

Tighe&Bond

Proposed Neighborhood Center 1342 Congress Street Portland, ME

Drainage Study

Prepared For:

Jewish Community Alliance of Southern Maine

Last Revised June 23, 2015

Section 1 N	larrative	
1.1	On Site Soil Description	1-1
Section 2 D	Drainage Analysis	
2.1	Calculation Methods	2-1
2.2	Pre-Development Conditions	
	2.2.1 Pre-Development Calculations	2-2
	2.2.2 Pre-Development Watershed Plan, WS-1	2-2
2.3	Post-Development Conditions	
	2.3.1 Post-Development Calculations	2-4
	2.3.2 Post-Development Watershed Plan, WS-2	2-4
2.4	Peak Rate Comparisons	
2.5	Stormwater Treatment Volume	2-6
2.6	Mitigation Description and Best Management Practices	2-6
Section 3 L	ong Term Operation & Maintenance Plan	
3.1	Contact/Responsible Party	3-1
3.2	Maintenance Items	3-1
3 3	Overall Site Operation & Maintenance Schedule	3-2

Appendices

- A Plans Bound Separately
- B Precipitation Table
- C Boring Logs

J:\J\J0096 Jewish Community Alliance\DRAINAGE\DRAINAGE STUDIES\Revised 6-23-15\J0096-Drainage Study-(Revised 6-23-15).doc

Section 1 Narrative

The proposed project consists on the construction of a one (1) story Neighborhood Center on a 2.16 acre lot in the R-5 Residential Zone There will also be associated site improvements that include surface parking lot, utilities, site lighting, landscaping, and stormwater management system.

The site is currently developed with a 14,960 SF Church that includes associated parking lot and driveways. The existing building and parking lot will be demolished as part of the proposed project. Currently, the runoff from the majority of the site including the parking lot and roof flows to the south of the property where it enters an existing drainage swale. Due to the lack of any stormwater treatment infrastructure, all runoff leaves the site untreated.

The proposed project includes substantial improvements to manage and treat runoff through the use of Stormtech Chambers and an underdrained soil filter bed. The proposed redevelopment will increase impervious area by approximately 12,500 SF. The proposed stormwater management system has been designed to mitigate additional impervious areas by decreasing peak runoff rates for the 2-year, 10-year, and 25-year design storms.

The proposed stormwater management system has been designed to meet the requirements and design principles outlined in the City of Portland Technical Manual and the Maine Stormwater Best Management Practices Manual.

1.1 On Site Soil Description

Section 7 of the City of Portland Technical Manual requires a Soil Survey be completed by a Maine Certified Soil Scientist for Level III Site Plan Submissions. We are requesting a waiver from this requirement as soil borings were completed as part of a Phase I/II Environmental Site Assessment at this site. Based on the soil information the runoff analyzed within this study area has been modeled assuming Class C soils. The boring logs have been included in the Appendix of this report. Due to the low infiltration rates associated with Class C soils, the drainage design has been completed assuming no exfiltration.

Section 2 Drainage Analysis

2.1 Calculation Methods

The design storms analyzed in this study are the 2-year, 10-year and 50-year 24-hour duration storm events. The stormwater modeling system, HydroCAD 10.0 was utilized to predict the peak runoff rates from these storm events. A Type III storm pattern was used in the model.

The time of concentration was computed using the TR-55 Method, which provides a means of determining the time for an entire watershed to contribute runoff to a specific location via sheet flows, shallow concentrated flow and channel flow. Runoff curve numbers were calculated by estimating the coverage areas and then summing the curve number for the coverage area as a percent of the entire watershed.

References:

1. HydroCAD Stormwater Modeling System, by HydroCAD Software Solutions LLC, Chocorua, New Hampshire.

2.2 Pre-Development Conditions

Pre-development conditions are considered, for this study, to be the conditions of the site prior to the start of the ongoing excavation operations. In order to analyze the pre-development condition, the site has been divided into three (3) contributing watershed areas modeled at three (3) points of analysis. These points of analysis and watersheds are depicted on the plan entitled "Pre-Development Watershed Plan", Sheet WS-1.

Each of the points of analysis and their contributing watershed areas are described below:

Point of Analysis (PA-1)

Point of Analysis One (PA-1) is comprised of Pre-Development Watershed 1 (WS-1), which accounts for approximately 75% of the total watershed area. WS-1 consists of runoff generated from a portion of the roof of the existing building, parking lot, driveway, and grass/wooded areas at the south side of the parcel. Runoff travels in a southwestern direction via overland flow where it enters an existing drainage swale at PA-1.

Point of Analysis (PA-2)

Point of Analysis Two (PA-2) is comprised of Pre-Development Watershed 2 (WS-2). WS-2 consists primarily of runoff generated from the roof of the existing building, sidewalks, and grass areas. Runoff travels west via overland flow onto the adjacent parking lot of Westgate Plaza at PA-2.

Point of Analysis (PA-3)

Point of Analysis Three (PA-3) is comprised of Pre-Development Watershed 3 (WS-3). WS-3 consists of runoff generated from the driveway and grass on the north side of the site. Runoff generated travels via overland flow north onto Congress Street and eventually into the City's closed drainage system.

Point of Analysis (PA-4)

Point of Analysis Four (PA-4) is comprised of the existing roof of the Chruch. The roof leaders are connected to the sanitary sewer on site for a combined sewer/stormwater system. The combined sewer/stormwater ultimately discharges into the sewer system in Congress Street. The configuration of the existing roof drainage system was verified in the field via camera inspection and dye flow testing. The City of Portland does not permit stormwater runoff to be conveyed into the City sewer system, so this connection will only be re-used for sanitary sewer for the proposed development.

2.2.1 Pre-Development Calculations

2.2.2 Pre-Development Watershed Plan, WS-1



Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
1.106	74	>75% Grass cover, Good, HSG C (WS-1, WS-2, WS-3)
0.490	98	Paved parking, HSG C (WS-1, WS-2, WS-3)
0.355	98	Roofs, HSG C (ROOF)
0.227	72	Woods/grass comb., Good, HSG C (WS-1)
2.179	83	TOTAL AREA

Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
2.179	HSG C	ROOF, WS-1, WS-2, WS-3
0.000	HSG D	
0.000	Other	
2.179		TOTAL AREA

J0096-PRE
Prepared by Tighe & Bond
HydroCAD® 10.00 s/n 03436 © 2013 HydroCAD Software Solutions LLC

Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment ROOF:	Flow Length=50'	Runoff Area=15,47 Slope=0.0400 '/'	70 sf 100.00 Tc=5.0 min	% Impervious CN=98 Ru	s Runoff Dep noff=1.07 cfs	oth>2.77" 0.082 af
Subcatchment WS-1:	I	Runoff Area=64,3 Flow Length=451'	314 sf 25.78 Tc=7.6 min	% Impervious CN=80 Ru	s Runoff Dep noff=2.01 cfs	oth>1.25" 0.154 af
Subcatchment WS-2:	Flow Length=44'	Runoff Area=5,3 Slope=0.0150 '/'	325 sf 25.60 Tc=5.9 min	% Impervious CN=80 Ru	Runoff Dep noff=0.18 cfs	oth>1.25" 0.013 af
Subcatchment WS-3:		Runoff Area=9, Flow Length=87'	792 sf 34.74 Tc=5.0 min	% Impervious CN=82 Ru	Runoff Dep noff=0.37 cfs	oth>1.38" 0.026 af
Link PA1:				In Prin	flow=2.01 cfs hary=2.01 cfs	0.154 af 0.154 af
Link PA2:				In Prin	flow=0.18 cfs hary=0.18 cfs	0.013 af 0.013 af
Link PA3:				In [.] Prin	flow=0.37 cfs nary=0.37 cfs	0.026 af 0.026 af
Link PA4: Congress Street	Sewer			ln [.] Prin	flow=1.07 cfs nary=1.07 cfs	0.082 af 0.082 af

Total Runoff Area = 2.179 ac Runoff Volume = 0.274 af Average Runoff Depth = 1.51" 61.20% Pervious = 1.333 ac 38.80% Impervious = 0.845 ac

Summary for Subcatchment ROOF:

Runoff = 1.07 cfs @ 12.07 hrs, Volume= 0.082 af, Depth> 2.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.00"

A	rea (sf)	CN	Description					
	15,470	98	Roofs, HSG	S C				
	15,470		100.00% Im	pervious A	rea			
Tc (min)	Length (feet)	Slope (ft/ft)	e Velocity (ft/sec)	Capacity (cfs)	Description			
4.4	50	0.0400	0.19	• •	Sheet Flow, Grass: Short	n= 0.150	P2= 3.00"	
4.4	50	Total,	Increased t	o minimum	Tc = 5.0 min			

Summary for Subcatchment WS-1:

Runoff = 2.01 cfs @ 12.11 hrs, Volume= 0.154 af, Depth> 1.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.00"

Α	rea (sf)	CN	Description			
	16,583	98	Paved park	ing, HSG C)	
	37,846	74 :	>75% Gras	s cover, Go	ood, HSG C	
	9,885	72	Woods/gras	ss comb., G	Good, HSG C	_
	64,314	80	Weighted A	verage		
	47,731		74.22% Pei	vious Area		
	16,583	:	25.78% Imp	pervious Are	ea	
_						
Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
4.4	50	0.0400	0.19		Sheet Flow,	
					Grass: Short n= 0.150 P2= 3.00"	
0.4	90	0.0320	3.63		Shallow Concentrated Flow,	
					Paved Kv= 20.3 fps	
2.8	311	0.0150	1.84		Shallow Concentrated Flow,	
					Grassed Waterway Kv= 15.0 fps	
7.6	451	Total				

Summary for Subcatchment WS-2:

Runoff = 0.18 cfs @ 12.09 hrs, Volume= 0.013 af, Depth> 1.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.00"

Type III 24-hr 2-YR Rainfall=3.00" Printed 6/23/2015 Page 6

J0096-PRE

Prepared by Tighe & Bond HydroCAD® 10.00 s/n 03436 © 2013 HydroCAD Software Solutions LLC

A	rea (sf)	CN	Description					
	1,363	98	Paved park	ing, HSG C	;			
	3,962	74 :	>75% Gras	s cover, Go	ood, HSG C			
	5,325 3,962 1,363	80	Weighted A 74.40% Pei 25.60% Imp	verage vious Area pervious Are	ea			
Tc (min)	Length	Slope	Velocity	Capacity	Description			
	44	0.0150	0.12	(00)	Shoot Flow			
5.9	44	0.0150	0.12		Grass: Short	n= 0.150	P2= 3.00"	

Summary for Subcatchment WS-3:

Runoff = 0.37 cfs @ 12.08 hrs, Volume= 0.026 af, Depth> 1.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.00"

A	Area (sf)	<u>CN</u> E	Description		
	3,402	98 F	aved park	ing, HSG C)
	6,390	74 >	75% Gras	s cover, Go	ood, HSG C
	9,792	82 V	Veighted A	verage	
	6,390	6	5.26% Per	vious Area	
	3,402	3	4.74% Imp	pervious Are	ea
Тс	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.3	30	0.0500	1.51		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.00"
0.3	57	0.0350	2.81		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
0.6	87	Total, I	ncreased t	o minimum	Tc = 5.0 min

Summary for Link PA1:

Inflow Area	a =	1.476 ac, 2	25.78% Impe	ervious,	Inflow Dep	pth > 1.	.25" for	2-YF	R event	
Inflow	=	2.01 cfs @	12.11 hrs,	Volume	=	0.154 af				
Primary	=	2.01 cfs @	12.11 hrs,	Volume	=	0.154 af,	, Atten=	0%,	Lag= 0.0	min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA2:

Inflow Ar	ea =	0.122 ac, 2	25.60% Imp	ervious,	Inflow Dep	oth > 1.2	25" for 2	2-YR event	
Inflow	=	0.18 cfs @	12.09 hrs,	Volume	= (0.013 af			
Primary	=	0.18 cfs @	12.09 hrs,	Volume	= (0.013 af,	Atten= 09	%, Lag= 0.0 n	nin

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA3:

Inflow /	Area =	0.225 ac,	34.74% Imperviou	us, Inflow Depth >	1.38" for 2-	YR event
Inflow	=	0.37 cfs @	12.08 hrs, Volu	me= 0.026	af	
Primary	y =	0.37 cfs @	12.08 hrs, Volu	me= 0.026	af, Atten= 0%	, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA4: Congress Street Sewer

Inflow Area	a =	0.355 ac,10	0.00% Imp	ervious,	Inflow De	epth > 2	2.77"	for 2-Y	R event	
Inflow	=	1.07 cfs @	12.07 hrs,	Volume	=	0.082 a	ıf			
Primary	=	1.07 cfs @	12.07 hrs,	Volume	=	0.082 a	if, Atte	en= 0%,	Lag= 0.0 mi	in

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

J0096-PRE	7
Prepared by Tighe & Bond	
HydroCAD® 10.00 s/n 03436 © 2013 HydroCAD Software Solutions LLO	С

Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment ROOF:	Flow Length=50'	Runoff Area=15,47 Slope=0.0400 '/'	′0 sf 100.00 Tc=5.0 min	% Impervious CN=98 Rur	Runoff Dep noff=1.69 cfs	oth>4.46" 0.132 af
Subcatchment WS-1:	I	Runoff Area=64,3 Flow Length=451'	314 sf 25.78 Tc=7.6 min	% Impervious CN=80 Rur	Runoff Dep noff=4.31 cfs	oth>2.63" 0.323 af
Subcatchment WS-2:	Flow Length=44'	Runoff Area=5,3 Slope=0.0150 '/'	825 sf 25.60 Tc=5.9 min	% Impervious CN=80 Rur	Runoff Dep noff=0.38 cfs	oth>2.63" 0.027 af
Subcatchment WS-3:		Runoff Area=9,7 Flow Length=87'	′92 sf 34.74 Tc=5.0 min	% Impervious CN=82 Rur	Runoff Dep noff=0.77 cfs	oth>2.81" 0.053 af
Link PA1:				Infl Prim	ow=4.31 cfs ary=4.31 cfs	0.323 af 0.323 af
Link PA2:				Infl Prim	ow=0.38 cfs ary=0.38 cfs	0.027 af 0.027 af
Link PA3:				Infl Prim	ow=0.77 cfs ary=0.77 cfs	0.053 af 0.053 af
Link PA4: Congress Street	Sewer			Infl Prim	ow=1.69 cfs ary=1.69 cfs	0.132 af 0.132 af

Total Runoff Area = 2.179 ac Runoff Volume = 0.535 af Average Runoff Depth = 2.95" 61.20% Pervious = 1.333 ac 38.80% Impervious = 0.845 ac

Summary for Subcatchment ROOF:

Runoff = 1.69 cfs @ 12.07 hrs, Volume= 0.132 af, Depth> 4.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=4.70"

Α	rea (sf)	CN	Description					
	15,470	98	Roofs, HSG	S C				
	15,470		100.00% Im	npervious A	rea			
Tc (min)	Length (feet)	Slope (ft/ft	velocity (ft/sec)	Capacity (cfs)	Description			
4.4	50	0.0400	0.19		Sheet Flow,	m- 0 150		
					Grass: Short	n = 0.150	PZ= 3.00 ^{°°}	
4.4	50	Total,	Increased t	o minimum	Tc = 5.0 min			

Summary for Subcatchment WS-1:

Runoff = 4.31 cfs @ 12.11 hrs, Volume= 0.323 af, Depth> 2.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=4.70"

A	rea (sf)	CN	Description			_
	16,583	98	Paved park	ing, HSG C	;	
	37,846	74	>75% Gras	s cover, Go	ood, HSG C	
	9,885	72	Woods/gras	ss comb., G	Good, HSG C	_
	64,314	80	Weighted A	verage		
	47,731		74.22% Pei	vious Area		
	16,583		25.78% Imp	pervious Are	ea	
Тс	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		_
4.4	50	0.0400	0.19		Sheet Flow,	
					Grass: Short n= 0.150 P2= 3.00"	
0.4	90	0.0320	3.63		Shallow Concentrated Flow,	
					Paved Kv= 20.3 fps	
2.8	311	0.0150	1.84		Shallow Concentrated Flow,	
					Grassed Waterway Kv= 15.0 fps	_
7.6	451	Total				

Summary for Subcatchment WS-2:

Runoff = 0.38 cfs @ 12.09 hrs, Volume= 0.027 af, Depth> 2.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=4.70"

J0096-PRE

 Type III 24-hr
 10-YR Rainfall=4.70"

 Printed
 6/23/2015

 C
 Page 10

Prepared by Tighe & Bond HydroCAD® 10.00 s/n 03436 © 2013 HydroCAD Software Solutions LLC

A	rea (sf)	CN	Description						
	1,363	98	Paved park	ing, HSG C	;				
	3,962	74	>75% Gras	s cover, Go	ood, HSG C				
	5,325	80	Weighted A	verage					
	3,962		74.40% Per	vious Area					
	1,363		25.60% Impervious Area						
-		0	N / 1 · · ·	0	D				
IC	Length	Slope	e Velocity	Capacity	Description				
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)					
5.9	44	0.0150	0.12		Sheet Flow,				
					Grass: Short	n= 0.150	P2= 3.00"		

Summary for Subcatchment WS-3:

Runoff = 0.77 cfs @ 12.07 hrs, Volume= 0.053 af, Depth> 2.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=4.70"

A	Area (sf)	<u>CN</u> E	Description							
	3,402	98 F	aved park	ing, HSG C)					
	6,390	74 >	75% Gras	s cover, Go	ood, HSG C					
	9,792	82 V	Veighted A	verage						
	6,390	6	5.26% Per	vious Area						
	3,402	3	34.74% Impervious Area							
Тс	Length	Slope	Velocity	Capacity	Description					
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)						
0.3	30	0.0500	1.51		Sheet Flow,					
					Smooth surfaces n= 0.011 P2= 3.00"					
0.3	57	0.0350	2.81		Shallow Concentrated Flow,					
					Grassed Waterway Kv= 15.0 fps					
0.6	87	Total, I	ncreased t	o minimum	Tc = 5.0 min					

Summary for Link PA1:

Inflow Area	a =	1.476 ac, 2	25.78% Impe	ervious,	Inflow Dep	th > 2.6	63" for 1	0-YR event
Inflow	=	4.31 cfs @	12.11 hrs,	Volume	= 0	.323 af		
Primary	=	4.31 cfs @	12.11 hrs,	Volume	= 0	.323 af,	Atten= 0%	6, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA2:

Inflow /	Area	=	0.122 ac,	25.60% Imp	ervious,	Inflow Depth	> 2.6	63" for	10-YR	event
Inflow	=	=	0.38 cfs @	12.09 hrs,	Volume	= 0.0)27 af			
Primar	y =	=	0.38 cfs @	12.09 hrs,	Volume	= 0.0)27 af,	Atten= ()%, La	g= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA3:

Inflow A	vrea =	0.225 ac, 3	34.74% Imperv	vious, Inflow	Depth > 2.8°	1" for 10-`	YR event
Inflow	=	0.77 cfs @	12.07 hrs, V	/olume=	0.053 af		
Primary	=	0.77 cfs @	12.07 hrs, V	/olume=	0.053 af, 7	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA4: Congress Street Sewer

Inflow Area	ı =	0.355 ac,10	0.00% Imp	ervious,	Inflow De	epth >	4.46"	for 10-	YR eve	ent
Inflow	=	1.69 cfs @	12.07 hrs,	Volume	=	0.132 a	af			
Primary	=	1.69 cfs @	12.07 hrs,	Volume	=	0.132 a	af, At	ten= 0%,	Lag=	0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

J0096-PRE	7
Prepared by Tighe & Bond	
HydroCAD® 10.00 s/n 03436 © 2013 HydroCAD Software Solutions L	LC

Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment ROOF:	Flow Length=50'	Runoff Area=15,4 Slope=0.0400 '/'	70 sf 100.00 Tc=5.0 min	% Impervious CN=98 Ru	s Runoff Dep noff=1.98 cfs	oth>5.26" 0.156 af
Subcatchment WS-1:	I	Runoff Area=64, Flow Length=451'	314 sf 25.78 Tc=7.6 min	% Impervious CN=80 Ru	s Runoff Dep noff=5.45 cfs	oth>3.33" 0.410 af
Subcatchment WS-2:	Flow Length=44'	Runoff Area=5,3 Slope=0.0150 '/'	325 sf 25.60 Tc=5.9 min	% Impervious CN=80 Ru	s Runoff Dep noff=0.48 cfs	oth>3.33" 0.034 af
Subcatchment WS-3:		Runoff Area=9, Flow Length=87'	792 sf 34.74 Tc=5.0 min	% Impervious CN=82 Ru	s Runoff Dep noff=0.96 cfs	oth>3.53" 0.066 af
Link PA1:				In Prin	flow=5.45 cfs nary=5.45 cfs	0.410 af 0.410 af
Link PA2:				In Prin	flow=0.48 cfs hary=0.48 cfs	0.034 af 0.034 af
Link PA3:				In Prin	flow=0.96 cfs nary=0.96 cfs	0.066 af 0.066 af
Link PA4: Congress Street	Sewer			In Prin	flow=1.98 cfs nary=1.98 cfs	0.156 af 0.156 af

Total Runoff Area = 2.179 ac Runoff Volume = 0.665 af Average Runoff Depth = 3.66" 61.20% Pervious = 1.333 ac 38.80% Impervious = 0.845 ac

Summary for Subcatchment ROOF:

Runoff = 1.98 cfs @ 12.07 hrs, Volume= 0.156 af, Depth> 5.26"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.50"

Α	rea (sf)	CN	Description					
	15,470	98	Roofs, HSG	S C				
	15,470		100.00% Im	npervious A	rea			
Tc (min)	Length (feet)	Slope (ft/ft	velocity (ft/sec)	Capacity (cfs)	Description			
4.4	50	0.0400	0.19		Sheet Flow,	m- 0 150		
					Grass: Short	n = 0.150	PZ= 3.00 ^{°°}	
4.4	50	Total,	Increased t	o minimum	Tc = 5.0 min			

Summary for Subcatchment WS-1:

Runoff = 5.45 cfs @ 12.11 hrs, Volume= 0.410 af, Depth> 3.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.50"

A	rea (sf)	CN	Description				
	16,583	98	Paved park	ing, HSG C	:		
	37,846	74	>75% Gras	s cover, Go	ood, HSG C		
	9,885	72	Woods/gras	ss comb., G	Good, HSG C	_	
	64,314	80	Weighted A	verage			
	47,731 74.22% Pervious Area						
	16,583 25.78% Impervious Area						
Тс	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
4.4	50	0.0400	0.19		Sheet Flow,		
					Grass: Short n= 0.150 P2= 3.00"		
0.4	90	0.0320	3.63		Shallow Concentrated Flow,		
					Paved Kv= 20.3 fps		
2.8	311	0.0150	1.84		Shallow Concentrated Flow,		
					Grassed Waterway Kv= 15.0 fps		
7.6	451	Total					

Summary for Subcatchment WS-2:

Runoff = 0.48 cfs @ 12.09 hrs, Volume= 0.034 af, Depth> 3.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.50"

J0096-PRE

 Type III 24-hr
 25-YR Rainfall=5.50"

 Printed
 6/23/2015

 C
 Page 14

Prepared by Tighe & Bond HydroCAD® 10.00 s/n 03436 © 2013 HydroCAD Software Solutions LLC

A	rea (sf)	CN	Description					
	1,363	98	Paved park	ing, HSG C	;			
	3,962	74	>75% Gras	s cover, Go	ood, HSG C			
	5,325	80	Weighted A	verage				
	3,962		74.40% Per	vious Area				
	1,363		25.60% Imp	pervious Ar	ea			
Та	Longth	Clone	Volocity	Consoitu	Description			
IC (min)	Lengin	Siope		Capacity	Description			
<u>(min)</u>	(leet)	(ועונ) (II/sec)	(CIS)				
5.9	44	0.0150	0.12		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.00"	

Summary for Subcatchment WS-3:

Runoff = 0.96 cfs @ 12.07 hrs, Volume= 0.066 af, Depth> 3.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.50"

A	rea (sf)	CN E	Description		
	3,402	98 F	Paved park	ing, HSG C	;
	6,390	74 >	75% Gras	s cover, Go	ood, HSG C
	9,792	82 V	Veighted A	verage	
	6,390	6	5.26% Per	vious Area	
	3,402	3	4.74% Imp	pervious Are	ea
Тс	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.3	30	0.0500	1.51		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.00"
0.3	57	0.0350	2.81		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
0.6	87	Total, I	ncreased t	o minimum	Tc = 5.0 min

Summary for Link PA1:

Inflow Area	a =	1.476 ac, 2	25.78% Impe	ervious,	Inflow Dept	h> 3.3	33" for 25	-YR event
Inflow	=	5.45 cfs @	12.11 hrs,	Volume	= 0.	410 af		
Primary	=	5.45 cfs @	12.11 hrs,	Volume	= 0.	410 af,	Atten= 0%	, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA2:

Inflow A	Area =	0.122 ac, 2	25.60% Impe	ervious,	Inflow Depth	<mark>ו> 3</mark> .3	33" for 2	5-YR eve	nt
Inflow	=	0.48 cfs @	12.09 hrs,	Volume	= 0.0	034 af			
Primary	/ =	0.48 cfs @	12.09 hrs,	Volume	= 0.0	034 af,	Atten= 0%	%, Lag= 0	.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA3:

Inflow /	Area =	0.225 ac,	34.74% Imp	ervious,	Inflow Dep	th > 3.5	53" for 25-	YR event
Inflow	=	0.96 cfs @	12.07 hrs,	Volume	= 0	.066 af		
Primar	y =	0.96 cfs @	12.07 hrs,	Volume	= 0	.066 af,	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA4: Congress Street Sewer

Inflow Area	ı =	0.355 ac,10	0.00% Imp	ervious,	Inflow De	epth >	5.26"	for 25-	YR event
Inflow	=	1.98 cfs @	12.07 hrs,	Volume	=	0.156	af		
Primary	=	1.98 cfs @	12.07 hrs,	Volume	=	0.156	af, At	ten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs



2.3 Post-Development Conditions

The post-development drainage condition is also characterized by three (3) watershed areas modeled at the same three (3) points of analysis as the pre-development condition. These three (3) watershed areas are depicted on the Post-Development Watershed Plan, WS-2.

Point of Analysis (PA-1)

Point of Analysis One (PA-1) is comprised Post-Development Watershed 1A (WS-1A), Watershed 1B (WS-1B), and Watershed 1C (WS-1C). WS-1A consists of the proposed parking lot, sidewalks, and landscaped areas in the southwestern side of the site. Runoff from WS-1A travels via sheetflow into the underdrained soil filter bed to the rear of the parking lot.

