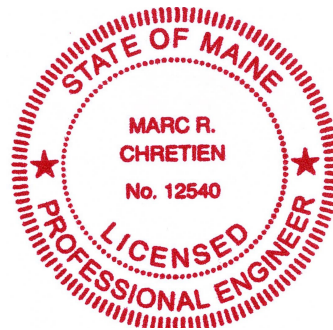


## Structural Design Calculations



A handwritten signature in black ink, appearing to read "Marc R. Chretien".

**Site No.:** 4DN2202A - Deering Pavilion  
**Client:** J Lee Associates  
**Date:** November 28, 2016

**Synopsis:**

The proposed T-Mobile equipment installation will be replacing three (3) existing EMS panel antennas with three (3) Ericsson AIR21 panel antennas. As detailed on plans by this office, the antennas will be mounted to the existing mount pipes that are supported by the existing industry-standard wall mounts.

**Loads:**

Environmental Loads:

*Wind Load:*

Exposure category,	EC := C	(ASCE 7-05 Sec 6.5.6.3)
Basic wind velocity,	V <sub>w</sub> := 98 mph	(MSBC Table 1604.11)
Importance factor,	I := 1 (Category II)	(ASCE 7-05 Table 6-1)
Height of Equipment,	Height := 110ft	
Exposure coefficient,	K <sub>z</sub> = 1.28	(ASCE 7-05 Table 6-3)
Velocity wind pressure,	q <sub>z</sub> := .00256 · V <sub>w</sub> <sup>2</sup> · K <sub>z</sub> · I · psf = 31.55 · psf	(ASCE 7-05 6.5.10)
Flat Force coeff.,	C <sub>f</sub> := 1.4	(ASCE 7-05 Fig. 6-21)
Wind load pressure,	WL <sub>f</sub> := q <sub>z</sub> · C <sub>f</sub> = 44.16 · psf	(ASCE 7-05 Sec. 6.5.15)
Round Force coeff.,	C <sub>r</sub> := 0.7	(ASCE 7-05 Fig. 6-21)
Wind load pressure,	WL <sub>r</sub> := q <sub>z</sub> · C <sub>r</sub> = 22.08 · psf	(ASCE 7-05 Sec. 6.5.15)
Radial ice thickness,	t <sub>ice</sub> := 0.75 · in	
Density of ice,	γ <sub>ice</sub> := 56 · pcf	

*Snow Load:*

Ground Snow Load	p <sub>g</sub> := 45psf	(ASCE 7-05 Fig. 7-1)
Exposure Factor	C <sub>e</sub> := 0.9 (Fully Exposed, exposure "B")	(ASCE 7-05 Table 7-2)
Thermal Factor	C <sub>t</sub> := 1.0	(ASCE 7-05 Table 7-3)
Importance Factor	I <sub>s</sub> := 1.0	(ASCE 7-05 Table 7-4)
Roof Snow Load,	p <sub>f</sub> := 0.7 · C <sub>e</sub> · C <sub>t</sub> · I <sub>s</sub> · p <sub>g</sub> = 28.35 · psf	(ASCE 7-05 Sec. 7.3)

## Analysis:

### Equipment Loads:

#### Proposed Antenna Properties:

Width,  $w_{\text{pant}} := 12 \cdot \text{in}$

Depth,  $t_{\text{pant}} := 8 \cdot \text{in}$

Length,  $l_{\text{pant}} := 56 \cdot \text{in}$

Weight,  $W_{\text{pant}} := 91.5 \cdot \text{lb}$

#### Weight of ice:

#### Proposed Antenna:

$$W_{\text{pant\_ice}} := \left[ \left( W_{\text{pant}} + (2 \cdot t_{\text{ice}}) \cdot \left[ t_{\text{pant}} + (2 \cdot t_{\text{ice}}) \cdot \left[ l_{\text{pant}} + (2 \cdot t_{\text{ice}}) \right] \right] - W_{\text{pant}} \cdot t_{\text{pant}} \cdot l_{\text{pant}} \right) \cdot \gamma_{\text{ice}} \right]$$

$$W_{\text{pant\_ice}} = 64.76 \text{ lb}$$

Wind force on proposed antenna,  $P_{\text{pa}} := \left( \sqrt{w_{\text{pant}}^2 + t_{\text{pant}}^2} \cdot l_{\text{pant}} \right) \cdot W_{\text{Lf}} = 247.7 \text{ lb}$

