

DISPLAY THIS CARD ON PRINCIPAL FRONTAGE OF WORK



CITY OF PORTLAND BUILDING PERMIT

This is to certify that UNIVERSITY OF MAINE

Located At 246 DEERING AVE

Job ID: 2012-04-3828-CH OF USE

CBL: 051- E-001-001

has permission to Modify & upgrade existing rooftop wireless communication system & equipment, addition of 3 new antenna provided that the person or persons, firm or corporation accepting this permit shall comply with all of the provisions of the Statues of Maine and of the Ordinances of the City of Portland regulating the construction, maintenance and use of the buildings and structures, and of the application on file in the department.

Notification of inspection and written permission procured before this building or part thereof is lathed or otherwise closed-in. 48 HOUR NOTICE IS REQUIRED.

A final inspection must be completed by owner before this building or part thereof is occupied. If a certificate of occupancy is required, it must be

Fire Prevention Officer

 
Code Enforcement Officer / Plan Reviewer

**THIS CARD MUST BE POSTED ON THE STREET SIDE OF THE PROPERTY
PENALTY FOR REMOVING THIS CARD**

City of Portland, Maine - Building or Use Permit Application

389 Congress Street, 04101 Tel: (207) 874-8703, FAX: (207) 8716

Job No: 2012-04-3828-CH OF USE	Date Applied: 4/23/2012	CBL: 051- E-001-001	
Location of Construction: 246 DEERING AVE	Owner Name: UNIVERSITY OF MAINE	Owner Address: 107 MAINE AVE BANGOR, ME 04401	Phone:
Business Name: Law School Building	Contractor Name: Nexlink Global Services	Contractor Address: 800 Marshall Phelps Rd, Windsor Ct 06095	Phone: 860-640-4834 978-399-8600
Lessee/Buyer's Name:	Phone:	Permit Type: BLDG ALT	Zone: USM Overlay/R-5
Past Use: University Law School	Proposed Use: Same: University Law School -To modify and upgrade the existing wireless communication sit with 3 addition antenna & associated equipment	Cost of Work: \$20,000.00	CEO District:
		Fire Dept: 5/15/12 <input checked="" type="checkbox"/> Approved <input type="checkbox"/> Denied <input type="checkbox"/> N/A Signature: <i>[Signature]</i> (58)	Inspection: Use Group: B/U Type: N/A IBC-2009 Signature: <i>[Signature]</i>
Proposed Project Description: modification & upgrade of existing wireless commun		Pedestrian Activities District (P.A.D.) 5/16/12	
Permit Taken By: Gayle		Zoning Approval	

<p>1. This permit application does not preclude the Applicant(s) from meeting applicable State and Federal Rules.</p> <p>2. Building Permits do not include plumbing, septic or electrical work.</p> <p>3. Building permits are void if work is not started within six (6) months of the date of issuance. False informatin may invalidate a building permit and stop all work.</p>	Special Zone or Reviews <input type="checkbox"/> Shoreland <input type="checkbox"/> Wetlands <input type="checkbox"/> Flood Zone <input type="checkbox"/> Subdivision <input type="checkbox"/> Site Plan <input type="checkbox"/> Maj <input type="checkbox"/> Min <input type="checkbox"/> MM Date: OK 4/24/12	Zoning Appeal <input type="checkbox"/> Variance <input type="checkbox"/> Miscellaneous <input type="checkbox"/> Conditional Use <input type="checkbox"/> Interpretation <input type="checkbox"/> Approved <input type="checkbox"/> Denied Date:	Historic Preservation <input checked="" type="checkbox"/> Not in Dist or Landmark <input type="checkbox"/> Does not Require Review <input type="checkbox"/> Requires Review <input type="checkbox"/> Approved <input type="checkbox"/> Approved w/Conditions <input type="checkbox"/> Denied Date:
	CERTIFICATION		

I hereby certify that I am the owner of record of the named property, or that the proposed work is authorized by the owner of record and that I have been authorized by the owner to make this application as his authorized agent and I agree to conform to all applicable laws of this jurisdiction. In addition, if a permit for work described in the application is issued, I certify that the code official's authorized representative shall have the authority to enter all areas covered by such permit at any reasonable hour to enforce the provision of the code(s) applicable to such permit.

SIGNATURE OF APPLICANT	ADDRESS	DATE	PHONE
RESPONSIBLE PERSON IN CHARGE OF WORK, TITLE		DATE	PHONE

BUILDING PERMIT INSPECTION PROCEDURES

Please call 874-8703 or 874-8693 (ONLY)

or email: buildinginspections@portlandmaine.gov

With the issuance of this permit, the owner, builder or their designee is required to provide adequate notice to the city of Portland Inspections Services for the following inspections. Appointments must be requested 48 to 72 hours in advance of the required inspection. The inspection date will need to be confirmed by this office.

- **Please read the conditions of approval that is attached to this permit!! Contact this office if you have any questions.**
- **Permits expire in 6 months. If the project is not started or ceases for 6 months.**
- **If the inspection requirements are not followed as stated below additional fees may be incurred due to the issuance of a "Stop Work Order" and subsequent release to continue.**

Electrical Inspection prior to covering

Final Inspection

The project cannot move to the next phase prior to the required inspection and approval to continue, REGARDLESS OF THE NOTICE OF CIRCUMSTANCES.

IF THE PERMIT REQUIRES A CERTIFICATE OF OCCUPANCY, IT MUST BE PAID FOR AND ISSUED TO THE OWNER OR DESIGNEE BEFORE THE SPACE MAY BE OCCUPIED.



PORTLAND MAINE

Strengthening a Remarkable City, Building a Community for Life • www.portlandmaine.gov

Acting Director of Planning and Urban Development
Gregory Mitchell

Job ID: 2012-04-3828-CH OF USE

Located At: 246 DEERING AVE

CBL: 051- E-001-001

Conditions of Approval:

Building

1. Application approval based upon information provided by applicant. Any deviation from approved plans requires separate review and approval prior to work.
2. Separate permits are required for any electrical, plumbing, sprinkler, fire alarm, HVAC systems, heating appliances, including pellet/wood stoves, commercial hood exhaust systems and fuel tanks. Separate plans may need to be submitted for approval as a part of this process.

2012 04 30 26

66



General Building Permit Application

If you or the property owner owes real estate or personal property taxes or user charges on any property within the City, payment arrangements must be made before permits of any kind are accepted.