WS-1B is a redeveloped area as the characteristics of this watershed remain largely unchanged from the pre-development condition. This watershed consists of the driveway that provides access to Congress Street, a small portion of sidewalk near the proposed building, and lawn at the south side of the site. Runoff generated travels via overland flow in the same pattern as the pre-development condition to PA-1.

WS-1C consists of the roof of the proposed building and the designated play area directly adjacent to the building. Runoff generated from the roof and play area is collected and conveyed to an underground detention area in the parking lot. Detained stormwater is conveyed via closed drainage to PA-1.

Point of Analysis (PA-2)

Point of Analysis Two (PA-2) is comprised of Post-Development Watershed 2 (WS-2A). WS-2 consists of runoff generated from the lawn and landscaping on the west side of the building. The runoff travels via overland flow in the same pattern as the pre-development condition.

Point of Analysis (PA-3)

Point of Analysis Three (PA-3) is comprised of Post Development Watershed 3 (WS-3). WS-3 is comprised of the sidewalk and landscaped areas along Congress Street. The runoff generated travels via overland flow in the same pattern as the pre-development condition.

2.3.1 Post-Development Calculations

2.3.2 Post-Development Watershed Plan, WS-2

2.4 Peak Rate Comparisons

The following table summarizes and compares the pre- and post-development peak runoff rates for the 2-year, 10-year, and 25-year storm events. The post-development peak rate of runoff for each discharge point has been determined to be less than the peak runoff rate generated during the pre-development condition.

Point of Analysis	Pre/ Post 2-Year Storm (cfs)	Pre/ Post 10-Year Storm (cfs)	Pre/ Post 25-Year Storm (cfs)
PA1	2.01/ 2.01	4.31/ 3.73	5.45/ 4.50
PA2	0.18/ 0.11	0.38/ 0.24	0.48/ 0.31
PA3	0.37/ 0.14	0.77/ 0.31	0.96/ 0.40
PA4 (Roof)	1.07/ 0.0	1.69/ 0.0	1.98/ 0.0

2.5 Stormwater Treatment Volume

Table 6.1 - Underdrained Soil Filter							
Treatment Volume Calculations							
VARIABLE	DESCRIPTION	VALUE					
Pi	1 Inch of Rainfall for Impervious Area	1 inch					
Pv	0.4 Inch of Rainfall for Vegetated Area	0.4 inch					
А	Total Area Draining to Design Structure	23,512 SF					
Ai	Impervious Area Draining to Design Structure	14,558 SF					
Av	Vegetated Area Draining to Design Structure	9,104 SF					
ITV	Impervious Area Treatment Volume = Pi*Ai	1,213 CF					
ντν	Vegetated Area Treatment Volume = Pv*Av	304 CF					
	Total Treatment Volume Required	1,517 CF					
Vs	Total Treatment Volume Provided (see HydroCAD)	2,754 CF					

The Treatment Volume provided is greater than the Treatment Volume required. The total storage volume provided below the overflow rim elevation is 2,754 CF. The proposed Underdrained Soil Filter is treating a total of 14,558 SF of impervious area, which is equivalent to approximately 115% of the new impervious area and exceeds the requirements of the MaineDEP Chapter 500 General Standards.

Stage-Area-Storage for Pond 3P: Underdrained Soil Filter (continued)

Elevation	Storage	Elevation	Storage	Elevation	Storage
(feet)	(cubic-feet)	(feet)	(cubic-feet)	(feet)	(cubic-feet)
100.33	1,373	100.86	2,162	101.39	3,118
100.34	1,386	100.87	2,178	101.40	3,138
100.35	1,400	100.88	2,194	101.41	3,158
100.36	1,413	100.89	2,211	101.42	3,178
100.37	1,427	100.90	2,228	101.43	3,198
100.38	1,441	100.91	2,244	101.44	3,218
100.39	1,454	100.92	2,261	101.45	3,238
100.40	1,400	100.93	2,270		0 3,200 2 2 270
100.41	1,402	100.94	2,294	101.47	3 200
100.42	1,490	100.95	2,311	101.40	3,299
100.43	1,510	100.00	2,325	101.40	3 340
100.45	1,538	100.98	2,362	101.00	0,040
100.46	1,552	100.99	2,379		
100.47	1.566	101.00	2.397		
100.48	1,580	101.01	2,414		
100.49	1,594	101.02	2,431		
100.50	1,609	101.03	2,448		
100.51	1,623	101.04	2,466		
100.52	1,637	101.05	2,483		
100.53	1,652	101.06	2,501		
100.54	1,666	101.07	2,518		
100.55	1,681	101.08	2,536		
100.56	1,696	101.09	2,554		
100.57	1,710	101.10	2,572	_	
100.58	1,725	101.11	2,590		Overflow Rim
100.59	1,740	101.12	2,608	/ 	Elevation-101 20
100.60	1,755	101.13	2,626	/ Ľ	
100.61	1,770	101.14	2,044		
100.02	1,700	101.15	2,002		
100.03	1,000	101.10	2,000		
100.04	1,810	101.17	2,030	V V	
100.66	1,800	101.10	2,735	/	
100.67	1,861	101.20	2.754		
100.68	1,876	101.21	2,772		
100.69	1,891	101.22	2,791		
100.70	1,907	101.23	2,810		
100.71	1,922	101.24	2,828		
100.72	1,938	101.25	2,847		
100.73	1,953	101.26	2,866		
100.74	1,969	101.27	2,885		
100.75	1,985	101.28	2,904		
100.76	2,001	101.29	2,923		
100.77	2,016	101.30	2,942		
100.78	2,032	101.31	2,962		
100.79	∠,U48 2.064	101.32	2,981		
100.00	2,004 2 080	101.33	3,000		
100.01	2,000	101.34	3,020 3 030		
100.82	2,007	101.36	3 059		
100.84	2,129	101.37	3,078		
100.85	2.145	101.38	3.098		
	_, •		-,		



Area Listing (all nodes)

ŀ	Area	CN	Description
(ac	res)		(subcatchment-numbers)
1.	.047	74	>75% Grass cover, Good, HSG C (WS-1A, WS-1B, WS-1C, WS-2, WS-3)
0.	.689	98	Paved parking, HSG C (WS-1A, WS-1B, WS-1C, WS-2, WS-3)
0.	.443	98	Roofs, HSG C (WS-1C)
2	.179	86	TOTAL AREA

Soil Listing (all nodes)

Area	Soil	Subcatchment
 (acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
2.179	HSG C	WS-1A, WS-1B, WS-1C, WS-2, WS-3
0.000	HSG D	
0.000	Other	
2.179		TOTAL AREA

J0096-POST
Prepared by Tighe & Bond
HydroCAD® 10.00 s/n 03436 © 2013 HydroCAD Software Solutions LLC

Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment WS-1A:	Flow Length=130'	Runoff Area=23, Slope=0.0200 '/'	662 sf 61.52 Tc=5.0 min	% Impervio CN=89 I	ous Runoff De Runoff=1.25 cfs	oth>1.90" 0.086 af
Subcatchment WS-1B:		Runoff Area=34, Flow Length=495'	411 sf 34.55 Tc=5.5 min	% Impervio CN=82 I	ous Runoff De Runoff=1.29 cfs	oth>1.38" 0.091 af
Subcatchment WS-1C:		Runoff Area=28, Flow Length=240'	650 sf 75.57 Tc=5.0 min	% Impervio CN=92 I	ous Runoff De Runoff=1.69 cfs	oth>2.16" 0.118 af
Subcatchment WS-2:	Flow Length=22'	Runoff Area=3, Slope=0.0150 '/'	505 sf 17.12 Tc=5.0 min	% Impervio CN=78 I	ous Runoff De _l Runoff=0.11 cfs	oth>1.13" 0.008 af
Subcatchment WS-3:	Flow Length=30'	Runoff Area=4, Slope=0.0200 '/'	685 sf 13.06 Tc=5.0 min	% Impervio CN=77 I	ous Runoff De Runoff=0.14 cfs	oth>1.07" 0.010 af
Pond 1P: Stormtech 310		Peak Elev=100	.15' Storage=	=2,540 cf C	Inflow=1.69 cfs)utflow=0.36 cfs	0.118 af 0.091 af
Pond 3P: Underdrained Se	oil Filter	Peak Elev=	99.84' Storag	e=916 cf C	Inflow=1.25 cfs Outflow=0.56 cfs	0.086 af 0.080 af
Pond PDMH4:	12.0" Round	Culvert n=0.013	Peak Ele L=10.0' S=0.1	ev=98.06' 0100 '/' C	Inflow=0.90 cfs outflow=0.90 cfs	0.170 af 0.170 af
Link PA1:				Р	Inflow=2.01 cfs rimary=2.01 cfs	0.261 af 0.261 af
Link PA2:				Р	Inflow=0.11 cfs rimary=0.11 cfs	0.008 af 0.008 af
Link PA3:				Р	Inflow=0.14 cfs rimary=0.14 cfs	0.010 af 0.010 af
Total Runo	ff Area = 2.179 a	c Runoff Volun	ne = 0.312 a	f Avera	ge Runoff Der	oth = 1.72"

48.05% Pervious = 1.047 ac 51.95% Impervious = 1.132 ac

Summary for Subcatchment WS-1A:

Runoff = 1.25 cfs @ 12.07 hrs, Volume= 0.086 af, Depth> 1.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.00"

A	rea (sf)	CN E	Description		
	14,558	98 F	Paved park	ing, HSG C	
	9,104	74 >	75% Gras	s cover, Go	od, HSG C
	23,662	89 V	Veighted A	verage	
	9,104	3	88.48% Per	vious Area	
	14,558	6	61.52% Imp	ervious Are	ea
_					
TC	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cts)	
0.7	50	0.0200	1.16		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	80	0.0200	2.87		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
1.2	130	Total, I	ncreased t	o minimum	Tc = 5.0 min

Summary for Subcatchment WS-1B:

Runoff = 1.29 cfs @ 12.08 hrs, Volume= 0.091 af, Depth> 1.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.00"

_	A	rea (sf)	CN [Description						
		11,890	98 F	98 Paved parking, HSG C						
_		22,521	74 >	>75% Ġras	s cover, Go	ood, HSG C				
		34,411	82 \	Neighted A	verage					
		22,521	6	65.45% Per	vious Area					
		11,890	3	34.55% Imp	pervious Are	ea				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	0.9	50	0.0125	0.96		Sheet Flow,				
						Smooth surfaces n= 0.011 P2= 3.00"				
	1.0	125	0.0110	2.13		Shallow Concentrated Flow,				
						Paved Kv= 20.3 fps				
	3.6	320	0.0100	1.50		Shallow Concentrated Flow,				
-						Grassed Waterway Kv= 15.0 fps	_			
	5.5	495	Total							

Summary for Subcatchment WS-1C:

1.69 cfs @ 12.07 hrs, Volume= Runoff = 0.118 af, Depth> 2.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.00"

Ar	ea (sf)	CN D	Description		
1	19,300	98 F	Roofs, HSG	6 C	
	2,350	98 P	aved park	ing, HSG C	;
	7,000	74 >	75% Gras	s cover, Go	ood, HSG C
2	28,650	92 V	Veighted A	verage	
	7,000	2	4.43% Per	vious Area	
2	21,650	7	5.57% Imp	pervious Are	ea
_					
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
1.1	75	0.0150	1.12		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.00"
0.9	165	0.0050	3.21	2.52	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013 Corrugated PE, smooth interior
2.0	240	Total, I	ncreased t	o minimum	Tc = 5.0 min

Summary for Subcatchment WS-2:

0.008 af, Depth> 1.13" 0.11 cfs @ 12.08 hrs, Volume= Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.00"

A	rea (sf)	CN	Description					
	2,905	74	>75% Gras	s cover, Go	od, HSG C			
	600	98	Paved park	ing, HSG C	,			
	3,505	78	Weighted A	verage				
	2,905		82.88% Pei	vious Area				
	600		17.12% Imp	pervious Are	ea			
Тс	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
3.4	22	0.0150	0.11		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.00"	
3.4	22	Total.	Increased t	o minimum	Tc = 5.0 min			

I otal, Increased to minimum I c = 5.0 min

Summary for Subcatchment WS-3:

Runoff 0.14 cfs @ 12.08 hrs, Volume= 0.010 af, Depth> 1.07" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.00"

J0096-POST

Prepared by Tigl	ne & Bon	d		
HydroCAD® 10.00	s/n 03436	© 2013 HydroCAD	Software Solutions LL	С

A	rea (sf)	CN	Description						
	612	98	Paved park	ing, HSG C	;				
	4,073	74	>75% Ġras	s cover, Go	ood, HSG C				
	4,685	77	Weighted A	verage					
	4,073		86.94% Pei	vious Area					
	612		13.06% Imp	pervious Ar	ea				
_									
TC	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
3.9	30	0.0200	0.13		Sheet Flow,				
					Grass: Short	n= 0.150	P2= 3.00"		
3.9	30	Total,	Increased t	o minimum	Tc = 5.0 min				

Summary for Pond 1P: Stormtech 310

Inflow Area	=	0.658 ac, 7	75.57% Impe	ervious,	Inflow	Depth >	2.16"	for 2	-YR ever	nt
Inflow	=	1.69 cfs @	12.07 hrs,	Volume	=	0.118	af			
Outflow	=	0.36 cfs @	12.48 hrs,	Volume	=	0.091	af, At	ten= 79	%, Lag=	24.7 min
Primary	=	0.36 cfs @	12.48 hrs,	Volume	=	0.091	af		-	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 100.15' @ 12.48 hrs Surf.Area= 3,082 sf Storage= 2,540 cf Flood Elev= 101.50' Surf.Area= 3,082 sf Storage= 4,570 cf