Reactions acting on pipe,  $P_{\text{pipe}} := \frac{P_{\text{pa}}}{2} = 123.85 \text{ lb}$

Moment on pipe,  $M_{\text{pipe}} := 568 \cdot \text{ft} \cdot \text{lb}$

See attached Enercalc output

Allowable moment,  $M_{\text{allow}} := 1.245 \cdot \text{ft} \cdot \text{kip}$

$$\text{MomentCheck} := \begin{cases} \text{"OK"} & \text{if } M_{\text{allow}} \geq M_{\text{pipe}} \\ \text{"NG"} & \text{otherwise} \end{cases}$$

MomentCheck = "OK"

#### Check Wall Mounts:

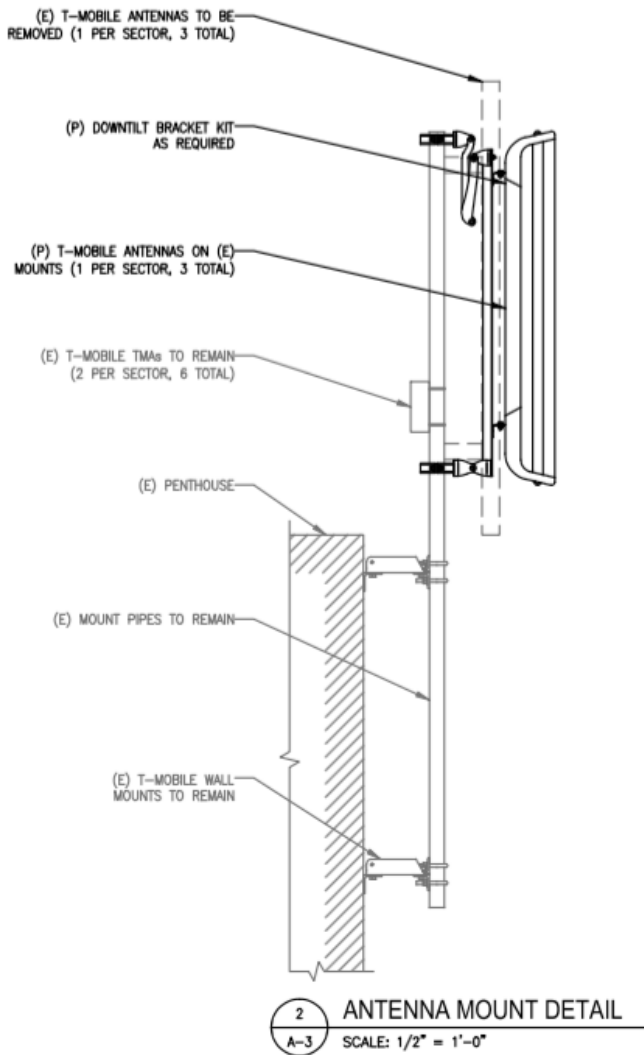
Total wind load acting on mount,  $P_{\text{tot}} := P_{\text{pa}}$

$$P_{\text{tot}} = 247.7 \text{ lb}$$

Weight of pipe, brackets,  $P_{\text{misc}} := 75 \cdot \text{lb}$

Distance of antenna off wall,  $d_1 := 16 \cdot \text{in}$

Fig. 1 Antenna Mount (from CDs)



Check Wall Mounts:

Wind force on proposed assembly,  $P_{\text{tot}} = 247.7 \text{ lb}$

Gravity load on assembly,  $P_g := W_{\text{pant\_ice}} + W_{\text{pant}} + P_{\text{misc}} = 231.26 \text{ lb}$

Bracket separation,  $d := 4 \cdot \text{ft}$

Number of bolts per bracket,  $n := 2$

$$\text{Approximate tensile force on bolt, } T_{\text{bolt}} := \frac{P_g \cdot d_1 + P_{\text{pipe}} \cdot [(d + 1.67 \cdot \text{ft}) + l_{\text{pant}}]}{d \cdot n}$$

$$T_{\text{bolt}} = 198.57 \text{ lb}$$

Allowable tensile capacity of 1/2" Hilti HIT HY 150,

$$T_{\text{allow}} := \frac{2725 \cdot \text{lb}}{4} = 681.25 \text{ lb}$$

$$\text{TensileCheck} := \begin{cases} \text{"OK"} & \text{if } T_{\text{allow}} \geq T_{\text{bolt}} \\ \text{"NG"} & \text{otherwise} \end{cases}$$

