Form # P 04 DISPLAY THIS CARD ON PRINCIPAL FRONTAGE OF WORK CITY OF PORTLAND

+

Please Read Application And Notes, If Any, Attached		Permit Number 05 155 UED
This is to certify that	ff	FEB - 2 - 2006
has permission to Multi-Family- new 24 unit	t a ment bi ing wordergroun wrking	
AT 98 GILMAN ST		DO03001CITY OF PORTLAND
provided that the person or persor	ns rm or entrone lepting	this permit shall comply with all
the construction, maintenance and this department.	d e of buildings and ouctures	, and of the application on file in
Apply to Public Works for street line and grade if nature of work requires such information.	ificatio of inspecton musice en and vien permition procide ore this ilding of urt there is ned or perwise losed-in 4 UR NO. THEQUIRED	A certificate of occupancy must be procured by owner before this build- ing or part thereof is occupied.
OTHER REQUIRED APPROVALS		
Fire Dept. <u>Grad</u> Arss 1-9-06 Health Dept		
Appeal Board		11 Tolala
Other		Director - Building & Intradition Services

PENALTY FOR REMOVING THIS CARD ℓ

ilding or 389 Congress Street, 04101 Tel: (207) 874			Permit 1 0	10: 5-177 3	Issue Date	ISSUED	CBL: 065	D003001
Location of Construction:	Owner Name:	·	Owner Add	lress:		2 0000	Phone:	
98 GILMAN ST	SILALUMI IIU		PO BOX	560		c /: .		
Business Name:	Contractor Name	:	Contractor	Address:	1/ A par pro	********	Phone	
	TBD			<u> </u>	YUFP	PRTLAN	þΙ	
Lessee/Buyer's Name	Phone:		Permit Typ Multi Fa	e: 1mily		and the second		Zone: R-
Past Use:	Proposed Use: Multi-Family- apartment buil parking	Proposed Use: Multi-Family- new 24 unit apartment building w/ underground parking		Permit Fee: Cost of Work: CEO District: \$24,396.00 \$2,700,000.00 2 FIRE DEPT: Approved INSPECTION: Denied Use Group: 542,702,702,000.00			t: 2_Type: 5-17	
Proposed Project Description: Multi-Family- new 24 unit apartment building w/ underground parking			Signature (PEDESTRI Action:	Cerce of IAN ACTT		Signature TRICT (P.A.	D.) (Denied
			Signature:			Da	te:	
Permit Taken By: ldobson	Date Applied For: 12/07/2005		,	Zoning	Approv	al		
1. This permit application do Applicant(s) from meeting Federal Rules.	bes not preclude the g applicable State and	Special Zone or Revi	ews	Zonin Variance	ng Appeal	Ŭ	Historic I / Not in Di	Preservation istrict or Landmark
2. Building permits do not in septic or electrical work.	nclude plumbing,	Wetland	0 - [Miscella	neous		Does Not	Require Review
 Building permits are void if work is not started within six (6) months of the date of issuance. 		Flood Zone PAre Zone		Conditio	nal Use		Requires	Review
permit and stop all work		Subdivision Site Plan	79	Approve	ation d		Approved	1 1 w/Conditions
		Maj K Minori MM Ol w h h (N Date	I CH	Denied		Date:	Denied	>

CERTIFICATION

I hereby certify that I am the owner of record of the named property, or that the proposed work is authorized by the owner of record and that I have been authorized by the owner to make this application as his authorized agent and I agree to conform to all applicable laws of this jurisdiction. In addition, if a permit for work described in the application is issued, I certify that the code official's authorized representative shall have the authority to enter all areas covered by such permit at any reasonable hour to enforce the provision of the code(s) applicable to such permit.

SIGNATURE OF APPLICANT	ADDRESS	DATE	PHONE
RESPONSIBLE PERSON IN CHARGE OF WORK, TITLE		DATE	PHONE

General Building Permit Application



If you or the property owner owes real estate or personal property taxes or user charges on any property within the City, payment arrangements must be made before permits of any kind are accepted.

Location/Address of Construction: Valley Str	eet Apartments	, Gilman Street - Portland, ME					
Total Square Footage of Proposed Structure		Square Footage of Lot 17.4	10 Sa	. Ft.			
7,938 Sq. Ft.			4				
Tax Assessor's Chart, Block & Lot Chart# 065 Block# Chart# 3-9	Owner: 315 Valley Street, L.P. PO Box 560 Portland, ME 04112			Telephone: (207) 874-1087			
Lessee/Buyer's Name (If Applicable)	Applicant na	ame, address & telephone:		ost Of			
	315 V PO B	/alley Street, L.P.	vv	01K. <u>\$ 2 700.000</u>			
	Portla	and. ME 04112	F	ee: <u>\$</u>24,321			
			С	of O Fee: \$ <u>1.800</u>			
Current Specific use: Vacant Lot				\$26,121 -Total			
Proposed Specific use: <u>R-2 Apartment Building</u>							
Project description: 24 Unit Apartment Building	g with Parking I	Below		24321			
				*24256			
Contractor's name, address & telephone: To be	edetermined			CN			
Who should we contact when the permit is read	dy: Bill Flo	ovd					
Mailing address:	Phone:(207)	874-1087		1 Section			
DEPT OF TOTAL							
Please submit all of the information out	lined in the	Commercial Application	Óhe	eklist.			
Failure to do so will result in the automa	atic denial o	f your permit.	```	λ			
In order to he sure the City fully understands the full scope of the project, the Planning and Development Department may request additional information prior to the issuance of a permit . For further information visit us on-line at <u>www.portlandmaine.gov</u> , stop by the Building Inspections office, room 315 City Hall or call 874-8703,							