Plug-Flow detention time= 177.6 min calculated for 0.091 af (76% of inflow) Center-of-Mass det. time= 95.4 min (894.0 - 798.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	98.60'	2,776 cf	38.17'W x 80.76'L x 2.83'H Field A
			8,733 cf Overall - 1,794 cf Embedded = 6,939 cf x 40.0% Voids
#2A	99.60'	1,794 cf	ADS_StormTech SC-310 x 121 Inside #1
			Effective Size= 28.9"W x 16.0"H => 2.07 sf x 7.12'L = 14.7 cf
			Overall Size= 34.0"W x 16.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 2.07 sf x 11 rows
		4.570 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	99.50'	12.0" Round Culvert L= 135.0' CPP, end-section conforming to fill, Ke= 0.500
#2 #3	Device 1 Device 1	99.50' 101.00'	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf 4.5" Vert. Orifice/Grate C= 0.600 4.0' Iong Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.36 cfs @ 12.48 hrs HW=100.15' TW=98.05' (Dynamic Tailwater)

-1=Culvert (Passes 0.36 cfs of 1.47 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.36 cfs @ 3.26 fps)

-3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 3P: Underdrained Soil Filter

Inflow Area	=	0.543 ac, 6	61.52% Impe	ervious,	Inflow Depth >	1.90"	for 2-YR	R event
Inflow	=	1.25 cfs @	12.07 hrs,	Volume=	= 0.086	af		
Outflow	=	0.56 cfs @	12.24 hrs,	Volume=	= 0.080	af, At	ten= 55%,	Lag= 9.9 min
Primary	=	0.56 cfs @	12.24 hrs,	Volume=	= 0.080	af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 99.84' @ 12.24 hrs Surf.Area= 1,945 sf Storage= 916 cf Flood Elev= 101.50' Surf.Area= 4,001 sf Storage= 3,340 cf

Plug-Flow detention time= 65.5 min calculated for 0.080 af (93% of inflow) Center-of-Mass det. time= 29.1 min (841.3 - 812.2)

Volume	Inve	ert Avail.S	Storage S	torage De	escription	
#1	100.0	0' 2	.,378 cf P	ond Stor	age (Prismat	tic)Listed below (Recalc)
#2	98.5	50'	439 cf S	oil Filter	(Prismatic)L	isted below (Recalc)
			1	,463 cf O	verall x 30.0%	% Voids
#3	97.1	5'	524 cf S	tone Res	evoir (Prism	atic)Listed below (Recalc)
			1	,309 cf O	verall x 40.0%	% Voids
		3	,340 cf T	otal Avail	able Storage	
Elevatio	n	Surf.Area	Inc.S	tore	Cum.Store	
(feet	t)	(sq-ft)	(cubic-f	eet)	(cubic-feet)	
100.0	0	1,150		0	0	
101.0	0	1,718	1,	434	1,434	
101.5	0	2,056		944	2,378	
Elevatio	n	Surf.Area	Inc.S	tore	Cum.Store	
(fee	t)	(sq-ft)	(cubic-f	eet)	(cubic-feet)	
98.5	0	975		0	0	
100.0	0	975	1,	463	1,463	
Elevatio	n	Surf.Area	Inc.St	tore	Cum.Store	
(feet	t)	(sq-ft)	(cubic-f	eet)	(cubic-feet)	
97.1	5	970		0	0	
98.5	0	970	1,	309	1,309	
Device	Routing	Inve	rt Outlet	Devices		
#1	Primary	97.6	5' 12.0 "	Round C	ulvert	
			L= 5.0'	CPP, er	nd-section co	nforming to fill, Ke= 0.500
			Inlet / C	Dutlet Inve	ert= 97.65' / 9	7.60' Š= 0.0100 '/' Cc= 0.900
			n= 0.01	13 Corrug	gated PE, sm	ooth interior, Flow Area= 0.79 sf
#2	Device 1	97.7	5' 4.0" V e	ert. Orific	e/Grate C=	0.600
#3	Device 1	101.2	0' 16.0" x Limited	to weir fl	oriz. Orifice/0 ow at low hea	Grate C= 0.600 ads
. .	o (E)	Mar. 0 50 af	40.04			

Primary OutFlow Max=0.56 cfs @ 12.24 hrs HW=99.84' TW=98.06' (Dynamic Tailwater) **1=Culvert** (Passes 0.56 cfs of 4.92 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.56 cfs @ 6.43 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond PDMH4:

 Inflow Area =
 1.201 ac, 69.22% Impervious, Inflow Depth > 1.70" for 2-YR event

 Inflow =
 0.90 cfs @ 12.32 hrs, Volume=
 0.170 af

 Outflow =
 0.90 cfs @ 12.32 hrs, Volume=
 0.170 af, Atten= 0%, Lag= 0.0 min

 Primary =
 0.90 cfs @ 12.32 hrs, Volume=
 0.170 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 98.06' @ 12.32 hrs Flood Elev= 102.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	97.50'	12.0" Round Culvert
	-		L= 10.0' CPP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 97.50' / 97.40' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.90 cfs @ 12.32 hrs HW=98.06' TW=0.00' (Dynamic Tailwater) -1=Culvert (Barrel Controls 0.90 cfs @ 2.88 fps)

Summary for Link PA1:

Inflow Are	ea =	1.991 ac, 55.46% Impervious, Inflow	Depth > 1.57"	for 2-YR event
Inflow	=	2.01 cfs @ 12.10 hrs, Volume=	0.261 af	
Primary	=	2.01 cfs @ 12.10 hrs, Volume=	0.261 af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA2:

Inflow Are	a =	0.080 ac, 1	7.12% Impervio	us, Inflow Depth >	1.13	8" for 2-Y	R event
Inflow	=	0.11 cfs @	12.08 hrs, Volu	ime= 0.008	3 af		
Primary	=	0.11 cfs @	12.08 hrs, Volu	ime= 0.008	3 af, A	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA3:

Inflow A	Area :	=	0.108 ac,	13.06% Imp	ervious,	Inflow D	epth > 1	.07" 1	or 2-Y	'R event	
Inflow	=	=	0.14 cfs @	12.08 hrs,	Volume	=	0.010 a	f			
Primary	y =	•	0.14 cfs @	12.08 hrs,	Volume	=	0.010 a	f, Atter	= 0% ,	Lag= 0.0	min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

J0096-POST	-
Prepared by Tighe & Bond	
HydroCAD® 10.00 s/n 03436 © 2013 HydroCAD Software Solutions LI	LC

Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment WS-1A:	Flow Length=130'	Runoff Area=23,6 Slope=0.0200 '/'	662 sf 61.52 Tc=5.0 min	% Imperviou CN=89 Rι	s Runoff Dep Inoff=2.24 cfs	oth>3.48" 0.158 af
Subcatchment WS-1B:		Runoff Area=34,4 Flow Length=495'	411 sf 34.55 Tc=5.5 min	% Imperviou CN=82 Rι	s Runoff Dep inoff=2.65 cfs	oth>2.81" 0.185 af
Subcatchment WS-1C:		Runoff Area=28,6 Flow Length=240'	650 sf 75.57 Tc=5.0 min	% Imperviou CN=92 Ru	s Runoff Dep Inoff=2.89 cfs	oth>3.79" 0.208 af
Subcatchment WS-2:	Flow Length=22'	Runoff Area=3, Slope=0.0150 '/'	505 sf 17.12 Tc=5.0 min	% Imperviou CN=78 Rι	s Runoff Dep Inoff=0.24 cfs	oth>2.46" 0.016 af
Subcatchment WS-3:	Flow Length=30'	Runoff Area=4,6 Slope=0.0200 '/'	685 sf 13.06 Tc=5.0 min	% Imperviou CN=77 Rι	s Runoff Dep inoff=0.31 cfs	oth>2.37" 0.021 af
Pond 1P: Stormtech 310		Peak Elev=101	.07' Storage	=4,120 cf In Out	flow=2.89 cfs tflow=0.86 cfs	0.208 af 0.179 af
Pond 3P: Underdrained So	oil Filter	Peak Elev=100	.66' Storage	=1,850 cf In Out	flow=2.24 cfs flow=0.66 cfs	0.158 af 0.151 af
Pond PDMH4:	12.0" Round	Culvert n=0.013	Peak Ele L=10.0' S=0.	ev=98.26' In 0100 '/' Out	flow=1.51 cfs flow=1.51 cfs	0.331 af 0.331 af
Link PA1:				In Prir	iflow=3.73 cfs nary=3.73 cfs	0.515 af 0.515 af
Link PA2:				In Prir	flow=0.24 cfs nary=0.24 cfs	0.016 af 0.016 af
Link PA3:				In Prir	flow=0.31 cfs nary=0.31 cfs	0.021 af 0.021 af
Total Runo	ff Area = 2.179 a	c Runoff Volun	ne = 0.588 a	f Average	Runoff Dep	th = 3.24"

48.05% Pervious = 1.047 ac 51.95% Impervious = 1.132 ac

Summary for Subcatchment WS-1A:

Runoff = 2.24 cfs @ 12.07 hrs, Volume= 0.158 af, Depth> 3.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=4.70"

A	rea (sf)	CN E	Description					
	14,558	98 F	98 Paved parking, HSG C					
	9,104	74 >	75% Gras	s cover, Go	od, HSG C			
	23,662	89 V	Veighted A	verage				
	9,104	3	8.48% Per	vious Area				
	14,558	6	1.52% Imp	ervious Are	ea			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
0.7	50	0.0200	1.16		Sheet Flow,			
					Smooth surfaces n= 0.011 P2= 3.00"			
0.5	80	0.0200	2.87		Shallow Concentrated Flow,			
					Paved Kv= 20.3 fps			
1.2	130	Total, I	ncreased t	o minimum	Tc = 5.0 min			

Summary for Subcatchment WS-1B:

Runoff = 2.65 cfs @ 12.08 hrs, Volume= 0.185 af, Depth> 2.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=4.70"

_	A	rea (sf)	CN [Description						
		11,890	98 F	Paved parking, HSG C						
_		22,521	74 >	>75% Ġras	s cover, Go	ood, HSG C				
		34,411	82 \	Neighted A	verage					
		22,521	6	65.45% Per	vious Area					
		11,890	3	34.55% Imp	pervious Are	ea				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	0.9	50	0.0125	0.96		Sheet Flow,				
						Smooth surfaces n= 0.011 P2= 3.00"				
	1.0	125	0.0110	2.13		Shallow Concentrated Flow,				
						Paved Kv= 20.3 fps				
	3.6	320	0.0100	1.50		Shallow Concentrated Flow,				
-						Grassed Waterway Kv= 15.0 fps	_			
	5.5	495	Total							

Summary for Subcatchment WS-1C:

Runoff = 2.89 cfs @ 12.07 hrs, Volume= 0.208 af, Depth> 3.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=4.70"

A	rea (sf)	CN D	Description						
	19,300	98 F	98 Roofs, HSG C						
	2,350	98 P	aved park	ing, HSG C	;				
	7,000	74 >	75% Gras	s cover, Go	ood, HSG C				
	28,650	92 V	Veighted A	verage					
	7,000	2	4.43% Per	vious Area					
	21,650	7	5.57% Imp	pervious Are	ea				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
1.1	75	0.0150	1.12		Sheet Flow,				
					Smooth surfaces n= 0.011 P2= 3.00"				
0.9	165	0.0050	3.21	2.52	Pipe Channel,				
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
					n= 0.013 Corrugated PE, smooth interior				
2.0	240	Total, I	ncreased t	o minimum	Tc = 5.0 min				

Summary for Subcatchment WS-2:

Runoff = 0.24 cfs @ 12.08 hrs, Volume= 0.016 af, Depth> 2.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=4.70"

A	rea (sf)	CN	Description					
	2,905	74	>75% Gras	s cover, Go	od, HSG C			
	600	98	Paved park	ing, HSG C	,			
	3,505	78	Weighted A	verage				
	2,905		82.88% Pei	vious Area				
	600		17.12% Imp	pervious Are	ea			
Тс	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
3.4	22	0.0150	0.11		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.00"	
3.4	22	Total,	Increased t	o minimum	Tc = 5.0 min			

Summary for Subcatchment WS-3:

Runoff = 0.31 cfs @ 12.08 hrs, Volume= 0.021 af, Depth> 2.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=4.70"

J0096-POST

Prepared by Tigl	he & Bond	b				
HydroCAD® 10.00	s/n 03436	© 2013 H	ydroCAD	Software	Solutions	LLC

A	rea (sf)	CN	Description									
	612	98	98 Paved parking, HSG C									
	4,073	74	>75% Gras	s cover, Go	ood, HSG C							
	4,685	77	77 Weighted Average									
	4,073		86.94% Pei	vious Area								
	612		13.06% Imp	pervious Ar	ea							
Тс	l enath	Slope	Velocity	Capacity	Description							
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Beeenption							
3.9	30	0.0200	0.13		Sheet Flow,							
					Grass: Short	n= 0.150	P2= 3.00"					
3.9	30	Total,	Increased t	o minimum	Tc = 5.0 min							