USM overlay
R-5

Location/Address of Construction: <u>246 DEERING AVENUE (232)</u>					
Total Square Footage of Proposed Structure/Area <u>N/A</u>		Square Footage of Lot		Number of Stories	
Tax Assessor's Chart, Block & Lot Chart# <u>51</u> Block# <u>E</u> Lot# <u>1</u>		Applicant *must be owner, Lessee or Buyer* Name <u>ATT MOBILITY</u> Address <u>60 NEXLINK GLOBAL SERVICES</u> <u>800 MARSHALL PHELPS RD</u> City, State & Zip <u>WINDSOR CT 06095</u>		Telephone: <u>PETER COOKE</u> <u>978-399-8600</u>	
Lessee/DBA (If Applicable) <u>ATT MOBILITY RECEIVED</u> <u>APR 23 2012</u>		Owner (if different from Applicant) Name <u>UNIVERSITY OF MAINE</u> Address <u>107 MAINE AVE</u> City, State & Zip <u>BANGOR ME</u>		Cost Of Work: \$ <u>20000</u> C of O Fee: \$ _____ Total Fee: \$ <u>220</u>	
Dept. of Building Inspections City of Portland, Maine Current legal use (i.e. single family) <u>WIRELESS COMMUNICATIONS</u>			THIS IS NOT A CHANGE OF USE		
If vacant, what was the previous use? <u>N/A</u>		Number of Residential Units _____			
Proposed Specific use: <u>WIRELESS COMMUNICATIONS</u>		<u>Category put it in wrong</u>			
Is property part of a subdivision? <u>NO</u>		If yes, please name _____			
Project description: <u>MODIFICATION AND UPGRADE OF EXISTING WIRELESS COMMUNICATIONS SITE TO INCLUDE 3 ADDITIONAL ANTENNAE AND ASSOCIATED EQUIPMENT</u>					
Contractor's name: <u>NEXLINK GLOBAL SERVICES</u>					
Address: <u>800 MARSHALL PHELPS RD</u>				Telephone: <u>860-640-4834</u>	
City, State & Zip: <u>WINDSOR CT 06095</u>				Telephone: <u>978-399-8600</u>	
Who should we contact when the permit is ready: <u>PETER COOKE</u>				Telephone: _____	
Mailing address: <u>POB 894 WOLFEBORO NH 03894</u>					

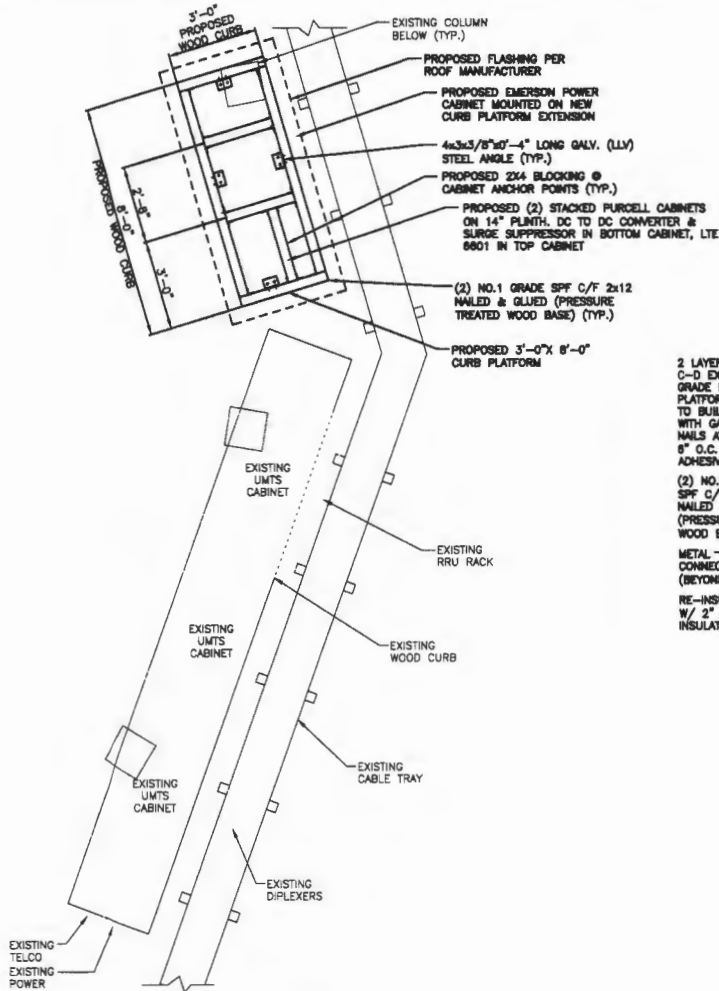
Please submit all of the information outlined on the applicable Checklist. Failure to do so will result in the automatic denial of your permit.

In order to be sure the City fully understands the full scope of the project, the Planning and Development Department may request additional information prior to the issuance of a permit. For further information or to download copies of this form and other applications visit the Inspections Division on-line at www.portlandmaine.gov, or stop by the Inspections Division office, room 315 City Hall or call 874-8703.

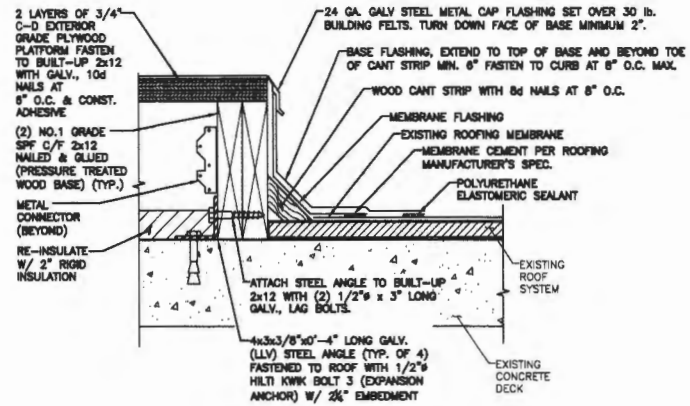
I hereby certify that I am the Owner of record of the named property, or that the owner of record authorizes the proposed work and that I have been authorized by the owner to make this application as his/her authorized agent. I agree to conform to all applicable laws of this jurisdiction. In addition, if a permit for work described in this application is issued, I certify that the Code Official's authorized representative shall have the authority to enter all areas covered by this permit at any reasonable hour to enforce the provisions of the codes applicable to this permit.

Signature: <u>[Signature]</u> <u>AGEN - FOR APPLICANT</u>	Date: <u>4/24/12</u>
-----------------------------------------------------------	----------------------

This is not a permit; you may not commence ANY work until the permit is issued



EQUIPMENT PLAN
SCALE: 1/2"=1'-0"



DETAIL @ WOOD CURB
SCALE: N.T.S.

NOTE:
REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA SETTINGS.

NOTE:
AN ANALYSIS FOR THE CAPACITY OF THE EXISTING STRUCTURES TO SUPPORT THE PROPOSED EQUIPMENT SHALL BE DETERMINED PRIOR TO CONSTRUCTION. REFER TO STRUCTURAL ANALYSIS BY: HUDSON DESIGN GROUP LLC, DATED: MARCH 08, 2012.

NOTES:
1. SUBCONTRACTOR SHALL LEVEL CURB AS NEEDED.
2. SUBCONTRACTOR SHALL COORDINATE ROOFING WORK WITH BUILDING VENDOR SO NOT TO VOID ROOF WARRANTY.
3. SUBCONTRACTOR TO FASTEN EQUIPMENT TO P.T. WOOD CURB PER MANUFACTURER'S SPECIFICATION.