I hereby certify that I am the Owner of record of the named property, or that the owner of record authorizes the proposed work and that I have been authorized by the owner to make this application as his/her authorized agent. I agree to conform to all applicable laws of this jurisdiction. In addition, if a permit for work described in this application is issued, I certify that the Code Official's authorized representative shall have the authority to enter all areas covered by this permit at any reasonable hour to enforce the provisions of the codes applicable to this permit.

	\sim	r r r r r r r r r r r r r r r r r r r
Signature of applicant:	David Llovd, As Apent for Shalom House	Date: 17-05

This is not a permit; you may not commence ANY work until the permit is issued.

City of Portland, Maine - Buil 389 Congress Street, 04101 Tel: (Permit No: 5 05-1773	Date Applied For: 12/07/2005	CBL: 065 D003001			
Location of Construction:	Owner Name:		Owner Address:		Phone:	
98 GILMAN ST	SHALOM HOUSE IN	чС	PO BOX 560			
Business Name:	Contractor Name:		Contractor Address:		Phone	
	Ledgewood Inc.		PO Box 8107 Port	land	(207) 767-1866	
Lessee/Buyer's Name	Phone:		Permit Type:	Permit Type:		
			Multi Family			
Proposed Use:		Propose	ed Project Description:			
Multi-Family- new 24 unit apartment parking	d Multi- parkir	-Family- new 24 uni Ig	t apartment building `	w/ underground		
Dept: Zoning -Status: A	Dept: Zoning -Status: Approved with Conditions Reviewer: Marge Schmuckal Approval Date: 01/18/2006					

Dept:	Fire	Status: - Approved with Conditions	Reviewer:	Cptn Greg Cass	Approval Date:	01/04/2	006
Note:					Ok t	o Issue:	\checkmark

Dept:	Planning	Status: Approved	with Conditions	Reviewer:	Barbara Barhydt	Approval Date:	01/25/2006
Note:						Ok	to Issue:
1) The conditions contained in the review by Carrie Marsh, Urban Designer, dated 10/13/05, shall be addressed by the applicant and							
revi	ewed and approve	d by the Planning Au	thority prior to the	issuance of a	a building permit.		

The Planning Board approved the following waiver: Upon the recommendation of the City's Traffic Engineer and his finding that parking activity and trunover should be minimal, and therefore the Planning Board does waive the City's Technical Standards for parking lots to allow the proposed aisle widths of 20 feet and a 20 foot curb uct into the basement level parking area.

3) A construction mobilization plan must be submitted for review and approval by the City prior to the issuance of a building permit.

4) A copy of the sewer capacity letter from the Department of Public Wrlks shall be subnutted prior to the release of the recording plat.

Location of Construction:	Owner Name:		Owner Address:	Phone:	
98 GILMAN ST	SHALOM HOUSE INC		PO BOX 560		
Business Name:	Contractor Name:		Contractor Address:	Phone	
	Ledgewood Inc.	PO Box 8107 Portland		(207) 767-1866	
Lessee/Buyer's Name	Phone:	Permit Type:			
			Multi Family		

8) The proposed Spectra III Area Luminaires shall be cut-off or full cut-off fixtures.

9) The grading and utility plan (Sheet 3) shall be revised showing the proposed underground electrical connection to the apartment building and a letter of capacity to serve from CMP shall be submitted prior to the release of the recording plat. The conditions contained in the review by Steve Bushey, Development Review Coordinator, DeLuca-Hoffman, Inc. Dated October 14, 2005 shall be met prior to issuance of a building permit.

Comments:

12/12/2005-mes: I do not have a stamped approved site plan - Barbara Barhydt said that she can not release it yet - She will also get me documentation when the zone was changed to R-7 - on hold in Marge's area

1/3/2006-mjn: Need statement of Special Inspections/Geotech report emailed John Shields.

1/20/2006-mjn: Hold for various planning prepermitting issues. Code issues

less than 5 inches (127 mm) when measured (in a horizontal plane) from tread nosing to the next tread nosing (see Figure 1009.10). Applying the limiting dimensions stated above would result in a device with a very steep incline (approximately4:1).

For alternating tread devices used as a means of egress from small-area mezzanines as prescribed in the exception, the treads must project at least $8^{1/2}$ inches (216 mm) as compared to the 5 inches (127 mm) stated above; treads are to be at least 10¹/₂ inches (267 mm) in depth [compared to $8^{1/2}$ inches (216 mm)] and risers are not to exceed 8 inches (203 mm) in height [compared to 91/2 inches (341 mm)]. Applying these latter limiting dimensiond would result in a device of lesser incline (approximate slope of 2:1) and a more comfortable and safer device to use for egress travel.