Summary for Pond 1P: Stormtech 310

Inflow Area	=	0.658 ac, 1	75.57% Impe	ervious,	Inflow Depth >	3.79"	for 10-Y	R event
Inflow	=	2.89 cfs @	12.07 hrs,	Volume	= 0.208	af		
Outflow	=	0.86 cfs @	12.38 hrs,	Volume	= 0.179	af, Atte	en= 70%,	Lag= 18.7 min
Primary	=	0.86 cfs @	12.38 hrs,	Volume	= 0.179	af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 101.07' @ 12.38 hrs Surf.Area= 3,082 sf Storage= 4,120 cf Flood Elev= 101.50' Surf.Area= 3,082 sf Storage= 4,570 cf

Plug-Flow detention time= 152.2 min calculated for 0.179 af (86% of inflow) Center-of-Mass det. time= 91.8 min (875.1 - 783.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	98.60'	2,776 cf	38.17'W x 80.76'L x 2.83'H Field A
			8,733 cf Overall - 1,794 cf Embedded = 6,939 cf x 40.0% Voids
#2A	99.60'	1,794 cf	ADS_StormTech SC-310 x 121 Inside #1
			Effective Size= 28.9"W x 16.0"H => 2.07 sf x 7.12'L = 14.7 cf
			Overall Size= 34.0"W x 16.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 2.07 sf x 11 rows
		4.570 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	99.50'	12.0" Round Culvert L= 135.0' CPP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 99.50' / 97.60' S= 0.0141 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	99.50'	4.5" Vert. Orifice/Grate C= 0.600
#3	Device 1	101.00'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.86 cfs @ 12.38 hrs HW=101.07' TW=98.26' (Dynamic Tailwater)

2=Orifice/Grate (Orifice Controls 0.62 cfs @ 5.66 fps)

-3=Sharp-Crested Rectangular Weir (Weir Controls 0.23 cfs @ 0.86 fps)

Summary for Pond 3P: Underdrained Soil Filter

Inflow Area	=	0.543 ac, 6	61.52% Impe	ervious,	Inflow Depth >	3.48"	for 10-	YR event	
Inflow	=	2.24 cfs @	12.07 hrs,	Volume	= 0.158	af			
Outflow	=	0.66 cfs @	12.29 hrs,	Volume	= 0.151	af, Atte	en= 71%	, Lag= 13.0 i	min
Primary	=	0.66 cfs @	12.29 hrs,	Volume	= 0.151	af			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 100.66' @ 12.40 hrs Surf.Area= 3,472 sf Storage= 1,850 cf Flood Elev= 101.50' Surf.Area= 4,001 sf Storage= 3,340 cf

Plug-Flow detention time= 53.8 min calculated for 0.151 af (96% of inflow) Center-of-Mass det. time= 31.3 min (826.5 - 795.1)

Volume	Inve	ert Avail.S	Storage	Storage	Description						
#1	100.0	0' 2	2,378 cf	Pond S	torage (Prismat	tic)Listed below (Recalc)					
#2	98.5	0'	439 cf	Soil Filt	ter (Prismatic)L	isted below (Recalc)					
	<u> </u>			1,463 ct	f Overall x 30.0%	% Voids					
#3	97.1	5'	524 ct	Stone Resevoir (Prismatic)Listed below (Recalc)							
			040 -5	1,309 C	r Overall X 40.0%	% VOIDS					
		Ċ	3,340 CT	I OTAL AV	allable Storage						
Elevatio	n	Surf.Area	Inc.	Store	Cum.Store						
(fee	t)	(sq-ft)	(cubic	-feet)	(cubic-feet)						
100.0	0	1,150		0	0						
101.0	0	1,718		1,434	1,434						
101.5	0	2,056		944	2,378						
Flevatio	n	Surf Area	Inc	Store	Cum Store						
	t)	(sq-ft)	(cubic	s-feet)	(cubic-feet)						
98.5	0	975	(00.010	0	0						
100.0	Õ	975		1,463	1,463						
Elevatio	n	Surf.Area	Inc.	Store	Cum.Store						
(fee	t)	(sq-ft)	(cubic	c-feet)	(cubic-feet)						
97.1	5	970		0	0						
98.5	0	970		1,309	1,309						
Device	Routing	Inve	ert Outle	et Device	S						
#1	Primary	97.6	5' 12.0 '	' Round	d Culvert						
			L= 5.	0' CPP	, end-section co	nforming to fill, Ke= 0.500					
			Inlet	/ Outlet I	Invert= 97.65' / 9	7.60' S= 0.0100 '/' Cc= 0.900					
#0	Davias 1	077	n= 0.	013 Co	rrugated PE, sm	ooth interior, Flow Area= 0.79 sf					
#Z #2	Device 1	97.7	5 4.0 "	vert. Or		0.000					
#3	Device I	101.2	Limit	ed to we	ir flow at low hea	ads					
			/								

Primary OutFlow Max=0.66 cfs @ 12.29 hrs HW=100.64' TW=98.20' (Dynamic Tailwater) **1=Culvert** (Passes 0.66 cfs of 5.91 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.66 cfs @ 7.52 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond PDMH4:

 Inflow Area =
 1.201 ac, 69.22% Impervious, Inflow Depth > 3.30" for 10-YR event

 Inflow =
 1.51 cfs @ 12.38 hrs, Volume=
 0.331 af

 Outflow =
 1.51 cfs @ 12.38 hrs, Volume=
 0.331 af, Atten= 0%, Lag= 0.0 min

 Primary =
 1.51 cfs @ 12.38 hrs, Volume=
 0.331 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 98.26' @ 12.38 hrs Flood Elev= 102.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	97.50'	12.0" Round Culvert
	,		L= 10.0' CPP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= $97.50' / 97.40'$ S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE smooth interior. Flow Area= 0.79 sf
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79

Primary OutFlow Max=1.51 cfs @ 12.38 hrs HW=98.26' TW=0.00' (Dynamic Tailwater) -1=Culvert (Barrel Controls 1.51 cfs @ 3.24 fps)

Summary for Link PA1:

Inflow Are	a =	1.991 ac,	55.46% Imp	ervious, l	Inflow Depth >	3.1	1" for 10-	YR event
Inflow	=	3.73 cfs @) 12.09 hrs,	Volume=	0.515	af		
Primary	=	3.73 cfs @) 12.09 hrs,	Volume=	• 0.515	af,	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA2:

Inflow /	Area	=	0.080 ac, <i>1</i>	17.12% Imp	ervious,	Inflow Depth >	> 2.4	46" for 1	0-YR event
Inflow		=	0.24 cfs @	12.08 hrs,	Volume	= 0.01	6 af		
Primar	у	=	0.24 cfs @	12.08 hrs,	Volume	= 0.01	6 af,	Atten= 0%	6, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA3:

Inflow /	Area	=	0.108 ac,	13.06% Imp	ervious,	Inflow De	epth >	2.3	7" for	10- `	YR ev	ent
Inflow	=	=	0.31 cfs @	12.08 hrs,	Volume	=	0.021	af				
Primar	y =	=	0.31 cfs @	12.08 hrs,	Volume	=	0.021	af,	Atten= 0)%,	Lag=	0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

J0096-POST	-
Prepared by Tighe & Bond	
HydroCAD® 10.00 s/n 03436 © 2013 HydroCAD Software Solutions LI	LC

Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment WS-1A:	Flow Length=130'	Runoff Area=23,6 Slope=0.0200 '/'	662 sf 61.52 Tc=5.0 min	% Imperviou CN=89 Ru	s Runoff Dep noff=2.71 cfs	oth>4.25" 0.192 af
Subcatchment WS-1B:		Runoff Area=34,4 Flow Length=495'	411 sf 34.55 Tc=5.5 min	% Imperviou CN=82 Ru	s Runoff Dep Inoff=3.31 cfs	oth>3.53" 0.232 af
Subcatchment WS-1C:		Runoff Area=28,6 Flow Length=240'	650 sf 75.57 Tc=5.0 min	% Imperviou CN=92 Ru	s Runoff Dep noff=3.45 cfs	oth>4.58" 0.251 af
Subcatchment WS-2:	Flow Length=22'	Runoff Area=3,5 Slope=0.0150 '/'	505 sf 17.12 Tc=5.0 min	% Imperviou CN=78 Ru	s Runoff Dep noff=0.31 cfs	oth>3.14" 0.021 af
Subcatchment WS-3:	Flow Length=30'	Runoff Area=4,6 Slope=0.0200 '/'	685 sf 13.06 Tc=5.0 min	% Imperviou CN=77 Ru	s Runoff Dep noff=0.40 cfs	oth>3.04" 0.027 af
Pond 1P: Stormtech 310		Peak Elev=101	.19' Storage	=4,273 cf In Out	flow=3.45 cfs flow=1.75 cfs	0.251 af 0.221 af
Pond 3P: Underdrained So	oil Filter	Peak Elev=101	.00' Storage	=2,398 cf In Out	flow=2.71 cfs flow=0.69 cfs	0.192 af 0.186 af
Pond PDMH4:	12.0" Round	Culvert n=0.013	Peak Ele L=10.0' S=0.	ev=98.54' In 0100 '/' Out	flow=2.38 cfs flow=2.38 cfs	0.407 af 0.407 af
Link PA1:				In Prin	flow=4.50 cfs nary=4.50 cfs	0.640 af 0.640 af
Link PA2:				In Prin	flow=0.31 cfs nary=0.31 cfs	0.021 af 0.021 af
Link PA3:				In Prin	flow=0.40 cfs nary=0.40 cfs	0.027 af 0.027 af
Total Runo	ff Area = 2.179 a	c Runoff Volum	ne = 0.724 a	f Average	Runoff Dep	th = 3.99"

48.05% Pervious = 1.047 ac 51.95% Impervious = 1.132 ac

Summary for Subcatchment WS-1A:

Runoff = 2.71 cfs @ 12.07 hrs, Volume= 0.192 af, Depth> 4.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.50"

A	rea (sf)	CN E	Description		
	14,558	98 F	Paved park	ing, HSG C	
	9,104	74 >	75% Gras	s cover, Go	od, HSG C
	23,662	89 V	Veighted A	verage	
	9,104	3	88.48% Per	vious Area	
	14,558	6	61.52% Imp	ervious Are	ea
_					
TC	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cts)	
0.7	50	0.0200	1.16		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	80	0.0200	2.87		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
1.2	130	Total, I	ncreased t	o minimum	Tc = 5.0 min

Summary for Subcatchment WS-1B:

Runoff = 3.31 cfs @ 12.08 hrs, Volume= 0.232 af, Depth> 3.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.50"

_	Ai	rea (sf)	CN [Description			
		11,890	98 F	Paved park	ing, HSG C		
_		22,521	74 >	>75% Gras	s cover, Go	bod, HSG C	
		34,411	82 \	Neighted A	verage		
		22,521	6	65.45% Per	vious Area		
		11,890	3	34.55% Imp	pervious Are	ea	
	_						
	Tc	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	0.9	50	0.0125	0.96		Sheet Flow,	
						Smooth surfaces n= 0.011 P2= 3.00"	
	1.0	125	0.0110	2.13		Shallow Concentrated Flow,	
						Paved Kv= 20.3 fps	
	3.6	320	0.0100	1.50		Shallow Concentrated Flow,	
_						Grassed Waterway Kv= 15.0 fps	
	5.5	495	Total				

Summary for Subcatchment WS-1C:

Runoff = 3.45 cfs @ 12.07 hrs, Volume= 0.251 af, Depth> 4.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.50"

A	rea (sf)	CN D	Description							
	19,300	98 F	98 Roofs, HSG C							
	2,350	98 P	aved park	ing, HSG C	;					
	7,000	74 >	75% Gras	s cover, Go	ood, HSG C					
	28,650	92 V	Veighted A	verage						
	7,000	2	4.43% Per	vious Area						
	21,650	7	5.57% Imp	pervious Are	ea					
Тс	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
1.1	75	0.0150	1.12		Sheet Flow,					
					Smooth surfaces n= 0.011 P2= 3.00"					
0.9	165	0.0050	3.21	2.52	Pipe Channel,					
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'					
					n= 0.013 Corrugated PE, smooth interior					
2.0	240	Total, I	ncreased t	o minimum	Tc = 5.0 min					

Summary for Subcatchment WS-2:

Runoff = 0.31 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 3.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.50"

A	rea (sf)	CN	Description					
	2,905	74	>75% Gras	s cover, Go	ood, HSG C			
	600	98	Paved park	ing, HSG C	,			
	3,505	78	Weighted A	verage				
	2,905		82.88% Pei	vious Area				
	600		17.12% Imp	pervious Are	ea			
Тс	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)				
3.4	22	0.0150	0.11		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.00"	
3.4	22	Total,	Increased t	o minimum	Tc = 5.0 min			

Summary for Subcatchment WS-3:

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 3.04"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.50"

J0096-POST

Prepared by Tig	he & Bono	d
HydroCAD® 10.00	s/n 03436	© 2013 HydroCAD Software Solutions LLC

A	rea (sf)	CN	Description						
	612	98	Paved park	ing, HSG C	;				
	4,073	74	>75% Gras	s cover, Go	ood, HSG C				
	4,685	77	77 Weighted Average						
	4,073		86.94% Per	vious Area					
	612		13.06% Imp	pervious Are	ea				
Тс	Length	Slone	Velocity	Canacity	Description				
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)	Description				
	30	0 0200	0.13	(0.0)	Sheet Flow				
0.0	00	0.0200	0.10		Grass: Short	n= 0.150	P2= 3.00"		
3.9	30	Total,	Increased t	o minimum	Tc = 5.0 min				

