

Geotechnical Report

UNE Dental School Building Stevens Avenue Portland, Maine

Prepared for:

University of New England

Prepared by:

Summit Geoengineering Services Project #11296 January 2012



January 31, 2012 Summit #11296

Al Thibeau University of New England 11 Hills Beach Road Biddeford, Maine 04005

Reference: Geotechnical Investigation, Proposed Dental School Building Stevens Avenue, Portland, Maine

Dear Al;

We have completed the geotechnical investigation for the proposed new dental school building at the Portland Campus. Our scope of services included performing 5 test borings at the site and preparing this report summarizing our findings and geotechnical recommendations.

1.0 <u>Project Description</u>

The project consists of the construction of a new building on the UNE campus at 750 Stevens Avenue in Portland. The building has a footprint of approximately 18,000 square feet. We understand that a parking level will be constructed beneath the building. The parking level will be at a depth of approximately 4 feet below the existing grade (elevation 23 feet +/-) and will have a paved surface. The location of the proposed building is currently occupied by three wood frame structures, two garages, parking lots, and lawns.

Column loads are estimated to range from 215 kips to 610 kips with a live load to dead load ratio of approximately 50% to 60%. Columns will be spaced from 15 to 35 feet.

2.0 <u>Subsurface Exploration and Laboratory Testing</u>

Summit Geoengineering Services (SGS) observed the subsurface conditions with the drilling of 5 borings on January 12, 2012. The borings were located by taping from existing buildings. Northern Test Borings, under contract to SGS, advanced the borings using 2¹/₄-inch hollow stem augers. Two borings were performed to a depth of 22 feet and three borings were advanced to refusal, ranging from16.1 to 27.4 feet. Standard penetration tests (SPT) with split spoon samples were obtained at 5-foot intervals. A 1-inch diameter PCV groundwater observation well was installed in boring B-3.

Summit was onsite to coordinate and observe the boring explorations. The location of the borings is shown on Boring Location Plan in Appendix A. Logs of the explorations are included in Appendix B.

The sample taken at a depth of 5 to 7 feet in B-4 was tested for grain size analysis in accordance with ASTM 422. The results of this test are presented in Appendix A.

3.0 <u>Subsurface Conditions</u>

The subsurface conditions generally consist of *topsoil* overlying *glacial marine deposits* overlying *glacial till* explored to a depth of 16.8 to 27.4 feet. Bedrock was encountered at borings B-1, B-2, and B-4 at depths of 27.4 feet, 20.4 feet, and 16.8 feet, respectively. The subgrade is further described into 3 layers as follows:

The topsoil ranged from 6 to 12 inches in thickness consisting of dark brown silt with little sand and rootlets and is visually classified as ML in accordance with the Unified Soil Classification System (USCS). The topsoil was generally loose to compact and damp to frozen.

The glacial marine deposit consisted of light brown to tan medium-fine sand with a trace to little silt and is visually classified as SM or SP in accordance with the Unified Soil Classification System (USCS). The sample taken in B-4 at a depth of 5 to 7 feet contained 97.9% sand and 2.1% silt. This sample has a USCS classification of SP. SPT-N values for the sand ranged from 4 to 38 blows per foot (bpf) and averaged 20 bpf, indicating compact to dense conditions. The glacial marine deposits were generally damp.

The glacial till, encountered in B-1, B-2, and B-4, ranged from brown medium-fine to mediumcoarse sand with little silt and gravel to brown silty clay with some sand and little gravel. The glacial till is visually classified as SM and CL in accordance with the Unified Soil Classification System (USCS). SPT-N values for the sand ranged from 54 to 62 blows per foot (bpf), indicating very dense / hard conditions. The glacial marine deposits were generally damp

Bedrock was encountered at borings B-1, B-2, and B-4 at depths of 27.4 feet, 20.4 feet, and 16.8 feet, respectively. Refusal was not encountered in the other explorations. Bedrock mapping by the Maine Geological Survey indicates the bedrock is part of the Berwick Formation consisting of fine-grained gray quartz-plagioclase biotite gneiss.

Groundwater was not observed in our explorations. Groundwater was measured at a depth of 20.3 feet in the observation well at B-3 on January 25, 2012.

4.0 Foundation Design Recommendations

Based on the proposed finished exterior grade (paved parking lot) and the required frost protection depth, the footings for the new building will be constructed on the native sandy glacial marine deposit. With proper preparation, this soil is suitable to support the proposed building on conventional spread footing foundations.