1009.11 Handrails. Stairways shall have handrails on each side. Handrails shall be adequate in strength and attachment in accordance with Section 1607.7. Handrails for ramps, where required by Section 1010.8, shall comply with this section.

Exceptions:

- 1. Aisle stairs complying with Section 1024 provided with a center handrail need not have additional handrails.
- 2. Stairways within dwelling units, spiral stairways and aisle stairs serving seating only on one side are permitted to have a handrail on one side only.
- 3. Decks, patios and walkways that have a single change in elevation where the landing depth on each side of the change of elevation is greater than what is required for a landing do not require handrails.

- 4. In Group R-3 occupancies, a change in elevation consisting of a single riser at an entrance or egress door does not require handrails.
- 5. Changes in room elevations of only one riser within dwelling units and sleeping units in Group R-2 and R-3 occupancies do not require handrails.
- Falls are the leading cause of nonfatal injuries in the United States, exceeding even motor vehicle injuries. To protect the user from falls to surfaces below and to aid in the use of the stairway, guards and handrails are to be provided. In cases of fire where vision might be obscured by smoke, handrails serve as guides directing the user along the path of egress travel.

This section requires that handrails be continuous along, and be placed on both sides of, a stairway so that a mobility-impaired person can support his or her "strong side" in both ascent and descent [see Figures 1009.4(1) and 1009.4(2)].

This section is referenced when handrails are required on ramps. Handrails on ramps must comply with Sections 1009.11 through 1009.11.7.

The exceptions state conditions where handrails are only required on one side or are not needed at all.

1009.11.1 Height. Handrail height, measured above stair tread nosings, or finish surface of ramp slope, shall be uniform, not less than 34 inches (864 mm) and not more than 38 inches (965 mm).

It has been demonstrated that for safe use, the height of handrails must not be less than 34 inches (864 mm) nor more than 38 inches (965 mm) above the leading edge



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January 31,2006

Mike Nugent Inspection Department City Hall Portland, Maine 04101

RE: Valley Street Apartments Gilman Street Portland, Maine

Dear Mike,

Enclosed are responses to the comments in your **email** of Friday, Wednesday, January 20, 2006.

UL and STC Ratings:

- Floor/Ceiling Type 1 (1) Hour ULL528. See page 6 of TPI publication National Design Standard for Metal Plate Connected Wood Truss Constructions enclosed, STC 51.
- Floor/Ceiling Type 2 (2) Hour UL J903. Per PCI Manual for the Design of Hollow Core Slabs, Table 7.4.1, Assembly No. 19, STC 52.
- Floor/Ceiling Type 3 (1) Hour Gypsum Association File No. FC 5120, STC. 50-54.

IECC Compliance: provided at our January 30,2006 meeting.

Statement of Special Inspections: enclosed.

Parking Garage Exhaust Rate: provided at our January 30, 2006 meeting.

Area of Refuge: not required per 1007.3, exception 3.

Alternating Tread Stair: see sketch attached and a letter from the ICC provided by the manufacturer.

Mechanical: Dryer venting, dampers, penetrations – I believe we settled these items **at** our January 30,2006 meeting.

Since John Shields

Architect

Cc: Bill Floyd - Shalom House





TRUSS PLATE INSTITUTE

FOR METAL PLATE CONNECTED WOOD TRUSS CONSTRUCTION

. ...

NATIONAL DESIGN STANDARD

TO ANSI/TPI 1-1995



COMMENTARY & APPENDICES

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Truss Plate Institute

ANSI/TPI 1-1995 Appendix E (Non-Mandatory)

wide strips Nominal 2" wide strip tightly wrapped around **pipe** covering or tube insulation (foil side **exposed**), secured with two steel **tie** wires and **slid** into hole-sawed opening in flooring (Item **16**) and in gyp**sum wallboard** ceiling (Item 1D). Bottom **edge** of wrap strip to project 9/16" to 11/16" below bottom surface df flooring and below bottom (ceiling) surface of gypsum wallboard

Minnesota Mining & Manufacturing Co. - Type FS-195 F/R.

5. FILL, VOID, OR CAVITY MATERIALS - CAULK

Nominal 1/4" thickness of caulk to be applied to the exposed edge of the wrap strip layer (top of flooring and bottom of gypsum wallbaord ceiling). Generous application of caulk to be applied to fill all gaps at the wrap strip/flooring and wrap strip/gypsum wallboard ceiling interface.

Minnesota Mining & Manufacturing *Co.* - Type CP-25 W/B caulk.

E.3A COUSTICAL PERFORMANCE CRITERIA (SOUND/NOISE CONTROL)

E.3.1 GENERAL

Model building **code** requirements and occupant demands for a comfortable living **envi-** ronment are placing increasing emphasis on acoustical performance as a building **design** consideration. Building codes may specify acoustical performance criteria as either noise insulation criteria for the components **used** or noise isolation criteria for **the** complete construction.