Summary for Pond 1P: Stormtech 310

Inflow Area	=	0.658 ac,	75.57% Imperv	vious, Inflow D	Depth > 4.58	8" for 25-Y	R event
Inflow	=	3.45 cfs @	12.07 hrs, Vo	olume=	0.251 af		
Outflow	=	1.75 cfs @	12.20 hrs, Vo	olume=	0.221 af, <i>i</i>	Atten= 49%,	Lag= 7.5 min
Primary	=	1.75 cfs @	12.20 hrs, Vo	olume=	0.221 af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 101.19' @ 12.20 hrs Surf.Area= 3,082 sf Storage= 4,273 cf Flood Elev= 101.50' Surf.Area= 3,082 sf Storage= 4,570 cf

Plug-Flow detention time= 137.9 min calculated for 0.221 af (88% of inflow) Center-of-Mass det. time= 83.9 min (862.3 - 778.4)

Volume	Invert	Avail.Storage	Storage Description
#1A	98.60'	2,776 cf	38.17'W x 80.76'L x 2.83'H Field A
			8,733 cf Overall - 1,794 cf Embedded = 6,939 cf x 40.0% Voids
#2A	99.60'	1,794 cf	ADS_StormTech SC-310 x 121 Inside #1
			Effective Size= 28.9"W x 16.0"H => 2.07 sf x 7.12'L = 14.7 cf
			Overall Size= 34.0"W x 16.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 2.07 sf x 11 rows
		4.570 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	99.50'	12.0" Round Culvert L= 135.0' CPP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 99.50' / 97.60' S= 0.0141 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	99.50'	4.5" Vert. Orifice/Grate C= 0.600
#3	Device 1	101.00'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=1.74 cfs @ 12.20 hrs HW=101.19' TW=98.54' (Dynamic Tailwater)

2=Orifice/Grate (Orifice Controls 0.65 cfs @ 5.91 fps)

-3=Sharp-Crested Rectangular Weir (Weir Controls 1.09 cfs @ 1.43 fps)

Summary for Pond 3P: Underdrained Soil Filter

Inflow Area	ı =	0.543 ac,	61.52% Imp	ervious,	Inflow Depth >	4.25"	for 25-	YR event	
Inflow	=	2.71 cfs @	12.07 hrs,	Volume	= 0.192	af			
Outflow	=	0.69 cfs @	12.57 hrs,	Volume	= 0.186	af, At	ten= 74%	, Lag= 29.9	min
Primary	=	0.69 cfs @	12.57 hrs,	Volume	= 0.186	af		-	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 101.00' @ 12.43 hrs Surf.Area= 3,664 sf Storage= 2,398 cf Flood Elev= 101.50' Surf.Area= 4,001 sf Storage= 3,340 cf

Plug-Flow detention time= 53.2 min calculated for 0.186 af (97% of inflow) Center-of-Mass det. time= 34.1 min (823.8 - 789.7)

Volume	Inve	rt Avail.Sto	orage Sto	orage Description	
#1	100.00	D' 2,3	78 cf Po	ond Storage (Prismatic)Listed below (Recalc)	_
#2	98.50	C' 4	39 cf So	bil Filter (Prismatic)Listed below (Recalc)	
			1,4	463 cf Overall x 30.0% Voids	
#3	97.18	5' 5	24 cf Sto	one Resevoir (Prismatic)Listed below (Recalc)	
			1,3	309 cf Overall x 40.0% Voids	—
		3,3	40 ct I of	otal Available Storage	
Elevatior	n 5	Surf.Area	Inc.Sto	ore Cum.Store	
(feet))	(sq-ft)	(cubic-fee	et) (cubic-feet)	
100.00)	1,150		0 0	
101.00)	1,718	1,43	1,434	
101.50)	2,056	94	944 2,378	
Flevation	, (Surf Area	Inc Sto	ore Cum Store	
(feet)		(sq-ft)	(cubic-fee	et) (cubic-feet)	
98.50)	975	(00010100		
100.00	,)	975	1.46	1.463	
			.,		
Elevatior	n 5	Surf.Area	Inc.Sto	ore Cum.Store	
(feet))	(sq-ft)	(cubic-fee	et) (cubic-feet)	
97.15	5	970		0 0	
98.50)	970	1,30	309 1,309	
Device	Routing	Invert	Outlet De	Devices	
#1	Primary	97.65'	12.0" R	Round Culvert	_
			L= 5.0'	CPP, end-section conforming to fill, Ke= 0.500	
			Inlet / Ou	outlet Invert= 97.65' / 97.60' S= 0.0100 '/' Cc= 0.900	
	.	07.75	n= 0.013	3 Corrugated PE, smooth interior, Flow Area= 0.79 sf	
#2	Device 1	97.75	4.0" Ver	rt. Orifice/Grate $C=0.600$	
#3	Device 1	101.20	16.0" X 1 Limited t	16.0 " Horiz. Orifice/Grate C= 0.600 to weir flow at low beads	

Primary OutFlow Max=0.70 cfs @ 12.57 hrs HW=100.95' TW=98.22' (Dynamic Tailwater) **1=Culvert** (Passes 0.70 cfs of 6.26 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.70 cfs @ 7.96 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond PDMH4:

 Inflow Area =
 1.201 ac, 69.22% Impervious, Inflow Depth > 4.07" for 25-YR event

 Inflow =
 2.38 cfs @ 12.20 hrs, Volume=
 0.407 af

 Outflow =
 2.38 cfs @ 12.20 hrs, Volume=
 0.407 af, Atten= 0%, Lag= 0.0 min

 Primary =
 2.38 cfs @ 12.20 hrs, Volume=
 0.407 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 98.54' @ 12.20 hrs Flood Elev= 102.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	97.50'	12.0" Round Culvert
	,		L= 10.0' CPP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 97.50' / 97.40' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.38 cfs @ 12.20 hrs HW=98.54' TW=0.00' (Dynamic Tailwater) -1=Culvert (Barrel Controls 2.38 cfs @ 3.64 fps)

Summary for Link PA1:

Inflow Ar	ea =	1.991 ac,	55.46% Impe	ervious, I	nflow Depth >	3.8	6" for 25-	YR event	
Inflow	=	4.50 cfs @	12.08 hrs,	Volume=	0.640	af			
Primary	=	4.50 cfs @	2 12.08 hrs,	Volume=	0.640	af,	Atten= 0%,	Lag= 0.0 m	nin

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA2:

Inflow /	Area	=	0.080 ac, 1	17.12% Impe	ervious,	Inflow Depth >	3.1	14" for 25-	YR event
Inflow		=	0.31 cfs @	12.07 hrs,	Volume	= 0.021	af		
Primar	у	=	0.31 cfs @	12.07 hrs,	Volume	= 0.021	af,	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Link PA3:

Inflow A	Area =	0.108 ac, 1	3.06% Impervi	ious, Inflow	Depth > 3.0	4" for 25-	YR event
Inflow	=	0.40 cfs @	12.07 hrs, Vc	olume=	0.027 af		
Primary	y =	0.40 cfs @	12.07 hrs, Vo	olume=	0.027 af,	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Stormtech 310

Inflow Area	ı =	0.658 ac,	75.57% Impe	ervious,	Inflow Depth 3	> 5.75"	for 100-	YR event
Inflow	=	4.28 cfs @	12.07 hrs,	Volume	= 0.31	l5 af		
Outflow	=	3.42 cfs @	12.13 hrs,	Volume	= 0.28	35 af, At	ten= 20%,	Lag= 3.4 min
Primary	=	3.42 cfs @	12.13 hrs,	Volume	= 0.28	35 af		-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 101.36' @ 12.13 hrs Surf.Area= 3,082 sf Storage= 4,474 cf Flood Elev= 101.50' Surf.Area= 3,082 sf Storage= 4,570 cf

Plug-Flow detention time= 122.6 min calculated for 0.285 af (90% of inflow) Center-of-Mass det. time= 75.6 min (848.1 - 772.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	98.60'	2,776 cf	38.17'W x 80.76'L x 2.83'H Field A
			8,733 cf Overall - 1,794 cf Embedded = 6,939 cf x 40.0% Voids
#2A	99.60'	1,794 cf	ADS_StormTech SC-310 x 121 Inside #1
			Effective Size= 28.9"W x 16.0"H => 2.07 sf x 7.12'L = 14.7 cf
			Overall Size= 34.0"W x 16.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 2.07 sf x 11 rows
		4 570 cf	Total Available Storage

4,570 Ci Tolai Avaliable Slorage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	99.50'	12.0" Round Culvert
	2		L= 135.0' CPP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 99.50' / 97.60' S= 0.0141 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	99.50'	4.5" Vert. Orifice/Grate C= 0.600
#3	Device 1	101.00'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=3.41 cfs @ 12.13 hrs HW=101.36' TW=99.13' (Dynamic Tailwater)

-1=Culvert (Passes 3.41 cfs of 3.93 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.69 cfs @ 6.22 fps)

-3=Sharp-Crested Rectangular Weir (Weir Controls 2.72 cfs @ 1.95 fps)

Summary for Pond 3P: Underdrained Soil Filter

Inflow Area	a =	0.543 ac, 6	61.52% Impe	ervious,	Inflow Depth >	5.41"	for 10	0-YR event	
Inflow	=	3.41 cfs @	12.07 hrs,	Volume	= 0.245	af			
Outflow	=	1.26 cfs @	12.31 hrs,	Volume	= 0.239	af, Atte	en= 63%	, Lag= 14.2	2 min
Primary	=	1.26 cfs @	12.31 hrs,	Volume	= 0.239	af		-	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 101.31' @ 12.30 hrs Surf.Area= 3,869 sf Storage= 2,952 cf Flood Elev= 101.50' Surf.Area= 4,001 sf Storage= 3,340 cf

Plug-Flow detention time= 50.7 min calculated for 0.238 af (97% of inflow) Center-of-Mass det. time= 35.0 min (818.2 - 783.2)

Volume	Inve	ert Avail.	Storage	Storage	Description	
#1	100.0	0'	2,378 cf	Pond S	torage (Prismat	tic)Listed below (Recalc)
#2	98.5	0'	439 cf	Soil Filt	ter (Prismatic)	isted below (Recalc)
#2	07 1	5'	524 of	1,463 Cl	Overall X 30.0%	% Volds atic) listed below (Beegle)
#5	57.1	5	JZ4 CI	1.309 cl	Overall x 40.09	% Voids
			3,340 cf	Total Av	/ailable Storage	
	_		La a	01	0	
Elevatio	n +)	Surf.Area	INC.	Store	Cum.Store	
(100	<u>()</u>	<u>(Sq-II)</u>	(Cubic			
100.0	0	1,150		0	0	
101.0		1,718		044	1,434	
101.5	Ū	2,050		944	2,370	
Elevatio	n	Surf.Area	Inc.	Store	Cum.Store	
(fee	t)	(sq-ft)	(cubic	-feet)	(cubic-feet)	
98.5	0	975		0	0	
100.0	0	975		1,463	1,463	
Elevatio	n	Surf.Area	Inc.	Store	Cum.Store	
(fee	t)	(sq-ft)	(cubic	-feet)	(cubic-feet)	
97.1	5	970		0	0	
98.5	0	970		1,309	1,309	
Device	Routing	Inv	ert Outle	et Device	S	
#1	Primary	97.6	65' 12.0 '	' Round	l Culvert	
			L= 5.	0' CPP	, end-section co	nforming to fill, Ke= 0.500
			Inlet	/ Outlet I	nvert= 97.65' / 9	7.60' S= 0.0100 '/' Cc= 0.900
			n= 0.	013 Co	rrugated PE, sm	ooth interior, Flow Area= 0.79 sf
#2	Device 1	97.	/5' 4.0 "	vert. Or	itice/Grate C=	0.600
#3	Device 1	101.2	20' 16.0' Limit	' x 16.0 " ed to we	ir flow at low hea	Grate C= 0.600 ads

Primary OutFlow Max=1.26 cfs @ 12.31 hrs HW=101.30' TW=98.76' (Dynamic Tailwater) **1=Culvert** (Passes 1.26 cfs of 6.04 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.67 cfs @ 7.69 fps)

-3=Orifice/Grate (Weir Controls 0.59 cfs @ 1.06 fps)



2.6 Mitigation Description and Best Management Practices

In order to mitigate the increase in impervious area required for the proposed project, a stormwater system has been designed for this project utilizing low impact development measures.

The intent of the stormwater management system design is for runoff to be collected, detained, and treated, where possible. An Underdrained Soil Filter has been provided to mitigate potential impacts from the increase in impervious area. The Underdrained Soil Filter has been designed to treat the entire runoff volume from the 2 and 10-year 24 hour storms. As shown in Section 2.5, the treatment volume provided is greater than the volume required by the stormwater regulations.

The underground detention basin, which consists of Stormtech SC-310 chambers, has been designed to detain and mitigate peak flows generated by the roof and grass play area. Runoff generated from the roof will not be treated as it is inherently clean. Deep sump catch basins with Casco traps will provide pre-treatment for stormwater that is collected within the play area adjacent to the building prior to discharge into the detention basin.