A. Allowable Bearing Pressure

We recommend that the foundations be designed using an allowable bearing pressure of 4,000 psf for interior and exterior isolated and continuous footings. For the proposed footing loads, the

total settlement associated with the above bearing pressure ranges from $\frac{1}{2}$ " to $\frac{3}{4}$ ". Due to the uniformity of the subsurface conditions, differential settlement will be negligible, on the order of 0.1%.

We recommend that the subgrade soil in the building footprint be prepared as follows:

- Remove topsoil, pavement, and existing building foundations in their entirety from within the building footprint. Voids left after the removal of existing foundations can be backfilled with the existing sandy glacial marine soil. This soil should be compacted to 95% of its maximum dry density where it is placed within the building footprint. Outside the building footprint the compaction requirement can be reduced to 90%.
- After removal and backfilling of removed foundations, the soil within the building footprint is proofrolled prior to excavating for the footings. Proofrolling should consist of making a minimum of 5 passes in 2 perpendicular directions using a large vibratory roller with a minimum operating weight of 10 tons.
- Exterior footings are constructed to a depth of 4 feet below exterior grade for frost protection.
- Footing trenches are excavated using a smoothed edge bucket to minimize disturbance to the native soil. The footing subgrade should be proofrolled to redensify the disturbed soil. Proofrolling should consist of making a minimum of 5 passes using a large walk behind vibratory roller. Wet and soft areas, if encountered, should be removed and replaced with crushed stone.

We recommend the following parameters be used for the existing sandy glacial marine soil in the design of subsurface structures.

DESIGN PARAMETERS – EXISTING SANDY	Y GLACIAL MARINE SOIL
Total Natural (moist) Unit Weight (γ_t)	125 pcf
Saturated (buoyant) Unit Weight (γ_s)	63 pcf
Friction Coefficient (f)	0.45
Passive Earth Pressure Coefficient (K _p)	3.1
Active Earth Pressure Coefficient (K _a)	0.33
Friction Angle (f _c)	30^{0}
Cohesion (c)	0

B. Frost Protection

The design air freezing index for the Portland area is approximately 1,200 degree F days (10 year, 90% probability). Based on this, exterior footings on the existing granular fill soil should be constructed at a minimum depth of 4 feet below the exterior finished grade.

We recommend that the exterior of the foundation walls be backfilled with soil meeting the following gradation specification:

FOUNDATION BACKFILL (FB)					
Sieve Size	Percent finer				
3 inch	100				
¹ / ₄ inch	60 to 100				
No. 40	0 to 50				
No. 200	0 to 7				

Reference: MaineDOT Specification 703.06, Type F

The maximum particle size should be limited to 6 inches. The Foundation Backfill should be compacted to a minimum of 95 percent of its maximum dry density, determined in accordance with ASTM D1557. This compaction requirement can be reduced to 90% in landscaped areas.

The interior of foundation walls should be backfilled with Structural Fill as described below.

C. Building Slab

We recommend the building slab be constructed on a minimum 12-inch thick layer of Structural Fill (SF). The maximum particle size should be limited to 6 inches and meet the following gradation specifications passing the 3-inch sieve:

STRUCTURAL FILL (SF)							
Sieve Size	Percent finer						
3 inch	100						
1/4 inch	0 to 70						
No. 200	0 to 10						

Reference: MDOT Specification 703.20, Gravel Borrow

SF should be placed in 6 to 12-inch lifts and should be compacted to 95 percent of its maximum dry density determined in accordance with ASTM D1557.

An alternative is to construct the slab on 6 inches of ³/₄ inch crushed stone. The crushed stone can be placed directly on the proofrolled subgrade. It should be compacted using a vibratory roller sufficiently to lock the aggregate particles together.

For the conditions described above, the slab can be designed using a subgrade modulus of 175 pci.

We recommend the subgrade be proof-rolled as described in Section 4A of this report.

D. Groundwater Control

Groundwater was not observed in the explorations performed at the site. The water level was measured at a depth of 20.3 feet in the observation well at boring B-3 on January 25, 2012. This measurement was taken with an electronic depth meter. Based on this we anticipate that groundwater will be well below the bottom of the building footings and perimeter underdrains are not strictly necessary.

It is generally good practice to install underdrains to account for unanticipated changes in regional hydrogeology and to control potential infiltration of surface or roof runoff water into the foundation backfill. We recommend exterior grades slope away from the building footprint to reduce runoff water from infiltrating the Foundation Backfill.