Hudson
Design Group, Inc.
140 OROONOK STREET
BANGOR, ME 04401, 6889 3-101
N. ANDOVER, MA 01845
TEL: (778) 887-6500
FAX: (778) 756-6886

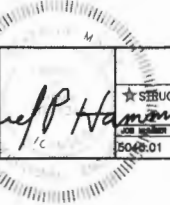
NEXLINK
GLOBAL SERVICES
a Uniftek GLOBAL SERVICES company
800 MARSHALL PHELPS ROAD UNIT: 2A
WINDSOR, CT 06095

SITE NUMBER: ME5045
SITE NAME: PORTLAND USM
246 DEERING AVENUE
PORTLAND, ME 03082
CUMBERLAND COUNTY

at&t
550 COCHITUATE ROAD
FRAMINGHAM, MA 01701

NO.	DATE	REVISIONS	BY	CHKD	APP'D
2	03/20/12	ISSUED FOR CONSTRUCTION	RP	HC	DC/DRH
1	02/23/12	ISSUED FOR PERMITTING	RP	RP	DRH
0	02/14/12	ISSUED FOR REVIEW	RP	RP	DRH

SCALE: AS SHOWN DESIGNED BY: RP DRAWN BY: RP



AT&T

★ STRUCTURAL DETAILS & MODIFICATION PLAN (LTE)

JOB NUMBER	DRAWING NUMBER	REV
5045.01	S-1	2



PORTLAND MAINE

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Receipts Details:

Tender Information: Check , BusinessName: Nexlink Global Services, Inc., Check Number: 6529

Tender Amount: 220.00

Receipt Header:

Cashier Id: gguertin

Receipt Date: 4/23/2012

Receipt Number: 43147

Receipt Details:

Referance ID:	6216	Fee Type:	BP-Constr
Receipt Number:	0	Payment Date:	
Transaction Amount:	220.00	Charge Amount:	220.00
Job ID: Job ID: 2012-04-3828-CH OF USE - modification & upgrade of existing wireless commun			
Additional Comments: 246 Deering Ave			

Thank You for your Payment!

STRUCTURAL ANALYSIS REPORT

For

ME 5045 (LTE)
PORTLAND USM
246 Deering Avenue
Portland, ME 03082

**Equipment Curb on the Roof; Antennas Mounted on the Building
Façade**



Prepared for:



at&t

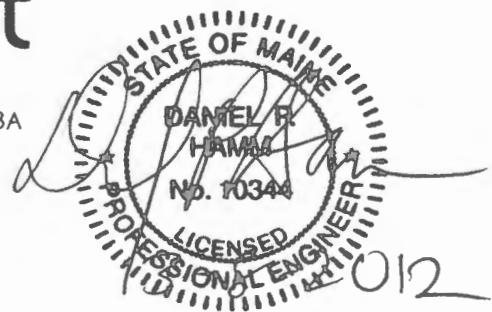
500 Enterprise Drive, Suite 3A
Rock Hill, CT 06067

Dated:

March 8, 2012

Prepared by:

HUDSON DESIGN GROUP, LLC.
1600 Osgood Street Building 20 North, Suite 2-101
North Andover, MA 01845
Phone: (978) 557-5553
www.hudsondesigngroupllc.com





SCOPE OF WORK:

Hudson Design Group LLC (HDG) has been authorized by AT&T to conduct a structural evaluation of the structure supporting the proposed AT&T equipment located in the areas depicted in the latest HDG's construction drawings.

This report represents this office's findings, conclusions and recommendations' pertaining to the support of AT&T's proposed LTE Equipment.

This office conducted an on-site visual survey of the above areas on March 6, 2012. Attendees included Sergio Anastacio (HDG-Assistant Project Manager).

CONCLUSION SUMMARY:

As-built plans prepared by Donald L. Dimick were available for our use. The previous stamped drawings and design calculations prepared by Areal Spectrum, were available for our reference.

A limited visual survey of the structure was completed in or near the areas of the Proposed Work. Based on our evaluation, we have determined that, in general, structural designs to support the proposed AT&T Equipment within or near the Proposed Location can be completed and components installed with **NO STRUCTURAL UPGRADES REQUIRED** to the existing structure.

HDG recommends supporting the new LTE Equipment on a curb platform extension. The new extension is recommended to be installed directly over the building columns to adequately support the new loading. Reference the latest HDG's construction drawings for details.

A summary of the proposed support types and attachment locations are as follows:

(1) LTE Antenna (SBNH-1D6565C) (96.4"x11.9"x7.1" – Wt. 61lbs.) (Alpha Sector)...Mounted on a new steel pipe and mounting brackets, secured by the building facade.

(2) LTE Antennas (KMW AM-X-CD-16-65-00T) (72"x11.8"x5.9" - Wt. 48.5lbs.) (Beta and Gamma Sectors)....Mounted on new steel pipes supported by the existing antenna mounts.

(1) Emerson Outdoor Power Cabinet (Wt.=2150 lbs)...Supported by the new equipment curb extension.

(2) Purcell Cabinets (Wt. = 250 lbs/each).....Supported by the new equipment curb extension.

(3) Surge Arrestor DC2-48-60-0-9E (1 per sector)...Mounted on new unistrut components.

(6) RRH (2 per sector) (Wt. = 50 lbs/each).....Mounted on new unistrut components. Referenced documents are attached.



Referenced documents are attached.

DESIGN CRITERIA:

1. International Building Code 2009, ASCE 7-10 Minimum Design Loads for Buildings and Other Structures.

Wind Analysis:

Reference Wind Speed:	110 MPH	(FIG 26.5-1C; ASCE 7-10)
Category:	C	(26.7.3; ASCE 7-10)
Gust Effect Factor (G):	0.85	(26.9.1; ASCE 7-10)
Force Coefficient (Cf):	Varies	(FIG 29.5-1 thru 29.5-3; ASCE 7-10)
$F = qz * G * Cf * Af:$		(Equation 29.5-1; ASCE 7-10)

Snow Loading:

Ground Snow Load (Pg):	60 psf	(FIG 7-1; ASCE 7-10)
Flat Roof Snow Load (Pf):	37.8 psf	

$$Pf = 0.7 * Ce * Ct * I * Pg \quad \text{(Equation 7.3-1; ASCE 7-10)}$$

$$Ce=0.9; Ct=1.0; I=1.0$$

2. EIA/TIA -222- G Structural Standards for Steel Antenna Towers and Antenna Supporting Structures

County:	Cumberland
Wind Load:	100 mph

3. Approximate height above grade to antennas:

85'-2" +/- (Beta and Gamma sectors)
88'-8" +/- (Alpha sector)



EXISTING ROOF CONSTRUCTION:

The roof construction appears to consist of an adhered roofing membrane on top of a reinforced concrete slab supported by reinforced concrete columns and bearing walls.

Antenna SUPPORT RECOMMENDATIONS:

- The new LTE Alpha sector antenna is proposed to be supported by a new steel pipe and mounting brackets, secured to the building facade.
- The new LTE Beta and Gamma sector antennas are proposed to be supported by new steel pipes, secured to the existing antenna support angles.

RRH's / Surge Arrestor SUPPORT RECOMMENDATIONS:

- The new Alpha sector Surge Arrestor and RRH's are proposed to be mounted on new unistrut components, secured to the building using epoxy anchors.
- The new Beta and Gamma sector Surge Arrestors and RRH's proposed to be mounted on new unistrut components, secured to the existing antenna support angles.