All soil erosion and sediment control measures shall be in accordance with regulations and principles as outlined in the Stormwater Management for Maine: Best Management Practices and Maine Erosion and Sediment Control Handbook for Construction. The intent of the outlined measures is to minimize erosion and sedimentation during construction, stabilize and protect the site from erosion after construction is complete and improve stormwater quality from the site. Best Management Practices for this project include:

- Temporary practices to be implemented during construction.
- Permanent practices to be implemented after construction.
- Stormwater treatment devices.

TEMPORARY PRACTICES

Sequencing:

- 1. Construct temporary and permanent sediment, erosion and detention control facilities. Erosion, sediment and detention measures shall be installed prior to any earth moving operations that will influence stormwater runoff such as:
 - New construction
 - Development of borrow pit areas
 - Disposal of sediment spoil, stump and other solid waste
 - Control of dust
- 2. All permanent ditches, swales, detention, retention and sedimentation basins to be stabilized using the vegetative and nonstructural BMPs prior to directing runoff to them.
- 3. Clear and dispose of debris.

- 4. Construct temporary culverts and diversion channels as required.
- 5. Begin permanent and temporary seeding and mulching. All cut and fill slopes shall be seeded and mulched immediately after their construction.
- 6. Daily, or as required, construct temporary berms, drains, ditches, silt fences, sediment traps etc., mulch and seed as required.
- 7. Finish pave all roadways and parking lots.
- 8. Inspect and maintain all erosion and sediment control measures.
- 9. Complete permanent seeding and landscaping.
- 10. Remove trapped sediment from collection devices as appropriate and then remove temporary erosion control measures.

Stabilization Practices:

- 1. Install stabilized construction entrance at the location shown on plans.
- 2. Loam stockpiles shall be mulched, seeded and contained by a silt fence barrier.
- 3. All erosion control devices, including silt fences and storm drain inlet filters, shall be inspected at least once per week and following any rainfall of 1/4 inch or greater. All necessary maintenance shall be completed within 48 hours. A Maintenance Inspection Report shall be kept on site and made available by the contractor at the city's request.
- 4. Inactivity: Area of the site which has been disturbed, where construction activity will not occur for more than twenty-one (21) days, shall be temporarily stabilized by mulching and seeding.
- 5. Waste Disposal/Spill Prevention: The Erosion Control Notes and Details Sheet of the Site Plans fully detail the waste disposal and spill prevention procedures. All waste from construction activities shall be collected and stored in receptacles. No construction materials shall be buried on site. The Spill Prevention Plan focuses on personnel training, housekeeping, storage and standard practices for use and disposal of materials.

PERMANENT PRACTICES

The objectives for developing permanent Best Management Practices for this site include the following:

- Develop a plan that provides the best hydrologic condition both on site and downstream.
- Provide a higher level of removal of pollutants from stormwater runoff.
- Minimize impact on the natural environment.
- Minimize future maintenance.

Section 3 Long Term Operation & Maintenance Plan

It is the intent of this Operation and Maintenance Plan to identify the areas of this site that need special attention and consideration, as well as implementing a plan to assure routine maintenance. By identifying the areas of concern as well as implementing a frequent and routine maintenance schedule the site will maintain a high quality of stormwater runoff.

Annual Reporting Requirements

The owner or operator of a BMP or a qualified post-construction stormwater inspector hired by that person, shall, on or by June 30 of each year, provide a completed and signed certification to City of Portland Department of Public Services (DPS) in a form provided by DPS, certifying that the person has inspected the BMP(s) and that they are adequately maintained and functioning as intended by the approved post-construction stormwater management plan, or that they require maintenance or repair, including the record of the deficiency and corrective action(s) taken.

3.1 Contact/Responsible Party

Steve Brinn Jewish Community Alliance of Southern Maine 57 Ashmont Street Portland, Maine

(Note: The contact information for the Contact/Responsible Party shall be kept current. If ownership changes, the Operation and Maintenance Plan must be transferred to the new party.)

3.2 Maintenance Items

Maintenance of the following items shall be recorded:

- Litter/Debris Removal
- Landscaping
- Catch basin/Yard drain Cleaning
- Pavement Sweeping
- Stormtech Chamber Cleaning
- Underdrained Soil Filter Cleaning and Maintenance

The following maintenance items and schedule represent the minimum action required. Periodic site inspections shall be conducted and all measures must be maintained in effective operating condition. The following items shall be observed during site inspection and maintenance:

- Inspect vegetated areas, particularly slopes and embankments for areas of erosion. Replant and restore as necessary
- Inspect catch basins for sediment buildup
- Inspect site for trash and debris

F

3.3 Overall Site Operation & Maintenance Schedule

Overall Site Operation and Maintenance Schedule							
Maintenance Item	Frequency of Maintenance	Operation					
Litter/Debris Removal	Weekly	Management Company					
Pavement Sweeping - Sweep impervious areas to remove sand and litter.	2 - 4 times annually	Parking Lot Sweeper					
Underdrain Soil Filter - Trash and debris to be removed. - Any required maintenance shall be addressed.	Two (2) times annually and after any rainfall event exceeding 2.5" in a 24-hr period	Management Company					
Stormtech Chambers - Visual inspection and cleaning.	Twice Yearly	Management Company / Vacuum Truck					
Rip Rap Aprons Trash and debris to be removed. Any required maintenance shall be addressed. 	Annually	Management Company					
Catch Basin (CB) / Yard Drain (YD) Cleaning - CBs/YDs to be cleaned of solids and oils.	Annually	Vacuum Truck					
Landscaping - Landscaped islands to be maintained and mulched.	Maintained as required and mulched each Spring	Management Company					

Underdrained Soil Filter	Underdrained Soil Filter Inspection/Maintenance Requirements					
Inspection/ Maintenance	Frequency	Action				

Monitor to ensure that Rain Gardens function effectively after storms	Four (4) times annually (quarterly) and after any rainfall event exceeding 2.5" in a 24-hr period	 Trash and debris to be removed Any required maintenance shall be addressed
Inspect Vegetation	Annually	 Inspect the condition of all Rain Garden vegetation Prune back overgrowth Replace dead vegetation Remove any invasive species
Inspect Drawdown Time - The system shall drawdown within 48- hours following a rainfall event.	Annually	- Assess the condition of the facility to determine measures required to restore the filtration function, including but not limited to removal of accumulated sediments or reconstruction of the filter.

StormTech Inspection/Maintenance Requirements										
Inspection/	Frequency	Action								
Maintenance										
Inspection with maintenance following as warranted	Twice Yearly	 Trash and debris to be removed Any required maintenance shall be addressed. 								

Rip Rap Inspection/Maintenance Requirements										
Inspection/ Frequency Action Maintenance										
Visual Inspection	Annually	 Visually inspect for damage and deterioration Repair damages immediately 								

3.3.1 Disposal Requirements

Disposal of debris, trash, sediment and other waste material should be done at suitable disposal/recycling sites and in compliance with all applicable local, state and federal waste regulations.

3.3.2 Snow & Ice Management for Standard Asphalt and Walkways

Snow storage areas shall be located such that no direct untreated discharges are possible to receiving waters from the storage site (snow storage areas have been shown

on the Site Plan). Curb cuts shown on the plan shall remain free of snow and ice buildup. Salt storage areas shall be covered or located such that no direct untreated discharges are possible to receiving waters from the storage site.

3.3.3 Annual Updates and Log Requirements

The Owner and/or Contact/Responsible Party shall review this Operation and Maintenance Plan once per year for its effectiveness and adjust the plan and deed as necessary.

A log of all preventative and corrective measures for the stormwater system shall be kept on-site and be made available upon request by any public entity with administrative, health environmental or safety authority over the site.

Project Name		Proposed I	roposed Neighborhood Center, 1342 Congress St, Portland, ME							
BMP Description	Date of Inspection	Inspector	BMP Installed and Operating Properly?	Cleaning / Corrective Action Needed	Date of Cleaning / Repair	Performed By				
			□Yes □No							
			□Yes □No							
			□Yes □No							
			□Yes □No							
			□Yes □No							
			□Yes □No							
			□Yes □No							
			□Yes □No							
			□Yes □No							
			□Yes □No							
			□Yes □No							
			□Yes □No							

J: \J\J0096 Jewish Community Alliance\DRAINAGE\DRAINAGE STUDIES\Revised 6-23-15\J0096-Drainage Study-(Revised 6-23-15).doc

Table 2-124 Hour Duration Rainfalls for Various Return PeriodsNatural Resources Conservation Service County Rainfall Data

			Return Interval or Frequency							
County	Storm Type	1-Yr	2-Yr	5-Yr	10- Yr	25- Yr	100- Yr	500 -Yr	Annual	
Androscoggin		2.5	3.0	3.9	4.6	5.4	6.5	7.8	45.3	
Aroostook C		2.1	2.1	3.2	3.6	4.2	5.0	5.9	36.1	(Presque Isle Area)
Aroostook N	S	2.0	2.3	3.0	3.5	4.0	4.8	5.7	36.1	(Fort Kent Area)
Aroostook S	Ε	2.2	2.5	3.3	3.8	4.4	5.3	6.4	39.0	(Houlton Area)
Cumberland NW	Ε	2.8	3.3	4.3	5.0	5.8	6.9	8.3	43.4	(NW of St. Route 11)
Cumberland SE		2.5	3.0	4.0	4.7	5.5	6.7	8.1	44.4	(SE of St. Route 11)
Franklin	Ν	2.4	2.9	3.7	4.2	4.9	5.9	7.0	45.6	
Hancock	0	2.4	2.7	3.6	4.2	4.9	6.0	7.2	45.2	
Kennebec	Т	2.4	3.0	3.8	4.4	5.1	6.1	7.2	41.7	
Knox-Lincoln	Ε	2.5	2.9	3.8	4.4	5.1	6.2	7.4	46.1	
Oxford E	S	2.5	3.0	4.0	4.6	5.3	6.4	7.6	43.0	(E of St. Route 26)
Oxford W		3.0	3.5	4.5	5.2	6.0	7.1	8.4	43.8	(W of St. Route 26)
Penobscot N	1	2.2	2.5	3.3	3.8	4.4	5.4	6.4	41.5	(N of CanAtl. Rwy)
Penobscot S	1	2.4	2.7	3.5	4.1	4.8	5.8	6.9	39.5	(S of CanAtl. Rwy)
Piscataquis N		2.2	2.5	3.3	3.8	4.4	5.3	6.3	38.5	(N of Can Atl. Rwy)
Piscataquis S	A N	2.3	2.6	3.4	4.0	4.6	5.5	6.6	41.0	(S of Can Atl. Rwy)
Sagadahoc	D	2.5	3.0	3.9	4.6	5.4	6.5	7.8	45.3	
Somerset N		2.2	2.5	3.3	3.8	4.4	5.3	6.3	37.3	(N of Can Atl. Rwy)
Somerset S	•	2.4	2.7	3.5	4.1	4.7	5.7	6.8	39.5	(S of Can Atl. Rwy)
Waldo	2	2.5	2.8	3.7	4.3	4.9	6.0	7.1	47.2	
Washington		2.4	2.5	3.4	4.0	4.8	5.9	7.1	44.2	
York		2.5	3.0	4.0	4.6	5.4	6.6	7.8	46.7	

NOTES: REVISED 4/10/92 Lew P. Crosby 24-HR DURATION RAINFALL

SOURCES: 24-HR. DATA - TP 40 ANNUAL DATA - CDAN

- **Note 1:** ¹Use *Type II* for Oxford County (with the exception of towns listed below) and Penobscot County (with the exception of towns listed below) and all Main counties not listed below)
- **Note 2:** ²Use *Type III* for York, Cumberland, Androscoggin, Sagadahoc, Kennebec, Waldo, Knox, Piscataquis, Somerset, Franklin, Aroostook, Lincoln, Hancock, Washington Counties; the following Oxford County Towns: Porter, Brownfield, Hiram, Denmark, Oxford, Hebron, Buckfield and Hartford; and the following Penobscot County Towns: Dixmont, Newburgh, Hampden, Bangor, Veazie, Orono, Bradley, Clifton, Eddington, Holden, Brewer, Orrington, Plymouth, Etna, Carmel, Hermon, Glenburn, Old Town, Milford and Greenfield.

March 18, 2013

St.Germain - Collins

Karen Johnson Charter Realty & Development Corporation 800 Westchester Avenue, Suite S-632 Rye Brook, NY 10573

Re: Phase II Environmental Site Assessment St. Patrick's Church 1342 and 1348 Congress Street Portland, Maine St.Germain Collins File No.: 3410.2

Dear Ms. Johnson:

St.Germain Collins is providing you with the results of a Phase II Environmental Site Assessment (ESA) conducted at St. Patrick's Church in Portland, Maine (Site) (see **Figure 1 - Site Location**). This work was in response to our identification of a 3,000-gallon #2 fuel oil underground storage tank (UST) formerly present on the Site. During completion of a Phase I ESA, St.Germain Collins determined that contaminated soil was observed during removal of this UST in 1991, and it therefore was considered a Recognized Environmental Condition (REC). The purpose of the Phase II ESA was to determine if the REC represented a threat to human health or the environment, and in turn could limit Site redevelopment.

Background and Site Description

The Site is located at 1342 and 1348 Congress Street in Portland, Maine in a mixed residential and light commercial neighborhood (see Figure 1). It encompasses approximately 2.2 acres and is occupied by a church and rectory, surrounded by paved driveways, parking, and vegetated areas (see **Figure 2 – Site Plan**).

The church was built on the Site in 1964, and prior to its construction the Site was occupied by a farm and a small residence. The topography of the Site and surrounding area slopes gently to the south and west toward the Fore River. The Site and surrounding area are served by public water and sewer.