Perimeter underdrains, if used, should consist of 4 inch rigid perforated PVC placed adjacent to the exterior footings and surrounded by a minimum of 6 inches of crushed stone wrapped in filter fabric to prevent clogging from the migration of the fine soil particles in the foundation backfill soils. The underdrain pipe should be outlet to a location where it will be free flowing. Where exposed at the ground surface, the ends of pipes should be screened or otherwise protected from entry and nesting of wildlife, which could cause clogging.

E. Seismic Design

Based on the depth to bedrock, the soil descriptions, and the blow counts obtained in the test borings, the soil at the site is classified as Seismic Site Class C in accordance with the International Building Code (IBC). We recommend the following seismic design coefficients be used:

SUBGRADE SITE SEISMIC DESIGN COEFFICIENTS - IBC							
Seismic Coefficient	Site Class C						
Short period spectral response (S _S)	0.314						
1 second spectral response (S ₁)	0.077						
Site coefficient (F _a)	1.2						
Site Coefficient (F_v)	1.7						
Design short period spectral response (S _{DS})	0.251						
Design 1 second spectral response (S _{DS})	0.087						

The sandy glacial marine are not susceptible to liquefaction based on their density.

5.0 Earthwork Considerations

Voids remaining after the removal of existing building foundations can be backfilled with the existing sandy glacial marine soil. This soil should be compacted to 95% of its maximum dry density where it is placed within the building footprint. Outside the building footprint the compaction requirement can be reduced to 90%.

Groundwater will not be an issue during construction of the footings. We recommend that surface water be diverted away from open excavations and that the footing trenches be kept dry.

We recommend that the building footprint be proofrolled as described in section 4.0A prior to placing SF or constructing foundations.

The existing glacial marine deposit may is too fine to meet the specifications for Foundation Backfill or Structural Fill.

Utility trenching and general excavations below 4 feet should be sloped no greater than 1.5H to 1V (OSHA type C) in the native sand. These slopes are based on the current OSHA Excavation Guidelines.

We recommend that a qualified geotechnical consultant be retained to monitor and test soil materials used during construction and confirm that soil conditions and construction methods are in consistence with this report.

7.0 Closure

Our recommendations are based on professional judgment and generally accepted principles of geotechnical engineering. Some changes in subsurface conditions, building elevations, and loads from those presented in this report may occur. Should these conditions differ materially from those described in this report, Summit should be notified so that we can re-evaluate our recommendations.

We appreciate the opportunity to serve you during this phase of your project. If there are any questions or additional information is required, please do not hesitate to call.

Sincerely yours, Summit Geoengineering Services,

William M. Peterlein, P.E. President & Principal Engineer



APPENDIX A

EXPLORATION LOCATION PLAN



APPENDIX B

EXPLORATION LOGS

EXPLORATION REPORT COVER SHEET

The exploration report has been prepared by the geotechnical engineer from both field and laboratory data. Differences between field logs and exploration reports may exist.

It is common practice in the soil and foundation engineering profession that field logs and laboratory data sheets not be included in engineering reports, because they do no represent the engineer's final opinion as to appropriate descriptions for conditions encountered in the exploration and testing work. The field logs will be retained in our office for review. Results of laboratory tests are generally shown on the borings logs or are described in the text of the report as appropriate.

Drilling and Sampling Symbols:

SS = Split Spoon	Hyd = Hydraulic advance of probes
ST = Shelby Tube - 2'' OD, disturbed	WOH = Weight of Hammer
UT = Shelby Tube - 3" OD, undisturbed	WOR = Weight of Rod
HSA = Hollow Stem Auger	GS = Grain Size Data
CS = Casing - size as noted	PI = Plasticity Index
Sv = Vane Shear	LL = Liquid Limit
PP = Pocket Penetrometer	w = Natural Water Content
RX = Rock Core - size as noted	USCS = unified Soil Classification System

Water Level Measurements:

Water levels indicated on the boring logs are the levels measured in the boring at the times indicated. In pervious soils, the indicated elevations are considered reliable groundwater levels. In impervious soils, the accurate determination of groundwater elevations may not be possible, even after several days of observations; additional evidence of groundwater elevations via observation or monitoring wells must be sought.