Noise insulation criteria specifies the performance **of** ?he components such as floor-ceiling assemblies. This **eases the burden** of **design** since performance testing of **the** completed building *is* not required. Airborne noise insulation is concerned with a structure's ability to attenuate sound incident upon and transmitting through a structure.

E.3.1.1 SOUND TRANSMISSION LOSS TESTS

Sound transmission loss is the quantity used to characterize airborne noise insulation. The sound transmission loss (TL) is a function of frequency. A larger value of TL denotes better noise insulation. One measure of sound transmission loss is the Sound Transmission Class (STC). The STC rating attempts to accomplish two objectives. First, it characterizes the





sound transmission loss data at various frequencies by a single number. Second, it attempts to provide a single number that correlates with an occupants subjective response to intruding noise. The rating is a relative scale based on the idealized TL curve of a 9" thick plastered brick wall that is assumed to provide occupants with an adequate degree of sound insulation. ASTM E413 "Determination of Sound Transmission Class," ASTM E90 "Recommended Method for Laboratory Measurement of Airborne Sound Transmission Loss of Building Partitions" or ASTM E336 "Recommended Method for Measurement of Airborne Sound Insulation in Buildings" are the standard used to determine sound transmission loss. To satisfy building code requirements, the designer will usually have to specify an STC rating above 45.

E.3.1.2 IMPACT NOISE TEST

Another physical measure of noise insulation is impact noise testing. Impact noise is usually generated by footsteps or dropped objects that are transmitted through floor-ceiling assemblies to the room below. The design of

floor-ceiling construction on the basis of impact noise insulation is a distinct consideration in addition to airborne noise insulation requirements (STC), since acceptable airborne noise insulation performance does not imply similar impact noise insulation using a single number classification called the Impact Insulation Class (IIC). The IIC ratings are obtained by fitting a *grading* curve to a plot of 1/3 octave band sound pressure level data. ASTM E492 "Methodfor Laboratory Measurement of impact Sound Transmission Through Floor-Ceiling Assemblies Using the Tapping Machine" is the standard to determine IIC ratings. Building code requirements usually specify an IIC rating above 45.

E.3.2 ASSEMBLY TYPES

E.3.2.1 UL L528 & L529

E.3.2.1.1 FLOOR-CEILING ASSEMBLY

The fire-rated metal plate connected wood truss assembly shall be constructed of the materials and in the manner specified in Design **No. UL 528** (E.1.3.2).

Truss Plate Institute

ANSI/TPI 1-1995 Appendix E (Non-Mandatory)



E.3.2.1.2 RATINGS

STC & IIC ratings for UL L528/L529 are listed in Table E.3.2-1.

E.3.2.2 FC-214

E.3.2.2.1 FLOOR-CEILINGASSEMBLY

The fire-rated metal **plate connected** wood **truss assembly** shalt be **constructed** of the materials and **in the** manner **specified** in **Design** No. FC-214 (E.1.3.4).

E.3.2.2.2 RATINGS STC 8 IIC ratings for FC-214 are **listed** in Table E.3.2-2.



- 59-

Truss Plate Institute

FLOOR COVERING	STC	IIC	TEST NUMBER
Carpet & Pad Vinyl Lightweight, Carpet & Pad Lightweight and Vinyl Gypcrete & Cushioned Vinyl Gypcrete, Carpet & Pad Gypcrete	48 45 57 57 58	56 37 72 70 53 74	NRC 1039 & 1040 NRC 1041 & 1042 NRC 1044 & 1045 NRC 1047 & 1048 6-442-2 Gypcrete 6-442-3 Gypcrete 6-442-5 Gypcrete

FLOOR COVERING	STC	HC	TEST NUMBER
Carpet & Pad	48	54	NRC 1059 & 1060
Vinyl	47	35	NRC 1063 & 1064
Lightweight, Carpet & Pad	56	7 <i>2</i>	NRC 1053& 1054
Lightweight and Vinyl	56	48	NRC 1051& 1052
Gypcrete, Carpet & Pad	52	63	NRC 1076& 1077
Gypcrete	53	43	NRC 1085& 1086

Gypcrete¾"Lightweight Concrete1"Carpet2.63 Kg/M²Pad1.37 Kg/M²

Table E.4-1 SUMMARY TABLE FOR ALL ASSEMBLIES

	FIRE					ACOUSTICS	
ASSEMBLY	SEPARATION		PENETRATION				
ΝΡΕ	ASSEMBLY	FINISH	F	Т	STC*	IIC*	
FC-392 UL-L528/L529 FC-214	1-hr. 1-hr. 1-hr.	25-min. 22-min.	1-hr. 1-hr. 1-hr.	1-hr. 1-hr. 1-hr.	48 48	56 54	
EC 225	45-min. 45-min.						
FC-249	1½-hr.	67-rnin.					

FC-426

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Flooring Applications

STC 51 IIC 75





STC 52 IIC 47



STC 54 IIC 51



STC 5<u>2 IIC 51</u>



440 SoundBarrier[®] Floor-Ceiling Assemblies



(Seepage 3 for an explanation of STC and IIC Ratings)

NAILED 6" O.C

UL L528

2 CALL TOLL FREE 1-800-257-9491 IN NJ 609-883-3300



Lapeyre Stair, Inc.