EQUIPMENT SUPPORT RECOMMENDATIONS:

HDG recommends that the proposed equipment be supported by the new equipment rooftop curb extension as shown in the latest HDG construction drawings.

OTHER RECOMMENDATIONS:

HDG recommends that the new curb extension be installed directly over the building columns to adequately support the new equipment load. (Contractor to verify the column locations).



Notes:

1. Reference the latest HDG construction drawings for all the equipment locations.
2. All detail requirements will be designed and furnished in the construction drawings.
3. Mount all equipment per manufacturer's specifications.
4. HDG is under the assumption that the equipment curb was located over building columns.
5. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.

EXISTING ANTENNAS:

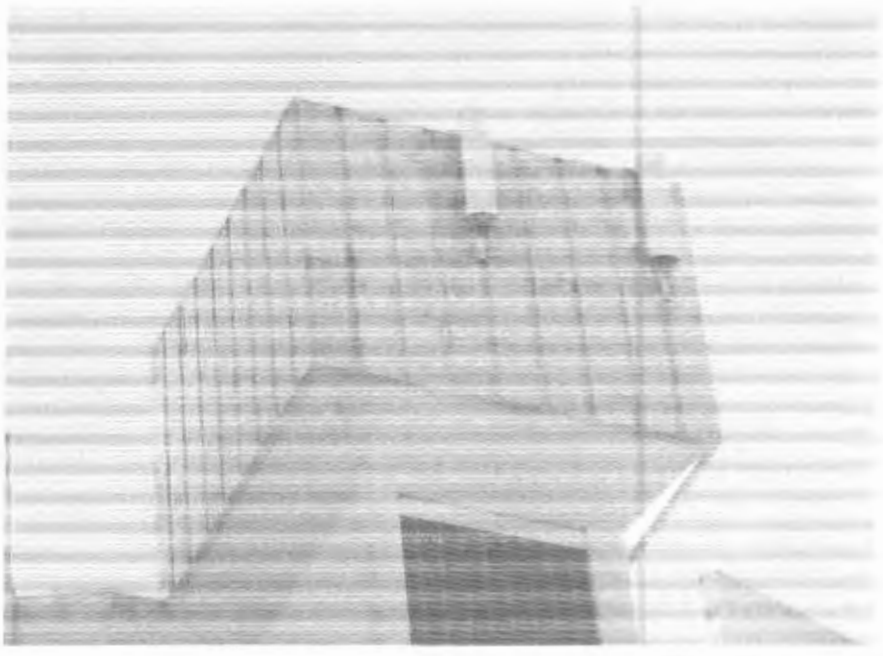


Photo 1: Sample photo illustrating the existing Alpha sector antennas.

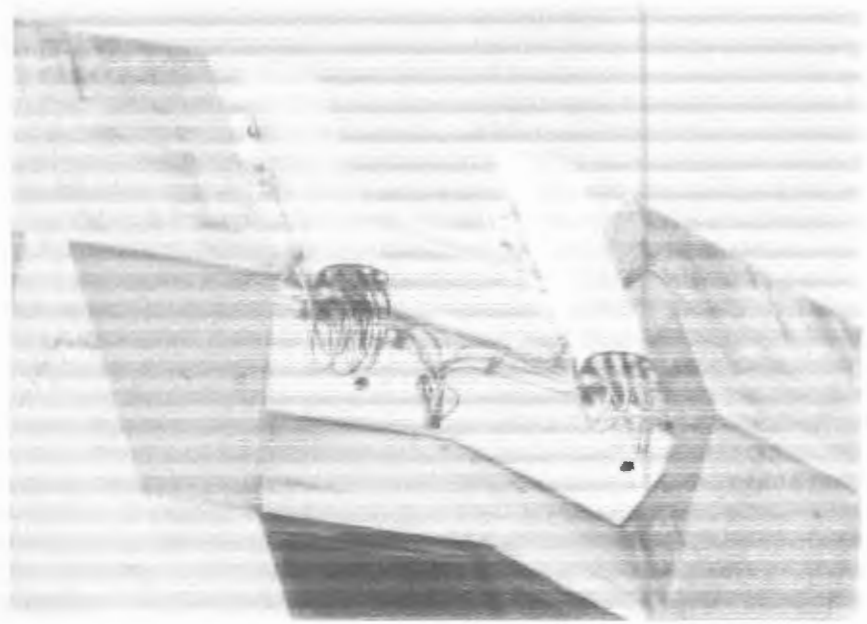


Photo 2: Sample photo illustrating the existing Beta sector antennas.

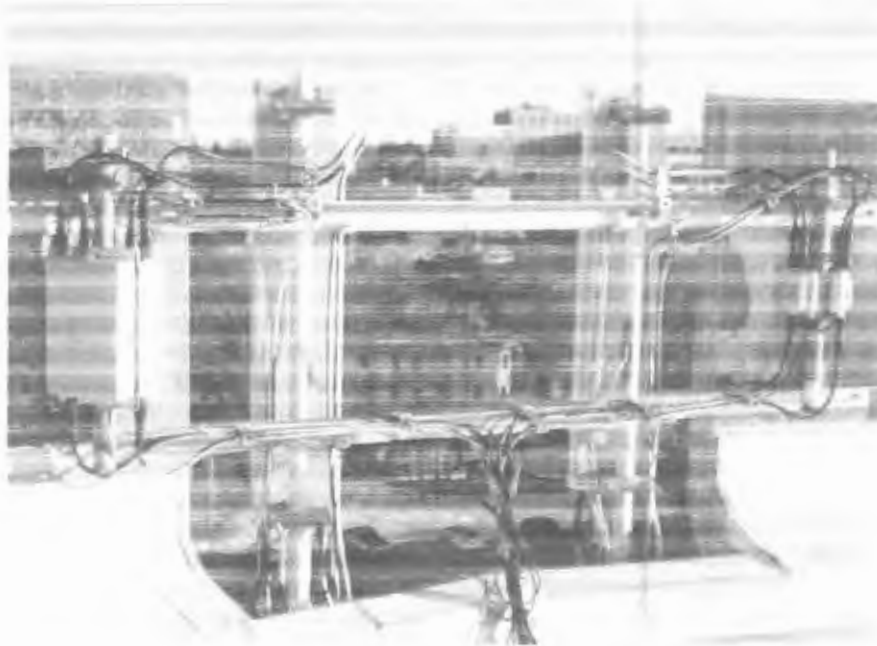


Photo 3: Sample photo illustrating the existing Gamma sector antennas.

EXISTING EQUIPMENT:



Photo 4: Sample photo illustrating the existing equipment.