Gradation Description and Terminology:

Boulders:	Over 8 inches	Trace:	Less than 5%
Cobbles:	8 inches to 3 inches	Little:	5% to 15%
Gravel:	3 inches to No.4 sieve	Some:	15% to 25%
Sand:	No.4 to No. 200 sieve	Silty, Sandy, etc.:	Greater than 25%
Silt:	No. 200 sieve to 0.005 mm		
Clay:	less than 0.005 mm		

Density of Granular Soils and Consistency of Cohesive Soils:

CONSISTENCY OF C	OHESIVE SOILS	DENSITY OF GRANULAR SOILS			
SPT N-value blows/ft	Consistency	SPT N-value blows/ft	Relative Density		
0 to 2	Very Soft	0 to 3	Very Loose		
3 to 4	Soft	4 to 9	Loose		
5 to 8	Firm	10 to 29	Compact		
9 to 16	Stiff	30 to 49	Dense		
17 to 32	Very Stiff	50 to 80	Very Dense		
>32	Hard				

		\wedge			SOIL BORING LOG			Boring #:	B-1
		CIINAN	ANT		Project:	UNE Dental Bu	ilding	Project #:	11296
					Location:	Stevens Avenu	e	Sheet:	1 of 2
	GEO	ENGINEERING	SERVICES			Portland, Main	е	Chkd by:	
Drilling	Co:	Northern Tes	t Boring		Boring Location:		Taped from existing buil	dings by Summit	
Personn	iel:	Nick			Elevation:		128 ft +/-		
Summit	Staff:	Erika Hawksl	еу		Date started:	1/12/2012	Date Completed:	1/12/2012	
DF	RILLING N	ATT /	SAN	MPLER			ESTIMATED GROUND \	VATER DEPTH	с.
Venicie:		AIV Diadriah D EO	Type:	24" SS	Date	Depth	Elevation	Kens Observed	erence
Method		2 1/4" HSA	Fall.	30"	1/12/2012	IN/ E	IN/ E	None Observed	
Depth		2 174 113/	r un.	30		SAMPI	F	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	Blows/6 in.		DESCRIP	LION	Test Data	Stratum
	S-1	24/20	0 - 2	5	Brown SILT, roo	tlets, loose, dar	np to frozen, ML	Lawn	TOPSOIL
1				4	Dark brown SILT	r, trace Sand ar	nd organics, loose,		0.7'
_				5	damp, ML				
2				4					GLACIAL MARINE
					-				DEPOSITS
3_									
4					-				
4-					-				
5					1				
Ŭ -	S-2	24/21	5 - 7	6	Light brown to b	rown medium-f	ine to medium-coarse		
6				8	SAND, little Silt,	compact, damp	, SM		
				10					
7				8	-				
					-				
8_									
0					-				
9-									
10					-				
	S-3	24/22	10 - 12	7	Tan to light brov	vn fine to mediu	um-fine SAND, little		
11				8	Silt, compact, damp, SM				
				9					
12				11	-				
10					-				
13									
1/									
14					-				
15									
	<u>S-</u> 4	24/20	15 - 17	10	Tan to light brov	vn medium-fine	SAND, little Silt,		
16				12	compact, damp,	SM			
				15	4				
17				15	4				
10					4				
10					1				
19					1				
1					1				
20]				
	S - 5	24/20	20 - 22	14	Tan to light brov	vn medium-coa	rse SAND, Itrace Silt,		
21				17	dense, damp to	moist, SP			
				19	4				
22				21	1				
Granu	lar Soils	Cohesin	re Soils	% Composition	NOTES	PP = Porket Da	enetrometer Resistance		Soil Moisture Condition
Blows/ft.	Densitv	Blows/ft.	Consistency						Dry: $S = 0\%$
0-4	V. Loose	<2	V. soft		Bedrock Joints				Humid: $S = 1$ to 25%
4-10	Loose	2-4	Soft	<5% trace	Shallow = 0 to 35	degrees			Damp: S = 26 to 50%
10-30	Compact	4-8	Firm	5-15 little	Dipping = 35 to 55	5 degrees			Moist: S = 51 to 75%
30-50	Dense	8-15	Stiff	15-25 some	Steep = 55 to 90 c	degrees			Wet: S = 76 to 99%
>50	V. Dense	15-30	V. Stiff	>25 and		10/ -			Saturated: S = 100%
L		>30	Hard		Boulders = diamet	er > 12 inches, C	obbles = diameter < 12 inc	hes and > 3 inches	