P.O. BOX 50699 • NEW ORLEANS, LA 70150 • PHONE: 504-733-6009 • FAX 504-733-4393 • TOLL-FREE: 800-535-7631

FAX To John hields From: And Vientle	ni
Fax: Date:	
Phone: Pages:	<u>~</u> .
Project: Nanchard Code Alternating Tread	Stan
Urgent OF For Review O Please Commont O Please Reply O Please Rocycle	
YOUR SALES REPRESENTATIVE IS:	
LINDA ABATE VENTLINEEVELYN FINNEYSHERRY BUI	
SHANNON LEBLANCDICK SATNICK	
COMMENTS:	
Thank You,	
www.lapeyrestair.com	



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MANY P. HOBGE, JR., C.R.D., CENF Biractur of Building and

Fire Cales Hittee Hand Island, South Carolina

BECHEVILLE HIRE

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WALLY BALLEY, C.B.S. Director, Development and Construction

Ft. Smith, Automat

ALA

EDINIEL M. WERKEL G.F.L. EDitor an and Fire Marshal Maddelle Fire Prenaction Clautics

MCX PANNEL JR. C.K.D. Manager, Cammercial Generation Services Fample, Filence

WILLIAM S. DUCK, JR., C.E.B. Chint, haspections and Code Enforcement, Division

Columbat, Gradie

Line Official Chesterficht, Migiela

WILLIAM R. BUTLEN

GERALO D. SEDIIGE, C.B.O. (Diel Daliday Official Sankin; Coloredy

CHETHY M. SAMUS Dipity Spiritery of State Albudy, New York

FRED HERLAN Chief Suideog Official Pale Alla, Culturale

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 Official Phasix City, Alabama

JANES T. HYAN, C.R.O Gaulies Ad Southed Part, Kanag STEVEN I. PLAPMU. C.K.B. Girattor of Dadas Compliand

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Los Cruche, New Marbo CHIMP EXECUTIVE OFFICER JAMES LEC WITT

Fire Chief

. IL "BUERAT REALENT'S, C.H.Q.

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TERMENCE L. COM. C.S.S. Diractor, Days, of Codes Administration

alities Granty, To

PRESIDENT

Marian Urak

MAR PRIME

Setting the Standard for Building Safety" -

Chicago District Office 4051 W. Plossenoor Read = Country Chub Hills, IL 60478-5795 U.S.A. Tel; +1 (708) 799-2300 = Fax: +1 (708) 799-4981

www.inconfo.org

July 23,2004

Stephen J. Wilczynski, AlA Fanning/Howey Associates, Inc. P.O. Box 71 540 East Market Street Celling, OH 45822

RE: Sections 1003.3.3.10.1 and 1003.3.3.11 of the 2000 International Building Code

Dear Mr. Wilczynski:

This latter is in response to your request for a written code interpretation regarding alternating mead devices used for mechanical access. Your letter states that the mechanical area is permitted to be served by a ladder but in the interest of safety and convenience, a customized alternating tread device is proposed. You ask if it is necessary for alternating tread devices to comply with handrail height and handrail extension requirements.

The code oriteria for alternating tread devices includes a blanket reference to Section 1003.3.3.11 (Handrails), which includes requirements for handrail height and handrail extensions applicable to normal atains and ramps. Alternating tread devices are configured to suit specific locations. As an alternating tread device becomes steeper, standard handrail height and extension requirements become less sensible. An alternating tread device of a given slope and configuration likely has an ideal handrail height that may be inconsistent with code criteria. Furthermore, extensions on handrails at the bottom of the steeper designs appear to serve little purpose. In the case of alternate components, such as alternating tread devices, it is more important to satisfy the intent of code requirements than to satisfy those literal requirements that do not advance such Intent.

Lastly, it is not the intent of the code to disallow the substitution of an alternate component (i.e., atternating tread device) judged to be safer than the minimum prescribed component (i.e., ladder) based on a technicality of the code when the safety of the alternate component is not adversely affected.

We are pleased to provide you with the opinions stated herein. They are based solely on information that you have provided. We have made no independent effort to verify the accuracy of this information nor have we conducted a review beyond the scope of your question. Understand that the final interpretation is always the legal responsibility of the authority having jurisdiction. As such, a review of these issues with the building official is recommended.

Hahn. h

Senior Staff Architect

Hendquarters: 5203 Locsborg Pike, Solit 600 . Fails Church, VA 22041-3405 U.S.A. Tel: +1 (703) 931-4513 = Fex: +1 (703) 379-1546

Received 08-04-2004 09:49am

From-418 586 2141

To-LAPEYRE STAIR INC.

TOTAL P.01

Page 001



PRECAST

PRECAST/PRESTRESSED CONCRETE INSTITUTE

207-934-8039

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■ CHAPTER 7

ACOUSTICAL PROPERTIES OF HOLLOW CORE FLOOR SLABS

71 Glossary

Airborne Sound - sound that reaches **the** point of interest by propagation through air.

Background Level - the ambient sound pressure level existing in a space.