TensileCheck = "OK"

#### Conclusion:

**Based on the results of the analysis, the proposed T-Mobile 2100 MHz equipment installation is structurally sound, as designed and depicted on plans by this office entitled "4DN2202A, Deering Pavilion", Rev 0, 11/22/16". The analysis was conducted in accordance with the Maine Uniform Building and Energy Code, and ASCE 7-05.**

#### References:

1. American Society of Civil Engineers (2005), Minimum Design Loads for Buildings and Other Structures (7-05), American Society of Civil Engineers, New York, NY
2. Maine Uniform Building and Energy Code.

**Steel Beam**

File = x:\ENER-P21\4DN2-2FB.EC6  
ENERCALC, INC. 1983-2016, Build:6.16.10.31, Ver:6.16.10.31  
Licensee : **ADVANCED ENGINEERING GROUP, PC**

Lic. # : **KW-06008463**

Description : **Mount Pipe**

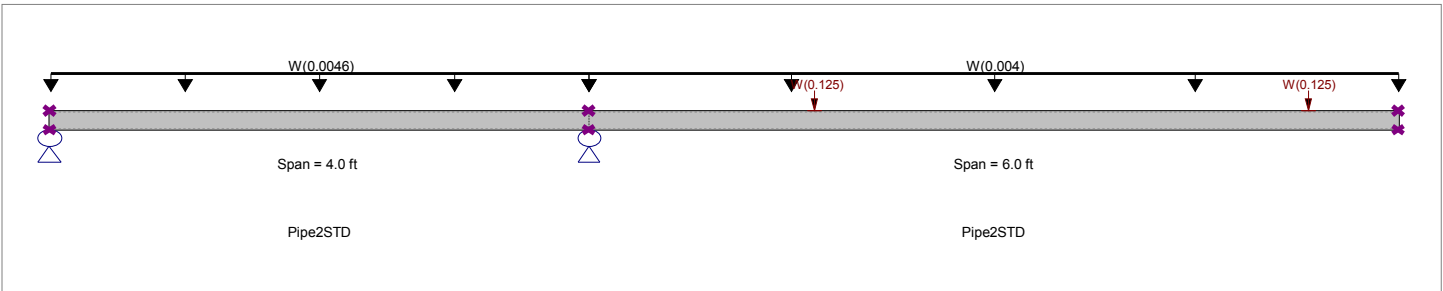
**CODE REFERENCES**

Calculations per AISC 360-05, IBC 2009, CBC 2010, ASCE 7-05  
Load Combination Set : ASCE 7-05

**Material Properties**

Analysis Method: **Allowable Strength Design**  
Beam Bracing: **Completely Unbraced**  
Bending Axis : **Major Axis Bending**

Fy : Steel Yield **35.0 ksi**  
E : Modulus : **29,000.0 ksi**



**Applied Loads**

Service loads entered. Load Factors will be applied for calculations.

Beam self weight NOT internally calculated and added  
Load for Span Number 1  
Uniform Load : W = 0.00460 k/ft, Tributary Width = 1.0 ft, (Wind)  
Load for Span Number 2  
Uniform Load : W = 0.0040 k/ft, Tributary Width = 1.0 ft, (Wind)  
Point Load : W = 0.1250 k @ 1.670 ft, (Antenna)  
Point Load : W = 0.1250 k @ 5.330 ft, (Antenna)