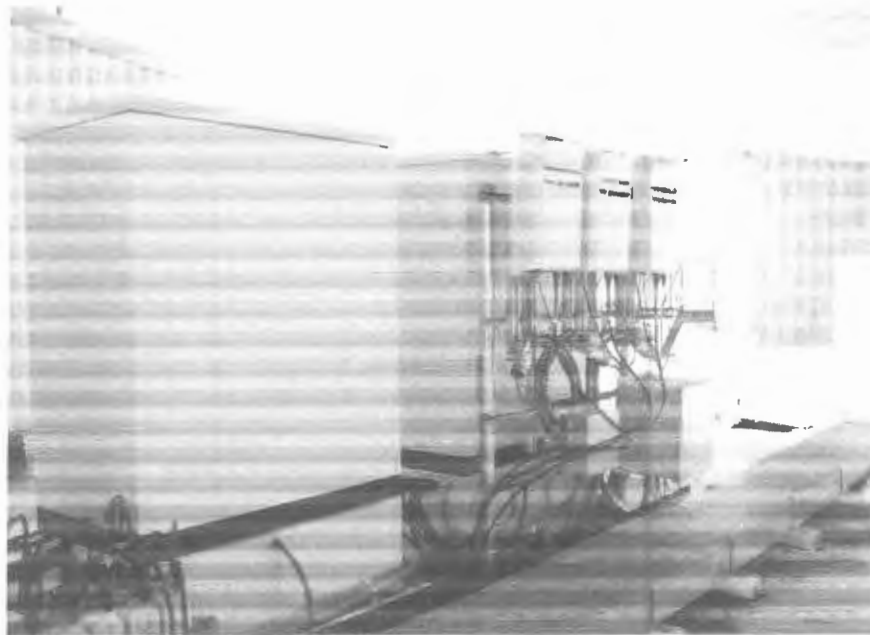


Photo 5: Sample photo illustrating the existing equipment.



Calculations

Date: 03-20-12

Project Name: Portland USM

Project Number: ME5045

Designed By: AA Checked By: MSC



2.6 5.2 Velocity Pressure Coeff:

$$K_z = 2.01 (z/z_g)^{2/\alpha}$$

$z = 88.67$ (ft)
 $z_g = 900$ (ft)
 $\alpha = 9.5$
 $K_z = 1.234$

$K_{zmin} \leq K_z \leq 2.01$

Table 2-4

Exposure	Z_g	α	K_{zmin}	K_e
B	1200 ft	7	0.70	0.90
C	900 ft	9.5	0.85	1
D	700 ft	11.5	1.03	1.10

2.6.6.4 Topographic Factor:

Table 2-5

Topo. Category	K_t	f
2	0.43	1.25
3	0.53	2
4	0.72	1.5

$K_{zt} = [1 + (K_e K_t / K_h)]^2$

$K_h = e^{(1+z/H)}$

$K_{zt} = \#DIV/0!$

$K_h = \#DIV/0!$

(If Category 1 then $K_{zt} = 1.0$)

$K_e = 0$ (from Table 2-4)

$K_t = 0$ (from Table 2-5)

$f = 0$ (from Table 2-5)

Category = 1

$z = 88.67$

$H = 0$ (Ht. of the crest above surrounding terrain)

$K_{zt} = 1.00$

Date: 03-20-12
 Project Name: Portland USM
 Project Number: ME5045
 Designed By: AA Checked By: MSC



2.6.7 Gust Effect Factors

2.6.7.1 Self Supporting Lattice Structures

Gh = 1.0 Latticed Structures > 600 ft

Gh = 0.85 Latticed Structures 450 ft or less

$G_h = 0.85 + 0.15 (h/150 - 3.0)$ h = ht. of structure

h = 88.67 Gh = 0.48867

2.6.7.2 Guyed Masts

Gh = 0.85

2.6.7.3 Pole Structures

Gh = 1.1

2.6.7.4 Structures Supported on Other Structures

(Cantilevered tubular or latticed spines, pole, structures on buildings (ht. : width ratio > 5))

Gh = 1.35

Gh = 1.35

Date: 03-20-12
 Project Name: Portland USM
 Project Number: ME5045
 Designed By: AA Checked By: MSC



2.6.8 Design Ice Thickness:

$$t_{iz} = 2.0 * t_i * I * K_{iz} * (K_{zt})^{0.35}$$

$t_i = 1$
 $I = 1$
 $K_{iz} = 1.10$
 $K_{zt} = 1$

$t_{iz} = 2.21$

$$K = [z/33]^{0.10} \leq 1.4$$

$K_{iz} = 1.10$

Calculating the weight of ice, the cross-sectional area of ice shall be determined by:

$$A_{iz} = \pi * t_{iz} * (D_c + t_{iz})$$

$D_c = 96.4$ (in) Largest Dim of Member

$A_{iz} = 683.94$

2.6.9 Design Wind Load:

$$F = q_z * G * h * (EPA's)$$

$$q_z = 0.00256 * K_z * K_{zt} * K_d * V_{max}^2$$

$K_z = 1.234$
 $K_{zt} = 1$
 $K_d = 0.95$
 $V_{max} = 100$

$q_z = 30.01$

Table 2-2

Structure Type	Wind Direction Probability Factor, Kd
Latticed structures with triangular, square or rectangular cross sections	0.85
Tubular pole structures, latticed structures with other cross sections, appurtenances.	0.95

Date: 03-20-12

Project Name: Portland USM

Project Number: ME5045

Designed By: AA Checked By: MSC



Determine Cf:

If lattice Structure See Manual

If Tubular Pole Structure, Use Corrected Value from Table 2.7 Below:

C mph.ft	Round	18 Sided	16 Sided	12 Sided	8 Sided
< 32 (Subcritical)	1.2	1.2	1.2	1.2	1.2
32 to 64 (Transitional)	$38.4/C^{1.0}$	$25.8/C^{0.885}$	$12.6/C^{0.678}$	$2.99/C^{0.263}$	1.2
> 64 (Supercritical)	0.6	0.65	0.75	1	1.2

$$C = (I * K_{rt} * K_r)^{0.2} * V * D$$

Dp = Outside Diameter or Out to Out: 0.2 feet

C= 22.22 Cf= 1.2

<u>Appurtenances</u>	<u>Height</u>	<u>Width</u>	<u>Depth</u>	<u>Flat Area</u>	<u>Force Per Appurtenance</u>
Item No.1	96.4	11.9	7.1	7.97	387.30 (lbs)
Item No.2	72	11.8	5.9	5.90	286.84 (lbs)
Item No.3	55	11	5	4.20	204.26 (lbs)
Item No.4	0	0	0	0.00	0.00 (lbs)
Item No.5	0	0	0	0.00	0.00 (lbs)

TOTAL FORCE (ΣF_A) =	878.40 (lbs)
------------------------------------------------	---------------------

ICE WEIGHT CALCULATIONS

Project: ME5045

Thickness of ice: 0.75
Weight of ice based on total radial SF area:
Depth (in): 7.1
height (in): 96.4
Width (in): 11.8
Total weight of ice on object: 89 pounds ice
Weight of object: 61 pounds
Combined weight of ice and object: 150 pounds

PROPOSED
Antenna

Per foot weight of ice:
pipe weight per foot: 3.65
pipe length (ft): 8.5
diameter (in): 2.375
Per foot weight of ice on object: 2 pounds ice /ft
Total weight of ice on object: 19 pounds
Total weight of pipe: 31.025 pounds
Combined weight of pipe and ice: 50 pounds

Pipe

* Density of ice used = 56 PCF

Total Weight: 199 pounds

ICE WEIGHT CALCULATIONS

Project: ME5045

Thickness of ice: 0.75

Weight of ice based on total radial SF area

EXISTING
Antenna

Depth (in): 5

height (in): 55

Width (in): 11

Total weight of ice on object: 43 pounds ice

Weight of object: 30 pounds

Combined weight of ice and object: 73 pounds

Per foot weight of ice:

Pipe

pipe weight per foot: 3.65

pipe length (ft): 6

diameter (in): 2.375

Per foot weight of ice on object: 2 pounds ice /ft

Total weight of ice on object: 13 pounds

Total weight of pipe: 21.9 pounds

Combined weight of pipe and ice: 35 pounds

* Density of ice used = 56 PCF

Total Weight: 108 pounds

Project: ME5045 (LTE)
 Location: ANTENNA SUPPORT ANGLE (WORSE CASE)
 Multi-Loaded Multi-Span Beam
 [2009 International Building Code(AISC 13th Ed ASD)]
 A36 L4x4x1/4 x 5.0 FT Leg Up
 Section Adequate By: 410.4%
 Controlling Factor: Shear

Andres Agudelo
 Hudson Design Group LLC
 1600 Osgood Steet, Suite 2-101, Bldg 20N
 North Andover, MA 01845

page
 of

StruCalc Version 8.0.111.0 3/20/2012 2:23:54 PM

DEFLECTIONS		Center
Live Load	0.02	IN L/3163
Horizontal Component	0.01	
Dead Load	0.00	in
Horizontal Component	0.00	in
Total Load	0.02	IN L/2908
Horizontal Component	0.01	
Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240		

REACTIONS		A	B
Live Load	167 lb	130 lb	
Dead Load	17 lb	17 lb	
Total Load	183 lb	146 lb	
Bearing Length	0.63 in	0.63 in	

BEAM DATA		Center
Span Length	5 ft	
Unbraced Length-Top	1.5 ft	
Unbraced Length-Bottom	5 ft	

STEEL ANGLE PROPERTIES
 L4x4x1/4 - A36

Properties:			
Yield Stress:	Fy =	36	ksi
Modulus of Elasticity:	E =	29000	ksi
Depth (Leg Length):	d =	4	in
Leg Thickness:	tw =	0.25	in
Distance to Angle Toe of Fillet:	k =	0.63	in
Moment of Inertia About X-X Axis:	Ix =	3	in4
Section Modulus About X-X Axis:	Sx =	1.03	in3

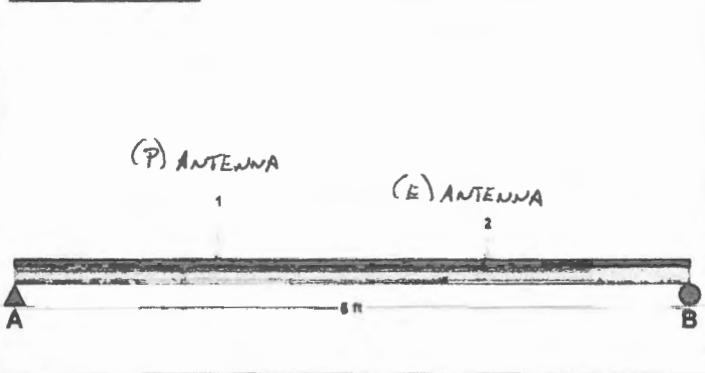
Design Properties per 13th Edition AISC Steel Manual:

Angle Tip is in Compression	
Flange Buckling Ratio:	FBR = 16
Allowable Flange Buckling Ratio for Compact:	AFBR = 15.33
Allowable Flange Buckling Ratio for Non-Compact:	AFBR_NC = 25.83
Elastic Lateral-Torsional Buckling Moment:	Me = 114.89 ft-lb
Nominal Flexural Strength w/ Safety Factor	Mn = 1962.04 ft-lb
Controlling Equation:	F10-3
Controlling Cv Factor:	Cv = 1
Nominal Shear Strength w/ Safety Factor:	Vn = 12934 lb

Controlling Moment: 267 ft-lb
 1.5 Ft from left support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2
Controlling Flexural Shear: 183 lb
Controlling Torsional Shear (C-G4-2): 2351 lb
Controlling Shear: 2534 lb
 At left support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s)

Comparisons with required sections:	Req'd	Provided
Moment of Inertia (deflection):	0.34 in4	3 in4
Moment:	267 ft-lb	1962 ft-lb
Shear:	2534 lb	12934 lb

LOADING DIAGRAM



UNIFORM LOADS		Center
Uniform Live Load	0	plf
Uniform Dead Load	0	plf
Beam Self Weight	7	plf
Total Uniform Load	7	plf

POINT LOADS - CENTER SPAN

Load Number	One	Two
Live Load	194 lb	102.5 lb
Dead Load	0 lb	0 lb
Location	1.5 ft	3.5 ft

$$F_{top} = \frac{358 \#}{2} = 179 \#$$

$$F_{bottom} = \frac{205 \#}{2} = 102 \#$$

* CHECK ANTENNA SUPPORT ANCHORAGE SYSTEM: (1,10RSE-002)

OVERVIEW: THE ANTENNA SUPPORT ANCHORS ARE ATTACHED TO THE PARAPET AT EACH END WITH (2) 1/2" WELTS NY 20 (REFERENCE ORIGINAL DESIGN DRAWINGS PREPARED BY AERIAL SPECTRUM)

$$F_T = 525\# \quad \left\{ \begin{array}{l} \text{HT-UV30} \\ \text{(2" EMBEDMENT)} \\ \text{1 ASSUMED} \end{array} \right.$$

$$F_V = 1230\#$$

- TENSION

$$f_T = \frac{192\#}{2 \text{ ANCHORS}} = 96\#/\text{ANCHOR} < 325\#/\text{ANCHOR} \therefore \text{O.K.}$$

- SHEAR

$$f = \frac{100\# + 100\# + 40\#}{2} = 170\#$$

$$f_V = \frac{170\#}{2 \text{ ANCHORS}} = 85\#/\text{ANCHOR} < 1230\#/\text{ANCHOR} \therefore \text{O.K.}$$