Decibel (dB) - a logarithmic unit of measure of sound pressure or sound power. Zero on the decibel **scale** corresponds to **a** standardized references pressure ($20 \mu Pa$) or sound power (10^{-12} watt).

Flanking Transmission - transmission of sound by indirect paths other than through the primary barner.

Frequency (Hz) - the number of complete vibration cycles per second.

Impact Insulation Class (IIC) - a single figure rating of the overall impact sound insulation merits of floor-ceiling assemblies in terms of a reference contour (ASTM E989).

Impact Noise - the sound produced by one object striking another.

Noise - unwanted sound.

Noise Criteria (NC) - a series of curves, used as design goals to specify satisfactory background sound levels as they relate to particular use functions.

Noise Reduction (NR) • the difference in decibels between the space-time average sound pressure levels produced in two enclosed spaces by one or more sound **sources** in one of them.

Noise Reduction Coefficient (NRC) the arithmetic average *cf the sound absorption* coefficients at 250,500,1000 and 2000 Hz expressed to the nearest multiple of 0.05 (ASTM C423).

Reverberation - the persistence \mathbf{c} sound in **an** enclosed or partially enclosed space after the source of sound has stopped.

Room Criteria (RC) Curves - a revision of the NC curves based on empirical studies of background sounds.

Sabin - the unit of measure of sound absorption (ASTM C423).

Sound Absorption Coefficient (α) - the fraction of randomly incident sound energy absorbed or otherwise not reflected off a surface (ASTM C423).

Sound Pressure Level (SPL)- ten times the common logarithm of the ratio of the square d the **sound** pressure to the square of the standard reference pressure of 20 μ Pa. Commonly measured with a sound level meter and microphone, this quantity is expressed in decibels.

Sound Transmission Class (STC) - the single number rating system used to give a preliininary estimate of the sound insulation properties of a partition system. This rating is derived from measured values of transmission loss (ASTME413).

Sound Transmission Loss (TL) - ten times the common logarithm of the ratio, expressed in decibels, of the airborne sound power incident an the partition that is transmitted **by** the partition and radiated on the other side (ASTM E90).

Structureborne Sound - **sound** that **reaches** the point **of interest over at** least part of its path by vibration of a solid structure.

7.2 General

The **basic** purpose of architectural acoustics is to provide a satisfactory environment in which desired sounds are ctearly heard by the intended listeners and unwanted sounds (noise) **are** isolated or absorbed.

Under most conditions, the architect/ engineer can determine the acoustical needs of the space and then design the building to satisfy those needs. Good acoustical design utilizes both absorptive and reflective surfaces, sound barriers

p.2

and vibration isolators. Some surfaces must reflect sound so that the loudness will **be** adequate in all areas where listeners are located. Other surfaces absorb sound to avoid echoes, sound **distor**tion and long reverberation times. Sound is isolated from rooms where it is not wanted by selected wall and floor-ceiling constructions. Vibration generated by mechanical equipment must be isolated from the structural frame of the building.

Most acoustical situations can be described in terms of: (1) sound source, (2) sound transmission path, and (3) sound receiver. Sometimes the source strength and path can be controlled and the receiver made more attentive **by** removing distraction or made more tolerant of disturbance. Acoustical design must include consideration of these three elements.

7.3 Approaching the Design Process

Criteria must be established before the acoustical design of a building can begin. Basically a satisfactory acoustical environment is one in which the character and magnitude of all sounds **arc** compatible with the intended space function.

Although a reasonable objective. it is not always easy to express these intentions in quantitative terms. In addition to the amplitude of sound, the properties such as spectral characteristics, continuity, reverberation and intelligibility must be specified.

People are highly adaptable to the sensations of heat, light, odor, sound, etc. with sensitivities varying widely. The human ex can detect a sound intensity of rustling leaves, 10dB, and can tolerate, if even briefly, **the** powerful exhaust of a jet engine at 120dB, 10¹² times the intensity of the rustling sound.

7.3.1 Dealing with Sound Levels

The problems of sound insulation are usually considerably more complicated than those *af* sound absorption. The former involves reductions of sound level, which are of the greater orders of magnitude than can be achieved by absorption. These reductions of sound level from space to space can be achieved **only** by continuous, impervious barriers. If the problem also involves structure borne sound, it may be necessary tu introduce resilient layers or discontinuities into the barrier.

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Sound absorbing inaterials and sound insulating materials are used for different purposes. There is not much sound absorption from an 8 in (200 mm) hollow core concrete slab; similarly, high sound insulation *is* **not** available from a porous lightweight material that may be applied to room surfaces. It is important to recognize that the basic mechanisms of sound absorption and sound insulation are quite different.

7.4 Sound Transmission Loss

Sound transmission loss measurements are made at I6 frequencies at one-third octave intervals covering the range from 125 to 4000 Hz. The testing procedure is ASTM Specification E90, Laboratory Measurement of Airborne Sound Transmission Loss of Building Partitions. To simplify specification of desired performance characteristics, the single number Sound Transmission Class (STC) was developed.

Airborne sound reaching a floor or ceiling produces vibration in the slab **and** is radiated with reduced intensity on the other side. Airborne sound transmission loss of a floor-ceiling assembly is a function of its weight, stiffness and vibration damping characteristics.