		\sim			SOIL BORING LOG			Boring #:	B-1
1		SILAAA	AN		Project: UNE Dental Building F			Project #:	11296
1	4	SUIVIN			Location:	Stevens Avenu	e	Sheet:	2 of 2
	GEO	ENGINEERING	SERVICES			Portland, Main	e	Chkd by:	
Drilling	Co:	Northern Tes	st Boring		Boring Location:		Taped from existing buil	dings by Summit	
Personn	el:	Nick			Elevation:		128 ft +/-		
Summit	Staff:	Erika Hawks	ey	101 55	Date started:	1/12/2012	Date Completed:	1/12/2012	
DF	RILLING	METHOD	SAI	MPLER	Dete	Derth	ESTIMATED GROUND V	VATER DEPTH	-forence
Venicle:		AIV Diodrich D 50	Type:	24" SS	Date 1/12/2012	Depth	Elevation	None Observed	erence
Method		2 1/4" HSA	Fall [.]	30"	1/12/2012	IN/ E	IN/E	None Observed	
Depth		2 1/1 110/1	i un	00		SAMPI	E	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	Blows/6 in.	-	DESCRIP	ΓΙΟΝ	Test Data	Stratum
23					-				GLACIAL MARINE
23_					-				DEFOSITS
24_									24'+/-
25_	S-6	24/20	25 - 27	23	Tan medium-coa	irse SAND, som	e Gravel, verv dense,		GLACIAL TILL
26				30	moist, SP, overly	ving brown med	lium-fine SAND,		
27				32 27	nutie slit and Gra	ivei, very dense	, moist, SM		
28					Auger Refusal at	27.4', Probable	e Bedrock		27.4'
29									PROBABLE BEDROCK
20					-				
30_					-				
31_					-				
32_									
33_					-				
34					-				
35					-				
36									
27					-				
37_					-				
38_					_				
39					-				
40					1				
41					4				
42					}				
43					-				
A A									
44									
Granu	lar Soils	Cohesiv	ve Soils	% Composition	NOTES:	PP = Pocket Pe	enetrometer Resistance		Soil Moisture Condition
Blows/ft.	Density	Blows/ft.	Consistency		De des els 1 1 1				Dry: $S = 0\%$
0-4	V. Loose	<2	V. soft	-EQ(+====	Bedrock Joints	dogroop			Humid: $S = 1$ to 25%
4-10	LOOSE	2-4 1 0	SOIT	< 5 % [face	Snallow = 0 to 35 Dipping = 25 to 55	uegrees degrees			Damp: $S = 20 \text{ to } 50\%$
30 50	Denso	4-0 Q 1F	CHIFF	15-25 come	Steen = 55 to 00 co	loaroos			Wet: $S = 76 + 0.00\%$
>50	V Dense	15-30	V Stiff	>25 and	5166p - 55 10 90 0	icgi ees			Saturated: $S = 100\%$
- 50	7. Dense	>30	Hard	. 20 and	Boulders = diamet	er > 12 inches, C	obbles = diameter < 12 incl	nes and > 3 inches	Saturated. 5 = 10070