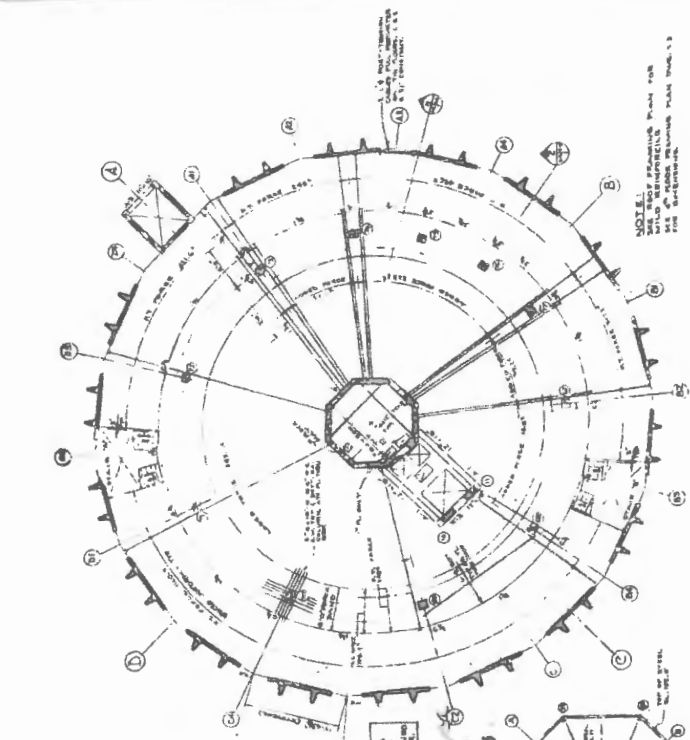
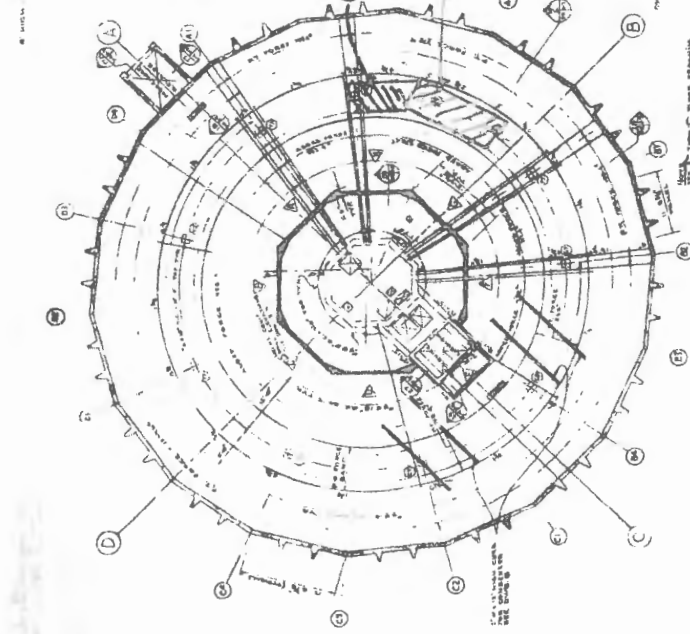
- CHECK COMBINED TENSION/SHEAR:

$$\frac{f_T}{F_T} + \frac{f_V}{F_V} \leq 1.0$$

$$\frac{96}{525} + \frac{85}{1230} = 0.24 < 1.0 \therefore \text{O.K.}$$

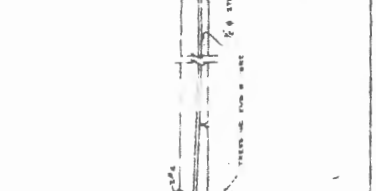
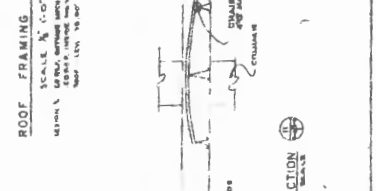
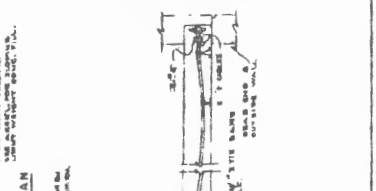
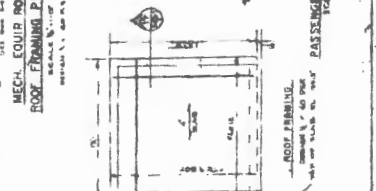
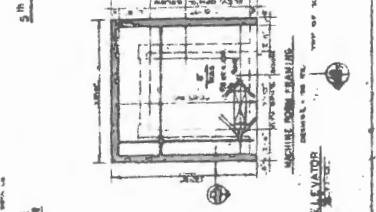


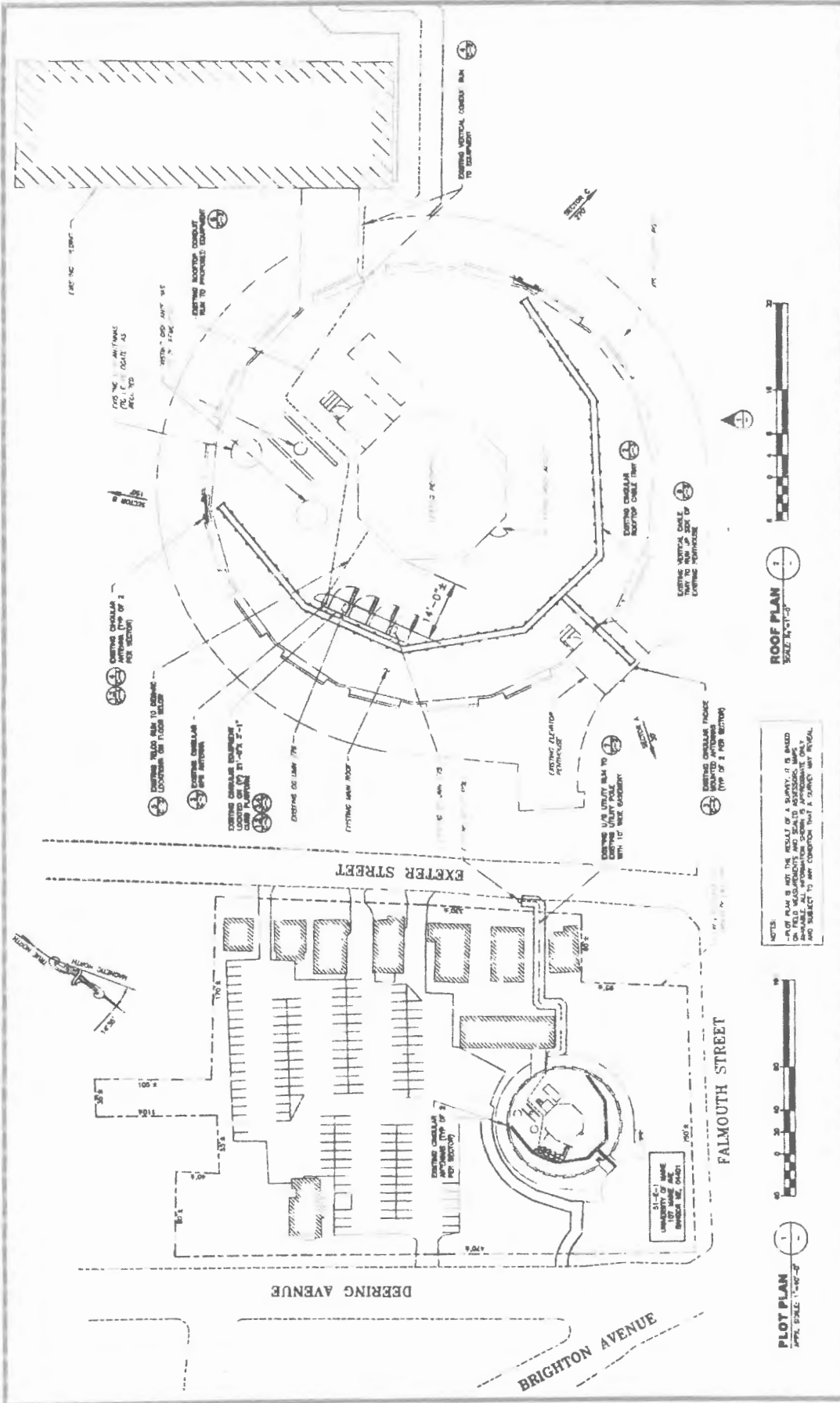
Referenced Drawings



NOTE:
THIS ROOF FRAMING PLAN FOR THE 5TH, 6TH AND 7TH FLOORS IS TO BE CONSIDERED AS A GENERAL GUIDE ONLY. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE FINAL DESIGN AND CONSTRUCTION OF THE ROOFING SYSTEM.