Weight is concrete's greatest asset when it is used as a sound insulator. For sections of similar design, but different weights, the STC increases approximately 6 units Cr each doubling of weight **as** shown in Figure 7.4.1.

Fig. 7.4.1 Sound Transmission Class as a function of weight of floor





Fig. 7.4.2 Acoustical test data of hollow core slabs (normal weight concrete)

Precast concrete floors aid **roofs usually do not** need additional treatments **in** order to **provide** adequate sound insulation. If desired, greater sound **insulation** can **be obtained** by using **a** resiliently attached layer(s) of gypsum board or other building matcnal. The increased transmission loss *oc*curs because the energy flow path is now increased to include a dissipative air column and additional mass.

The acoustical test results of both airborne sound transmission loss and impact insulation of 6 and 8 in (150 and 200 mm) hollow core slabs are shown in Figure 7.4.2. Table 7.4.1 presents the latings for various floor-ceiling assemblies.

7.5 Impact Noise Reduction

Footsteps, dragged chairs, dropped objects. slammed doors, and plumbing generate impact noise. Even when airborne sounds are adequately controlled there can be severe impact noise problemls.

The test method used *to* evaluate systems for impact sound insulation is described in ASTM Specification E492, Laboratory Measurement of Impact Sound Transmission Using the Tapping Machine. As with the airborne standard, measurements are made at 16 one-third octave intervals but in the range from 100 to 3150 Hz. For performance specification purposes, the single number Impact Insulation Class (IIC) is used.

Liollow cure **Elccrs** in combination with resilient inaterials effectively control impact sound. One simple solution *consists* of good carpeting on resilient padding. Table 7.4.1 shows that **a** carpet and pad over a **bare slab will significantly increase** the impact noise reduction. The overall efficiency varies according to the characteristics of the carpeting and padding such as resilience. thickness and weight. So called resilient flooring materials, such as linoleum, rubber. asphalt vinyl, etc. are not entirely satisfactory directly on concrete, nor are parquet or strip wood floors when applied directly. Impact sound also may be controlled by

Assembly			
NO.	Description	STC	IIC
1.	6 in (150 mm) hollow core slabs	4 8	23
2.	Assembly 1 with carpet and pad	48	69
3.	Assembly 1 with $\frac{1}{2}$ in (13 mm) wood block flooring adhered directly	48	48
4.	Assembly I with $\frac{1}{2}$ in (13 mm) wood block flooring adhered to $\frac{1}{2}$ in (13 mm)		40
F .	sound-deadening board underlayment adhered to concrete	49	49
J.	<u>Assembly 1</u> with $\frac{1}{4}$ in (19 mm) gypsum concrete	50	41
6.	Assembly I with $\frac{3}{4}$ in (19 mm) gypsum concrete on $\frac{1}{2}$ in (13 mm) sound-	50	50
7	deadening board underlayment adhered to concrete Assembly, I with sympt and an $\frac{1}{2}$ in (10 mm) symptometry on every	50	50
7.	<u>Assembly 1</u> with carpet and pad on 7_4 in (19 fitti) gypsum concrete on $\frac{1}{2}$ in (13 mm) sound deadening board underlowment adhered to concrete	50	72
-	⁷ / ₂ in (15 min) sound-deadening board undertoyment adhered to concrete		
8.	8 in (200 mm) hollow core slabs	50	28
9.	Assernbly 8 with carpet and pad	50	73
10.	Assembly 8 with $\frac{1}{2}$ in (1 3 mm) wood block flooring adhered directly	51	47
11.	Assembly 8 with $\frac{1}{2}$ in (13 mm) wood block flooring adhered to $\frac{1}{2}$ in (13 mm)	50	- 4
40	sound-deadening board underlayment adhered to concrete	52	54
12.	<u>Assembly δ with $\frac{1}{2}$ in (1.5 mm) wood block flooring adhered to $\frac{1}{2}$ in (1.5 mm)</u>		
	adhered to concrete	52	55
13	Assembly 8 with $\frac{5}{4}$ in (8 mm) wood block flooring adhered to $\frac{1}{4}$ in (6 mm)		
	polystyrene underlayment adhered to concrete	50	51
14.	Assembly 8 with vinyl tile adhered to $\frac{1}{2}$ in (13 mm) plywood adhered to		
	\mathcal{V}_{16} in (I 1 mm) sound-deadening board underlayment adhered to concrete	50	55
15.	Assembly 8 with vinyl tile adhered to $\frac{1}{4}$ in (6 tnm) inorganic felt supported		
	cushion underlayment adhered to concrete	50	51
16.	Assembly 8 with vinyl tile adhered to $\frac{1}{8}$ in (3 mm) polyethylene foam under-	-0	
	layment adhered to concrete	50	58
17.	<u>Assembly 8</u> with $1 \frac{1}{2}$ in (38 mm) concrete topping with carpet and pad	50	76
18.	Assembly 8 with $1 V_2$ in (38 mm) concrete topping with vinyl tile adhered to	50	
10	concrete (28 mm)	50	44
19.	<u>Assembly 6</u> with 1 $\frac{1}{2}$ in (38 mm) concrete topping with vinyl the adhered to $\frac{3}{2}$ in (9 mm) plywood adhered to $\frac{1}{2}$ in (13 mm) sound deadening board		
	adhered to concrete	52	55
20.	Assembly 8 with $1\frac{1}{2}$ in (38mm) concrete with $\frac{1}{2}$ in (13mm) wood block		
	flooring adhered to $\frac{1}{2}$ in (13 mm) sound-deadening board adhered to concrete	51	53
21.	Assembly 8 with $1\frac{1}{2}$ in (38 inm) concrete with $\frac{5}{16}$ in (8 mm) wood block		
	flooring adhered to foam backing adhered to concrete	51	54
22.	Assembly 8 with $\frac{3}{4}$ in (19 mm) gypsum concrete with $\frac{5}{16}$ in (8 rnm) wood		
	block flooring adhered to foam backing adhered to concrete	50	53
23.	Assembly 11 with acoustical ceiling	59	61
24.	<u>Assembly</u> 3 with quarry tile, $1 \frac{1}{4}$ in (32 mm) reinforced mortar bed with		
	3.4 in (10 mm) nylon and carbon black spinerette matting	60	54
25.	Assembly 24 with suspended $\frac{1}{8}$ in (16 mm) gypsum board ceiling with $\frac{31}{10}$ in (90 mm) insulation	61	62
		01	04