		\sim			SOIL BORING LOG			Boring #:	B-2
		CIINAN	AN		Project:	Project: UNE Dental Building			11296
	<u>_</u>	DUIVIIV			Location: Stevens Avenue			Sheet:	1 of 1
	GEO	ENGINEERING	SERVICES			Portland, Main	e	Chkd by:	
Drilling	Co:	Northern Tes	st Boring		Boring Location:		Taped from existing build	ings by Summit	
Personn	iel:	Nick			Elevation:	1/10/0010	127 ft +/-	1/10/2012	
Summit	Starr:		ey CAI		Date started:	1/12/2012			
Vehicle			JVDQ:	24" SS	Date	Denth	ESTIVIATED GROUND W		ference
Model:	I	Diedrich D-50	Hammer:	140 lb	1/12/2012	N/E	N/E	None Observed	
Method	:	2 1/4" HSA	Fall:	30"					
Depth						SAMPL	E	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	Blows/6 in.		DESCRIP	ΓΙΟΝ	Test Data	Stratum
	S-1	24/20	0 - 2	10	Dark brown SILT	, rootlets, little	Sand, loose to compact,	Lawn	TOPSOIL
1_				2	damp to frozen,	ML modium fino f	AND little Silt Jacco		11
2				2	damp SM	e meaium-nne s	and, Iitlie Siit, Ioose,		
<u> </u>				2	damp, SM				GLACIAL MARINE
3									DEPOSITS
-									
4									
_					-				
5_	5.2	24/24	57	4	Prownich orange	modium fino S	AND little Silt Joeco		
6	3-2	24/24	5-7	4	damn SM	e meulum-nne s	SAND, IIIIle SIII, IOOSE,		
°-				3	Light brown to ta	an fine SAND, li	ttle Silt, loose, damp,		
7				5	SM				
8									
0					-				
9_					-				
10									
	S-3	24/20	10 - 12	11	Light brown to ta	an medium-fine	SAND, little Silt,		
11				12	compact, damp,	SM			
				19					
12				23	-				
12					-				
13_									
14					-				
-									
15									
	S-4	24/18	15 - 17	12	Same as above,	compact, damp	o, SM		
16				17	4				
17				21 10	1				
· · · -				17	1				
18]				
1 -					1				
19					4				
20					4				
20	S-5	5/5	20 - 20 /	50/5"	Same as above	e light brown	dense damn SM		
21	5-5	5/5	20 - 20.4	30/3	Brown Silty CLA	, some Sand. I	ittle Gravel, verv dense.		20.2'
					damp, CL				GLACIAL TILL
22					Auger Refusal at	20.4', Probable	Bedrock		20.4'
L									PROBABLE BEDROCK
Granu	lar Soils	Cohesiv	ve Soils	% Composition	NOTES:	PP = Pocket Pe	enetrometer Resistance		Soil Moisture Condition
BIOWS/ft.	V	BIOWS/ft.	Consistency		Bedrock Joints				DFY: $S = 0\%$ Humid: $S = 1$ to 25%
4-10	Loose	2-4	Soft	<5% trace	Shallow = 0 to 35	degrees			Damp: $S = 26 \text{ to } 50\%$
10-30	Compact	4-8	Firm	5-15 little	Dipping = 35 to 55	5 degrees			Moist: $S = 51$ to 75%
30-50	Dense	8-15	Stiff	15-25 some	Steep = 55 to 90 c	legrees			Wet: S = 76 to 99%
>50	V. Dense	15-30	V. Stiff	>25 and					Saturated: S = 100%
		>30	Hard		Boulders = diamet	er > 12 inches, C	obbles = diameter < 12 inch	es and > 3 inches	

		\sim			SOIL BORING LOG			Boring #:	B-3
		CIINAN	TIL		Project: UNE Dental Building F			Project #:	11296
	<u>_</u>	DUIVIIV			Location: Stevens Avenue			Sheet:	1 of 1
	GEO	ENGINEERING	SERVICES			Portland, Main	e	Chkd by:	
Drilling	Co:	Northern Tes	st Boring		Boring Location:		Taped from existing build	ings by Summit	
Personn	el:	Nick			Elevation:	4/40/0040	127 ft +/-	4/40/0040	
Summit	Starr:		ey Can		Date started:	1/12/2012			
Ur Vobiclo:	KILLING N		SAI Typo:		Dato	Dopth	ESTIMATED GROUND W		foronco
Model:		Diedrich D-50	Hammer:	140 lb	1/12/2012	N/F	N/F	Measurement in we	II. No water observed
Method:		2 1/4" HSA	Fall:	30"	1/25/2012	20.3	106.7 ft +/-	Measurement in we	
Depth			0			SAMPI	E	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	Blows/6 in.		DESCRIP	TION	Test Data	Stratum
	S-1	24/20	0 - 2	10	Brown SILT, root	tlets, compact,	damp to frozen, ML	Lawn	TOPSOIL
1_				6	Dark brown SILT	, trace Sand ar	nd organics, loose		0.5'
2				4	to compact, dam	np to frozen, Mi	-		
² _				4					
3									DEI OSTIS
_									
4									
5_	6.0	24/10	F 7	7			to first CAND little		
6	5-2	24/18	5 - 7	7	Light brown to ta	an medium-fine	e to fine Sand, little		
<u> </u>				10	Siit, compact, ua	imp, sivi			
7				10					
_									
8									
9_									
10									
10_	S-3	24/20	10 - 12	7	Light brown to ta	an medium-fine	to medium-coarse		
11				10	SAND, little Silt,	compact, damp			
_				15					
12				24					
10									
13_									
14									
···_									
15									
	S-4	24/16	15 - 17	15	Light brown coar	rse SAND, trace	e Silt, compact, damp,		
16				14	SP, overlying light	nt brown fine S.	AND, little Silt, compact,		
17				10	uamp, SM				
1/-				17	1				
18					1				
_]				
19									
~~					{				
20	<u>с</u> г	24/14	20 22	11	light brown to	tan medium f	ing SAND little Silt		
21	3-0	24/10	20-22	12	compact. damp t	to moist. SM			
l -·-				12	and a set a set a set of a set				
22				12					
					End of Exploration	on at 22', No Re	efusal		22'
Granu	lar Soils	Cohesiv	ve Soils	% Composition	NOTES:	PP = Pocket Pe	enetrometer Resistance		Soil Moisture Condition
Blows/ft.	Density	Blows/ft.	Consistency		Rodrock Islate				Dry: $S = 0\%$
0-4 4-10	v. LOOSE	<2 2_1	V. SOFT	<5% trace	Shallow - 0 to 35	dearees			Humiu: $S = 1 \text{ to } 25\%$
10-30	Compact	4-8	Firm	5-15 little	Dippina = $35 \text{ to } 55$	degrees			Moist: $S = 51 \text{ to } 75\%$
30-50	Dense	8-15	Stiff	15-25 some	Steep = 55 to 90 c	legrees			Wet: S = 76 to 99%
>50	V. Dense	15-30	V. Stiff	>25 and		-			Saturated: S = 100%
		>30	Hard		Boulders = diameter	er > 12 inches, C	obbles = diameter < 12 inche	es and > 3 inches	

