Down
Factored DL Axial, PDU:	62	kips
Factored WL Axial, PWu:	0	kips
Factored WL Shear, Vu:	31	kips
Factored WL Moment, Mu:	370.7459	ft-kips
Factored WL Moment, Mu:	3963	ft-kips

77.75442 Kips  
 3592.254 ft-kips

Load Factor	Shaft Factored Loads	
1.00	1.2D+1.6W, Pu:	62 kips
0.90	0.9D+1.6W, Pu:	46.5 kips
1.00	Vu:	31 kips
	Mu:	370.7459 ft-kips

**1.2D+1.6W Load Combination, Bearing Results:**

(No Soil Wedges)		
[Reaction+Conc+Soil]	191.60	P1="1.2D+1.6W" (Kips)
Factored "1.6W" Overturning Moment (MW-Msoil), M1	474.08	ft-kips

Orthogonal Direction:

$ecc1 = M1/P1 = 2.47$  ft  
 Orthogonal  $qu = 2.43$  ksf  
 $qu/\phi * q_n$  Ratio= **8.09%** Pass

Diagonal Direction:

$ecc2 = (0.707M1)/P1 = 1.75$  ft  
 Diagonal  $qu = 2.65$  ksf  
 $qu/\phi * q_n$  Ratio= **8.84%** Pass

**Run** <-- Press Upon Completing All Input

**Overturning Stability Check**

**0.9D+1.6W Load Combination, Bearing Results:**

(w/ Soil Wedges)		
[Reaction+Conc+Soil]	143.70	P2="0.9D+1.6W" (Kips)
Factored "1.6W" Overturning Moment (MW-Msoil) - 0.9(M of Wedge + M of Cohesion), M2	474.08	ft-kips

Orthogonal  $ecc3 = M2/P2 = 3.30$  ft  
 Ortho Non Bearing Length, NBL= 6.60 ft  
 Orthogonal  $qu = 2.22$  ksf  
 Diagonal  $qu = 2.67$  ksf

Max Reaction Moment (ft-kips) so that $qu = \phi * q_n = 100\%$ Capacity Rating			
Actual M:	370.75		
M Orthogonal:	730.19	<b>50.77%</b>	<b>Pass</b>

Cohesion Force Eccentricity, K2	0.00	ft
---------------------------------	------	----

M Diagonal:	730.19	<b>50.77%</b>	<b>Pass</b>
-------------	--------	---------------	-------------

**APPENDIX D**  
**TOWER MODIFICATION DRAWINGS**