Table 7.4.1	Airborne sound transmission arid impact insulation class ratings from laborator	ry
	tests of hollow core slab floor-ceiling assemblies	

providing a discontinuity in the structure such as would be obtained by adding a resilient-mounted plaster or drywall suspended ceiling.

7.6 Absorption of Sound

A sound wave always loses part of its energy as it is reflected by a **surface.** This **loss** of energy is termed sound absorption. It appears as a decrease in sound pressure of the reflected wave. The sound absorption coefficient is the fraction of energy incident but not reflected per unit of surface area. Sound absorption can be specified **at** individual frequencies or as an average of absorption coefficients (NRC).

A dense, non-porous concrete surface typically absorbs 1 to 2% of incident sound arid has an NCR of 0.015. In the case where additional sound absorption of precast concrete is desired, a coating of acoustical material can be spray applied, acoustical tile can be applied with adhesive, or an acoustical ceiling can be suspended. Most of the spray applied fire retardant materials used to increase the fire! resistance of precast concrete and other floor-ceiling systems can also be used to absorb sound. The NCR of the sprayed fiber types range from 0.25 to 0.75. Most cementitious types have an NCR from 0.25 to 0.50.

If an acoustical ceiling were added to Assembly 11 of Table 7.4.1 (as in Assembly 23), the sound entry through a floor or roof would be reduced 7dB. In addition, the acoustical ceiling would absorb a portion of the sound after entry and provide a few more decibels of quieting. Use of the following expression can be made to determine the intra-room noise or loudness reduction due to the absorption of sound.

NR =
$$10 \log \frac{A_o + A_a}{A_a}$$
 (Eq. 7.6.1)

where

NK = sound pressure level reduction, dB

A, = original absorption, Sabins

A, = added absorption. Sabins

Values for **A**, and A, are **the** products of the **ab**sorption coefficients of the various room materials and their surface areas.

A plot of this equation is shown in Figure 7.6.1. For an absorption ratio of 5, the decibel reduction is 7dB. Note that the decibel reduction is the same, regardless of the original sound pressure

level and depends only on the absorption ratio. This is due to the fact that **the** decibel scale is itself a scale of ratios, rather than difference in sound energy.

While **a** decibel difference is an engineering quantity which can **bc** physically measured, it is also important to know how the ear judges the change in sound energy due to sound conditioning. Apart from the subjective annoyance factors associated with excessive sound reflection, the ear **can make** accuratejudgments of the relative loudness between sounds, An approximate relation between percentage loudness, reduction of reflected sound and absorption ratio *is* plotted in Figure 7.6.2

The percentage loudness reduction does not depend on the original loudness, but only on the absorption ratio. (The curve is drawn for loudness within the normal range of hearing and does not apply to extremely faint sounds.) Referring again to the absorption ratio of **5**, the loudness reduction is **read from** Figure 7.6.2 **as** approximately 40 percent.

7.7 Acceptable Noise Criteria As a rule, a certain amount of continuous sound

can be tolerated before it becomes noise. An "acceptable" level neither disturbs room occupants nor interferes with the communication of wanted sound.

The most widely accepted and used noise crite-

ria today are expressed as the Noise Criterion (NC) curves, Figure 7.7.1a. The figures in Table 7.7.1 represent general acoustical goals. They can also be compared with anticipated noise levels in specific rooms to assist in evaluating noise reduction problems.

The main criticism of NC curves is that they are too permissive when **the** control of low or high frequency noise is of concern. For this reason, **Room** Criterion (**RC**) Curves were developed (Figure 7.7.1b).^{39,40} RC curves are the result of extensive studies **based** on the human response to both sound **pressure** level **and frequency** and take into account the requirements for speech intelligibility.

A low background level obviously is necessary where listening and speech intelligibility is im-