According to Maine Geological Survey maps, the Site is underlain by the Presumpscot Formation consisting of silt, clay and minor deposits of sand to unknown depth.

EXPERIENCE YOU CAN RELY ON

WHEN IT COUNTS

Phase II ESA Tasks

On March 4, 2013, St.Germain Collins supervised the advancement of four geoprobe soil borings in the area of the former UST located in a grassed area north of the Rectory (see Figure 2). All borings were continuously sampled and field screened with the Oil in Soil[®] shake test for petroleum hydrocarbons and a photoionization detector (PID) following Maine Department of Environmental Protection (MEDEP) Standard Operating Procedure TS-004 (Compendium of Field Testing of Soil Samples for Gasoline and Fuel Oil). One soil sample was collected for analysis of extractable petroleum hydrocarbons (EPH) by Analytics Environmental Laboratory (Analytics) in Portsmouth, New Hampshire. **Soil Boring Logs** are provided as **Attachment A** and the **Laboratory Report** is included as **Attachment B**.

Results

As shown on the boring logs in Attachment A, site geology consists of interbedded sand, silt, and clay. Boring SB-1 encountered refusal at a depth of 9.5 feet; the other borings did not reach refusal with the deepest boring SB-2 terminated at 24 feet. Groundwater was not encountered in any of the borings, though the low permeability clay may have limited groundwater flow into the borings.

No headspace readings exceeding the MEDEP notification limit of 40 parts per million (ppm) were recorded in the any of the borings; the highest PID reading was 6 ppm at 8 to 9 feet below grade in SB-1. One soil sample was collected from this interval for laboratory analysis of EPH. None of the samples showed the presence of free product based on the field tests.

The analyzed soil sample had detectable levels of three EPH constituents (C9-C18 Aliphatics, C19-C36 Aliphatics, and C11-C22 Aromatics. The detection of the aliphatic and aromatic hydrocarbons confirms that a petroleum release occurred. None of the detected constituents exceeded the 2009 MEDEP Petroleum Remediation Guidelines (PRGs), including the Residential PRG.

Dibenzo(a,h)anthracene was reported as non-detect, but had a practical quantization limit (PQL) above the Residential and Park User PRGs. This means that it is possible this compound is present about these two PRGs; the PQL is below the Construction/Excavation Worker and Outdoor Commercial Worker PRGs. With this soil being 8 to 9 feet below grade, it does not pose a risk under the Residential or Parker User PRGs unless brought to the surface.

Although the impacted soil at SB-1 does not currently pose a risk, if this soil is brought to the surface it must be managed appropriately. The MEDEP typically allows such soil to be reused on-site, especially if the soil remains below the ground surface. Otherwise, the soil would need to be disposed of or recycled at a MEDEP-approved facility.

Closure

Based upon the March 2013 subsurface investigation and sample results, St.Germain Collins does not recommend any additional actions be taken at this time. If you have any questions, please do not hesitate to contact us at (207) 591-7000.

ST.GERMAIN COLLINS

Brian Bachmann, C.G. Geologist

Attachments

Figure 1 - Site Location Figure 2 – Site Plan

Attachment ASoil Boring LogsAttachment BLaboratory Report

OF MAIN ATE BRIAN D. BACHMANN 528 GEOLOGIE





ATTACHMENT A

Soil Boring Logs

BORING AND MONITORING WELL LOG									NG #:		SB-1
					Project Number: 3410.2	Client/Location:	Charter I	Realty,	St. Pa	atric	ks Church
St.Germain Collins				ins	Date of Installation: 3/4/13	Representative:	Brian Bachmann				
					Total Depth of Boring:9.5 feetDrilling Company:			EPI			
					Depth to Water: NA	Drilling Technology:	Direct pu	ısh			
	8	346 Main	Street		Depth of Well: NA	Sampler:	Dual Tub	be			
	West	brook, M	laine 040	092	Well Screen Interval: NA	Well Screen Type:	NA				
	www.s	stgermaii	ncollins.	com	Well Riser Interval: NA	Well Riser Type:	NA				
Depth (ft)	Sample number	Sample Interval	Blows	Rec/Driven (in.)	Description		Stratum	Headspace Results (ppm)	Saturation Test Result	Depth (ft)	Well Construction
0	S-1	0-2	NA	31/48	organic SILT with sand, 2.5Y 3/3 dar	k olive brown,				0	
					loose, slightly plastic, moist		SILT	0.4			
1										1	
2	S-2	2-4			CLAY with gravel, 2.5Y 4/2 dark gray	vish brown, medium				2	
2					stiff, plastic, dry			1.7	Neg	2	
3										3	
Δ	S-3	4-6	NΔ	24/48	same as above		CLAY			4	No well
-	00	+0	1 1/ 1	24/40	Same as above					-	installed
5								1.9		5	at this
-										-	location.
6	S-4	6-8			clayey SAND, 5Y 5/1 gray, very soft,	very plastic, moist				6	
								12	Nog		
7								4.2	ney	7	
							SAND				
8	S-5	8-10	NA	40/48	same as above (8.0 to 9.5 interval su	bmitted for laboratory	UAND			8	
					analysis of Extractable Petroleum Hy	drocarbons)	6.0 Neg 9				
9					Defined at 0.5 feat halow and 1.4						
					Refusal at 9.5 feet below ground surf	ace.				12	

NA = not applicable. NS = not sampled.

ppm = parts per million.

Soil headspace screening completed with a MiniRae 3000 Photoionization Detector (PID). Neg = negative result using Oil in Soil shaker test kit as prescribed by MEDEP SOP TS 004

BORING AND MONITORING WELL LOG									BORIN	IG #:		SB-2
					Project Number: 3410.2 Client/Location: Charter Realty, St. Patric						ks Church	
	St.G	ermair	n Coll	ins	Date of Installation:	3/4/13	Representative:	Brian Ba	ichman	n		
	_			_	Total Depth of Boring:	24.0	Drilling Company:	EPI				
					Depth to Water:	Drilling Technology:	Direct pu					
	8	346 Main	Street		Depth of Well:	NA	Sampler:	Dual Tul	be			
	West	brook, M	laine 04	092	Well Screen Interval:	NA	Well Screen Type:	NA				
_	www.s	stgermaii	ncollins.	com	Well Riser Interval:	NA	Well Riser Type:	NA				
Depth (ft)	Sample number	Sample Interval	Blows	Rec/Driven (in.)	ם	escription		Stratum	Headspace Results (ppm)	Saturation Test Result	Depth (ft)	Well Construction
0	S-1	0-2	NA	48/48	organic SILT, 2.5Y 3/3 da	ark olive bro	wn, medium dense,				0	
					slightly plastic, dry				4.8			
1											1	
2	6.0	2.4			aama aa ahaya			SILT			2	
2	3-2	2-4			same as above						2	
3				1	ł				4.8	Neg	3	
Ĕ					ł						- J	
4	S-3	4-6	NA	48/48	clayey SAND, 2.5Y 5/3 lie	aht olive bro	wn, stiff, plastic, dry				4	
-						5			39			
5									3.0		5	
								SAND				
6	S-4	6-8			same as above			0, 110			6	
									3.2	Neg	_	
1										Ŭ	1	
0	<u>с</u> б	<u>8</u> 10	ΝΔ	18/18	CLAV 2 EV 4/2 dark grov	ich brown o	tiff yon plaatia day				Q	
0	3-0	0-10	INA	40/40	CLAT, 2.51 4/2 dalk gray	ISTI DIOWII, S	sun, very plastic, dry				0	
9					-				1.8		9	
											•	
10	S-6	10-12			same as above						10	
									23			
11									2.0		11	No well
10	<u> </u>	10.11									10	installed
12	S-7	12-14	NA	48/48	CLAY, 2.5Y 4/2 dark gray	ish brown, s	soft, very plastic, dry				12	at this
12											12	location.
13											15	
14	S-8	14-16			CLAY 2.5Y 5/0 grav ver	v soft verv	plastic moist	CLAY			14	
			1	1	, <u></u>	,, , y						
15]						15	
					ļ							
16	S-9	16-18	NA	48/48	same as above						16	
17					ł						17	
					ł						17	
18	S-10	18-20			same as above				NA	NA	18	
			1	1							-	
19					1						19	
								L				
20	S-11	20-22	NA	48/48	clayey SAND, 2.5Y 3/0 v	ery dark gra	y, very soft, very				20	
64					plastic, moist						0.1	
21					ł						21	
22	S-12	22-24		+	+			SAND			22	
	0-12	<u></u> -27		1	ł						~~	
23				1	t						23	
				İ.	1							
24					Terminated boring at 24.0	0 feet below	ground surface				24	

NA = not applicable.

NS = not sampled.

ppm = parts per million. Soil headspace screening completed with a MiniRae 3000 Photoionization Detector (PID). Neg = negative result using Oil in Soil shaker test kit as prescribed by MEDEP Standard Operating Procedure TS 004.

	BORING AND MONITORING WELL LOG								NG #:		SB-3
					Project Number: 3410.2	Client/Location:	Charter I	Realty,	St. Pa	atric	ks Church
St.Germain Collins				ins	Date of Installation: 3/4/13	Representative:	Brian Ba	ichman	n		
				_	Total Depth of Boring: 12.0 Drilling Company:			EPI			
					Depth to Water: NA	Drilling Technology:	Direct pu	ısh			
	8	846 Main	Street		Depth of Well: NA	Sampler:	Dual Tub	ре			
	West	brook, M	laine 040	092	Well Screen Interval: NA	Well Screen Type:	NA				
	www.s	stgermaii	ncollins.	com	Well Riser Interval: NA	Well Riser Type:	NA				
Depth (ft)	Sample number	Sample Interval	Blows	Rec/Driven (in.)	Description		Stratum	Headspace Results (ppm)	Saturation Test Result	Depth (ft)	Well Construction
0	S-1	0-2	NA	48/48	organic SILT, 2.5Y 3/3 dark olive bro	wn, medium dense,				0	
					slightly plastic, dry			1.7			
1										1	
2	6.2	2.4					SILT			2	
2	3-2	2-4			Same as above					2	
3								1.8	Neg	3	
										÷	
4	S-3	4-6	NA	24/48	clayey SAND, 2.5Y 5/3 light olive bro	wn, stiff, plastic, dry				4	
								15	Nea		
5								1.5	neg	5	No well
							SAND				installed
6	S-4	6-8			same as above					6	at this
7								2.9		7	location.
1										1	
8	S-5	8-10	NA	40/48	CLAY 2 5Y 4/2 dark gravish brown is	tiff very plastic dry				8	
Ŭ	00	0 10	117.1	10/10	CERT, 2.51 4/2 dark gravish brown, 3					0	
9								3.6	Neg	9	
10	S-6	10-12			same as above		CLAY			10	
11								2.8		11	
4.0				ļ	T					10	
12					rerminated boring at 12.0 feet below	ground surface				12	

NA = not applicable.

NS = not sampled.

ppm = parts per million.

Soil headspace screening completed with a MiniRae 3000 Photoionization Detector (PID). Neg = negative result using Oil in Soil shaker test kit as prescribed by MEDEP Standard Operating Procedure TS 004.

	BORING AND MONITORING WELL LOG								IG #:		SB-4
					Project Number: 3410.2	Client/Location:	Charter	Realty,	St. Pa	atric	ks Church
	St.Ge	ermair	n Colli	ins	Date of Installation: 3/4/13	Representative:	Brian Ba	ichman	n		
					Total Depth of Boring: 12.0	EPI					
					Depth to Water: NA	Drilling Technology:	Direct pu	ısh			
	8	846 Main	Street		Depth of Well: NA	Sampler:	Dual Tul	be			
	West	brook, N	laine 040	092	Well Screen Interval: NA	Well Screen Type:	NA				
	www.s	stgermai	ncollins.	com	Well Riser Interval: NA	Well Riser Type:	NA				
Depth (ft)	Sample number	Sample Interval	Blows	Rec/Driven (in.)	Description		Stratum	Headspace Results (ppm)	Saturation Test Result	Depth (ft)	Well Construction
0	S-1	0-2	NA	48/48	organic SILT, 2.5Y 3/3 dark olive brow	wn, medium dense,				0	
					slightly plastic, dry			1.1			
1										1	
2	6.2	2.4					SILT			2	
2	3-2	2-4			same as above					2	
3								1.5	Neg	3	
										•	
4	S-3	4-6	NA	24/48	clayey SAND, 2.5Y 5/3 light olive brow	wn, stiff, plastic, dry				4	
						, ,, , ,		10			
5								1.0		5	No well
							SAND			_	installed
6	S-4	6-8			same as above		•••••			6	at this
7								2.4	Neg	-	location.
1									_	1	
8	S-5	8-10	ΝΔ	40/48	CLAY 2 5V 4/2 dark gravish brown	tiff vonunlastia dru				8	
0	0-0	0-10		+0/+0	CLAT, 2.51 4/2 UAIK gravish brown, S	un, very plastic, ury				0	
9								0.9		9	
										•	
10	S-6	10-12			same as above		CLAY			10	
11								0.9	Neg	11	
12					Terminated boring at 12.0 feet below	ground surface				12	

NA = not applicable.

NS = not sampled.

ppm = parts per million.

Soil headspace screening completed with a MiniRae 3000 Photoionization Detector (PID). Neg = negative result using Oil in Soil shaker test kit as prescribed by MEDEP Standard Operating Procedure TS 004.