			S	OIL BORI	NG LOG	Boring #:	B-4		
		CIINAN	ANT		Project:	UNE Dental Bu	ilding	Project #:	11296
Location: Stever			Stevens Avenu	ie	Sheet:	1 of 1			
	GEU	ENGINEERING	SERVICES			Portland, Main	e	Chkd by:	
Drilling	Co:	Northern Tes	st Boring		Boring Location:		Taped from existing build	dings by Summit	
Personn	el:	Nick Frike Howkel	01		Elevation:	1/12/2012	127 ft +/-	1/12/2012	
Summe			ey SAN		Date starteu.	1/12/2012			
Vehicle:		ATV	Type:	24" SS	Date	Depth	Elevation		eference
Model:	I	Diedrich D-50	Hammer:	140 lb	1/12/2012	N/E	N/E	None Observed	
Method		2 1/4" HSA	Fall:	30"					
Depth					-	SAMPL	-E	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	Blows/6 in.		DESCRIP		Test Data	Stratum
1	5-1	24/18	0 - 2	3	Brown SILL, roo	tiets, compact,	damp to frozen, ML	Lawn	
· · -				2		r, trace Sand, ic			0.5
2				3	-				GLACIAL MARINE
_									DEPOSITS
3					-				
4_									
5									
	S-2	24/20	5 - 7	5					
6				7	Light brown to ta	an medium-fine	to fine SAND, little		
_				10	Silt, compact, da	amp, SM			
/_				11	-				
8									
Ŭ –					-				
9									
					-				
10	6.2	24/20	10 10	10					
11	5-3	24/20	10 - 12	12	Light brown to tan medium-fine SAND, Little Silt,				
···-				14	compact to dens	ic, damp, sw			
12				17					
13_					-				
14									
14_									
15					-				
	S-4	21/14	15 - 16.8	19	Brown fine SANE	D, little Silt and	Gravel, very dense,		15'+/-
16				24	damp, SM				GLACIAL TILL
17				30 50/2"	-				
· · · -				30/3	Auger Refusal at	16.8'. Probable	e Bedrock		16.8'
18			1			,			PROBABLE BEDROCK
19					4				
20					-				
20					1				
21]				
22					4				
C	lor Selle	Cohort	in Soile	0/ Compatition	NOTES	DD - Dookot D	anatromator Decistores		Soil Moisture Candition
Granu Blows/ft	idi 3011S Densitv	Conesiv Blows/ft	Consistency	% composition	NUTES:	FF = POCKET PE	enetrometer kesistance		Drv: $S = 0\%$
0-4	V. Loose	<2	V. soft		Bedrock Joints				Humid: $S = 1$ to 25%
4-10	Loose	2-4	Soft	<5% trace	Shallow = 0 to 35	degrees			Damp: S = 26 to 50%
10-30	Compact	4-8	Firm	5-15 little	Dipping = 35 to 55	5 degrees			Moist: S = 51 to 75%
30-50	Dense	8-15	Stiff	15-25 some	Steep = 55 to 90 c	degrees			Wet: S = 76 to 99%
>50	V. Dense	15-30	V. Stiff	>25 and	Pouldoro diamant	or > 12 Inches 0	abblas - diamator - 10 le-l	oc and > 2 inches	Saturated: S = 100%
L		>30	Hard		Boulders = diamet	.er > 12 inches, C	oppies = diameter < 12 incl	ies and > 3 inches	