**DESIGN SUMMARY**

**Design OK**

Maximum Bending Stress Ratio =	<b>0.760</b> : 1	Maximum Shear Stress Ratio =	<b>0.043</b> : 1
Section used for this span	<b>Pipe2STD</b>	Section used for this span	<b>Pipe2STD</b>
Ma : Applied	0.947 k-ft	Va : Applied	0.2740 k
Mn / Omega : Allowable	1.245 k-ft	Vn/Omega : Allowable	6.413 k
Load Combination	<b>+D+W+H</b>	Load Combination	<b>+D+W+H</b>
Location of maximum on span	4.000ft	Location of maximum on span	4.000 ft
Span # where maximum occurs	<b>Span # 1</b>	Span # where maximum occurs	<b>Span # 1</b>
<b>Maximum Deflection</b>			
Max Downward Transient Deflection	1.567 in	Ratio =	<b>91</b> >=90.0
Max Upward Transient Deflection	-0.091 in	Ratio =	<b>524</b> >=90.0
Max Downward Total Deflection	1.575 in	Ratio =	<b>91</b> >=90.0
Max Upward Total Deflection	-0.091 in	Ratio =	<b>525</b> >=90.0

**Maximum Forces & Stresses for Load Combinations**

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values						Summary of Shear Values				
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega	
D Only															
Dsgn. L = 4.00 ft		1		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
Dsgn. L = 6.00 ft		2		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
+D+L+H															
Dsgn. L = 4.00 ft		1		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
Dsgn. L = 6.00 ft		2		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
+D+Lr+H															
Dsgn. L = 4.00 ft		1		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
Dsgn. L = 6.00 ft		2		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
+D+S+H															
Dsgn. L = 4.00 ft		1		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
Dsgn. L = 6.00 ft		2		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
+D+0.750Lr+0.750L+H															
Dsgn. L = 4.00 ft		1		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
Dsgn. L = 6.00 ft		2		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
+D+0.750L+0.750S+H															
Dsgn. L = 4.00 ft		1		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
Dsgn. L = 6.00 ft		2		0.000			2.08	1.25	1.00	1.00	-0.00	10.71	6.41		
+D+W+H															
Dsgn. L = 4.00 ft		1	0.760	0.043			-0.95	0.95	2.08	1.25	1.69	1.00	0.27	10.71	6.41



500 North Broadway  
 East Providence, RI 02914  
 (401) 354-2403

Project Title: **Cantilevered Pipe Mount**  
 Engineer: **MRC**  
 Project Descr: **L2100**

Project ID: **4DN2201A**

Printed: 28 NOV 2016, 4:42PM

**Steel Beam**

File = x:\ENER-P21\4DN2-2FB.EC6  
 ENERCALC, INC. 1983-2016, Build:6.16.10.31, Ver:6.16.10.31  
 Licensee : **ADVANCED ENGINEERING GROUP, PC**

Lic. #: **KW-06008463**

Description : **Mount Pipe**

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values						Summary of Shear Values				
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	VnxVnx/Omega		
Dsgn. L = 6.00 ft	2		0.760	0.043											
+D+0.70E+H															
Dsgn. L = 4.00 ft	1			0.000					2.08	1.25	1.00	1.00	-0.00	10.71	6.41
Dsgn. L = 6.00 ft	2			0.000					2.08	1.25	1.00	1.00	-0.00	10.71	6.41
+D+0.750Lr+0.750L+0.750W+H															
Dsgn. L = 4.00 ft	1		0.570	0.032		-0.71	0.71	2.08	1.25	1.69	1.00		0.21	10.71	6.41
Dsgn. L = 6.00 ft	2		0.570	0.032		-0.71	0.71	2.08	1.25	1.00	1.00		0.21	10.71	6.41
+D+0.750L+0.750S+0.750W+H															
Dsgn. L = 4.00 ft	1		0.570	0.032		-0.71	0.71	2.08	1.25	1.69	1.00		0.21	10.71	6.41
Dsgn. L = 6.00 ft	2		0.570	0.032		-0.71	0.71	2.08	1.25	1.00	1.00		0.21	10.71	6.41
+D+0.750Lr+0.750L+0.5250E+H															
Dsgn. L = 4.00 ft	1			0.000					2.08	1.25	1.00	1.00	-0.00	10.71	6.41
Dsgn. L = 6.00 ft	2			0.000					2.08	1.25	1.00	1.00	-0.00	10.71	6.41
+D+0.750L+0.750S+0.5250E+H															
Dsgn. L = 4.00 ft	1			0.000					2.08	1.25	1.00	1.00	-0.00	10.71	6.41
Dsgn. L = 6.00 ft	2			0.000					2.08	1.25	1.00	1.00	-0.00	10.71	6.41
+0.60D+W+H															
Dsgn. L = 4.00 ft	1		0.760	0.043		-0.95	0.95	2.08	1.25	1.69	1.00		0.27	10.71	6.41
Dsgn. L = 6.00 ft	2		0.760	0.043		-0.95	0.95	2.08	1.25	1.00	1.00		0.27	10.71	6.41
+0.60D+0.70E+H															
Dsgn. L = 4.00 ft	1			0.000					2.08	1.25	1.00	1.00	-0.00	10.71	6.41
Dsgn. L = 6.00 ft	2			0.000					2.08	1.25	1.00	1.00	-0.00	10.71	6.41