					SOIL BORING LOG			Boring #:	B-5
SILAAAIT			Project: UNE Dental Building			Project #:	11296		
δυινιινι			Location: Stevens Avenue			Sheet:	1 of 1		
	GEO	ENGINEERING	SERVICES			Portland, Main	e	Chkd by:	
Drilling Co: Northern Test Boring					Boring Location:		Taped from existing build	dings by Summit	
Personn	iel:	Nick			Elevation:		127 ft +/-		
Summit	Staff:	Erika Hawksl	еу		Date started:	1/12/2012	Date Completed:	1/12/2012	
	RILLING	METHOD	SAI	MPLER			ESTIMATED GROUND V	VATER DEPTH	<u>,</u>
Venicle:		AIV Diadriah D EO	Type:	24" SS	Date 1/12/2012	Depth	Elevation	K None Observed	ererence
Method			Fall.	30"	1/12/2012	IN/E	IN/E	None Observed	
Depth		2 1/4 113/	r un.	30		SAMPI	F	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	Blows/6 in.		DESCRIP	LION	Test Data	Stratum
()					Bituminous Pave	ment=6"			PAVEMENT
1	S-1	24/20	0.5 - 2.5	36	Brown SAND, litt	le Silt and Grav	el, compact, damp, SM		0.5'
_				15					
2				5					GLACIAL MARINE
				3	DE				DEPOSITS
3_					-				
4_					-				
5									
°_	S-2	24/2	5 - 7	14	Rock at spoon ti	p. Same as abo	ve		
6				8		-,			
_				9					
7				11					
8_									
0					-				
9_					-				
10					-				
10_	S-3	24/14	10 - 12	14	l ight brown to ta	an medium-fine	SAND compact		
11	00	20/11	10 12	14	damp, SP		of the , compact,		
				18					
12				18					
13									
					-				
14_					-				
15					-				
15	S-4	24/14	15 - 17	12	Same as above.	compact, damp). SP		
16				18			,		
_				17]				
17				16]				
					4				
18					4				
10					4				
19					1				
20					1				
-~~-	S-5	24/14	20 - 22	7	Light brown co	arse SAND, c	ompact, damp. SP.		
21				9	overlying tan fine	e SAND, compa	ct, damp to moist, SP		
				11					
22				9					
					End of Exploration at 22', No Refusal				22'
Granular Soils		Cohesive Soils		% Composition	NOTES: PP = Pocket Penetrometer Resistance			Soil Moisture Condition	
BIOWS/ft.	V	BIOWS/ft.	V soft		Bedrock Jointe				Ury: $S = 0\%$
0-4 4-10		<2 2_1	v. SUIL	<5% trace	Shallow = 0 to 35	dearees			Damp: $S = 26 \text{ to } 50\%$
10-30	Compact	4-8	Firm	5-15 little	Dipping = 35 to 55	degrees			Moist: $S = 51 \text{ to } 75\%$
30-50	Dense	8-15	Stiff	15-25 some	Steep = 55 to 90 degrees $Wolst: S = 51 to 75\%$ Wet: S = 76 to 90%				
>50	V. Dense	15-30	V. Stiff	>25 and		-			Saturated: S = 100%
		>30	Hard		Boulders = diamet	er > 12 inches, C	obbles = diameter < 12 inch	nes and > 3 inches	

APPENDIX C

LABORATORY TESTING



GRAIN SIZE ANALYSIS - ASTM D422

PROJECT NAME:	UNE Dental		PROJECT #:	14381 / 11296
CLIENT:	Summit Geoengineering Services	SUMMIT SAMPLE:	S2	
CLIENT SOIL DES:			INTENDED USE:	Investigation
SOURCE:	B4 5-7'		SPECIFICATION:	
DATE:	January 23, 2012		TECHNICIAN:	M. Gilman
		DATA		

PARTICLI	E SIZE mm	% BY WT FINER		
76.20	(3 in)	100.0		
50.80	(2 in)	100.0		
38.10	(1-1/2 in)	100.0		
25.40	(1 in)	100.0		
19.05	(3/4 in)	100.0		
12.70	(1/2 in)	100.0		
9.53	(3/8 in)	100.0		
6.35	(1/4 in)	100.0		
4.75	(No. 4)	100.0		
2.00	(No. 10)	99.5		
0.85	(No. 20)	95.5		
0.43	(No. 40)	83.5		
0.15	(No. 100)	15.9		
0.08	(No. 200)	2.1		



REMARKS:

Reviewed: Darrell A. Gilman, CMT Manager Date: 1/24/12