**Overall Maximum Deflections**

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
W Only	1	0.0000	0.000	W Only	-0.0914	2.320
	2	1.5750	6.000		0.0000	2.320

**Vertical Reactions**

Support notation : Far left is #'

Values in KIPS

Load Combination	Support 1	Support 2	Support 3
Overall MAXimum	-0.228	0.520	
Overall MINimum	-0.171	0.390	
D Only			
+D+L+H			
+D+Lr+H			
+D+S+H			
+D+0.750Lr+0.750L+H			
+D+0.750L+0.750S+H			
+D+W+H	-0.228	0.520	
+D+0.70E+H			
+D+0.750Lr+0.750L+0.750W+H	-0.171	0.390	
+D+0.750L+0.750S+0.750W+H	-0.171	0.390	
+D+0.750Lr+0.750L+0.5250E+H			
+D+0.750L+0.750S+0.5250E+H			
+0.60D+W+H	-0.228	0.520	
+0.60D+0.70E+H			
D Only			
Lr Only			
L Only			
S Only			
W Only	-0.228	0.520	
E Only			
H Only			



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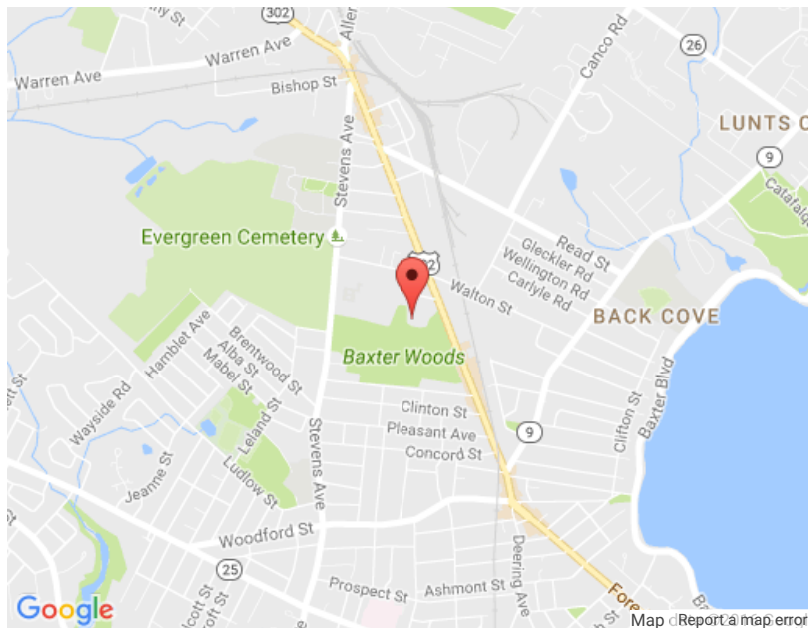
## Search Results

**Query Date:** Mon Nov 28 2016  
**Latitude:** 43.6781  
**Longitude:** -70.2899

**ASCE 7-10 Windspeeds  
 (3-sec peak gust in mph\*):**

**Risk Category I:** 107  
**Risk Category II:** 117  
**Risk Category III-IV:** 126  
**MRI\*\* 10-Year:** 76  
**MRI\*\* 25-Year:** 86  
**MRI\*\* 50-Year:** 91  
**MRI\*\* 100-Year:** 97

**ASCE 7-05 Windspeed:**  
 98 (3-sec peak gust in mph)  
**ASCE 7-93 Windspeed:**  
 83 (fastest mile in mph)



\*Miles per hour  
 \*\*Mean Recurrence Interval

Users should consult with local building officials to determine if there are community-specific wind speed requirements that govern.



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