5TH THRU 7TH FLOOR FRAMING PLAN
SCALE: 1/4" = 1'-0"
2" x 4" JOISTS, SPACING 16" O.C. AT PERIMETER AND 24" O.C. IN FIELD.
2" x 4" RAFTERS, SPACING 24" O.C. AT PERIMETER AND 36" O.C. IN FIELD.





NOTES:
 - THIS PLAN IS NOT THE RESULT OF A SURVEY. IT IS BASED ON FIELD MEASUREMENTS AND SHOWN AS APPROXIMATE. MARKS AND DIMENSIONS SHALL BE SUBJECT TO ANY CONDITIONS THAT A SURVEY MAY REVEAL.



ROOF PLAN
 SCALE: 1/4" = 1'-0"



PLOT PLAN
 APPX. SCALE: 1/4" = 1'-0"

CINGULAR WIRELESS

SITE PLAN & ROOF PLAN

PROJECT NO. 12-00000000-00000000-00000000-00000000

DATE	DESCRIPTION
12-1-10	ISSUED FOR PERMITS
12-1-10	ISSUED FOR PERMITS
12-1-10	ISSUED FOR PERMITS

MES045

USM PORTLAND

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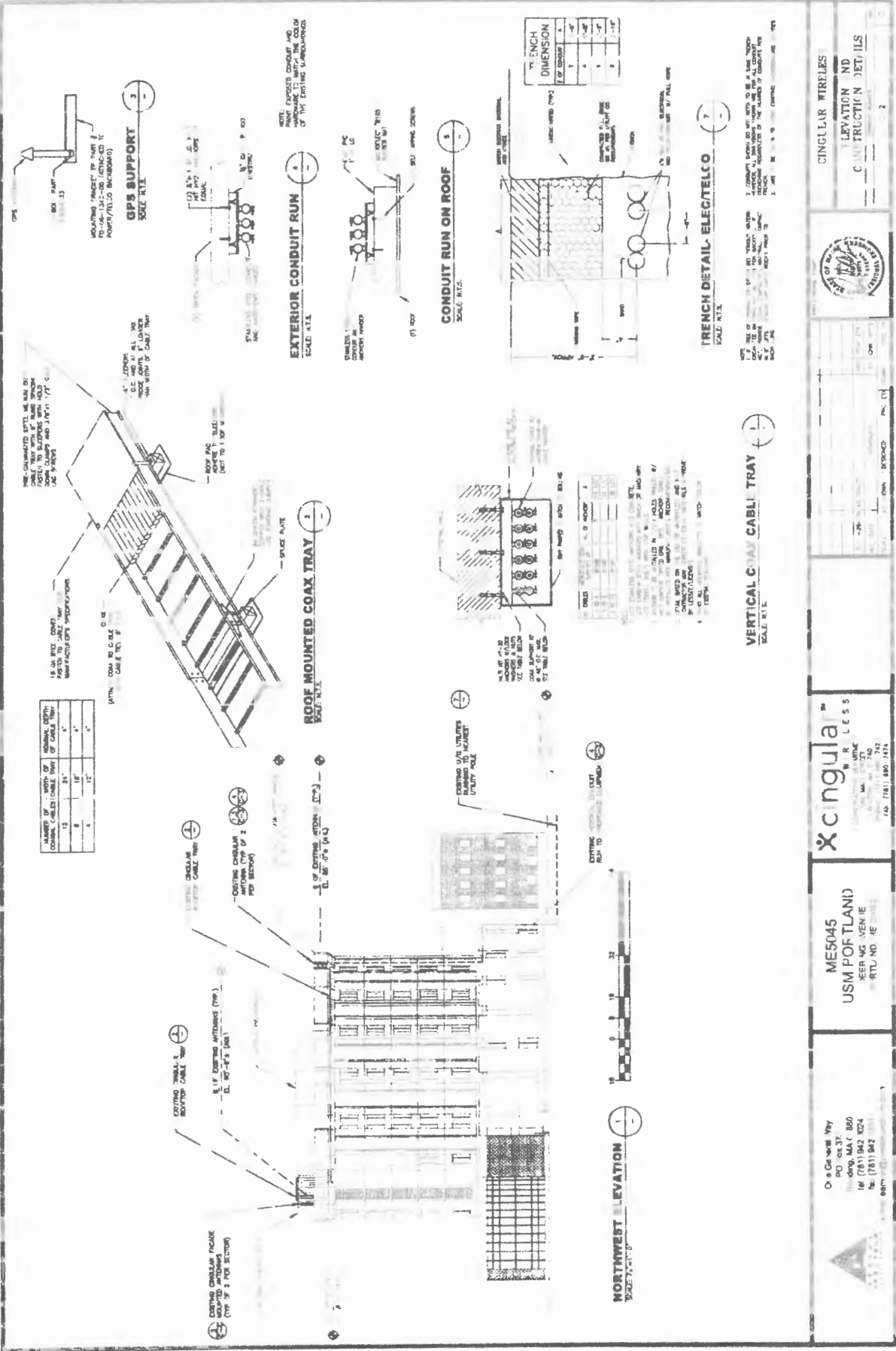


TABLE 1: NUMBER OF CHANNELS (CH) AND CHANNELS PER CABLE TRAY (CPCT) OF CABLE TRAY

NO. OF CHANNELS (CH)	CPCT	NO. OF CHANNELS (CH)	CPCT
12	24"	4"	4"
6	18"	2"	4"
3	12"	1"	4"

TABLE 2: 1/2" ENCH DIMENSION

TYPE OF GROUP	1"	2"	3"	4"
1				
2				
3				
4				

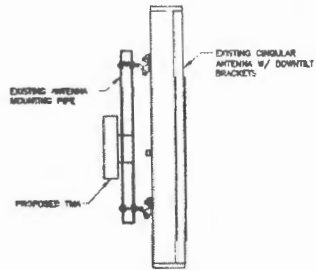
Or a Co. will Why
 P.O. Box 317
 Middletown, MA 01850
 Tel: (781) 942-1024
 Fax: (781) 942-1011

ME5045
 USM PORTLAND
 SEE ME VENTURE
 RTU NO. 4E

cingula
 W R L C S S
 UNIT
 740
 (781) 880-1272

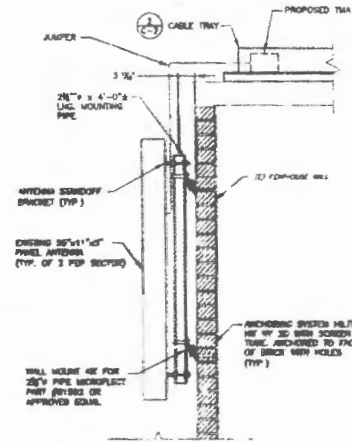


CINGULAR WIRELES
 ELEVATION AND
 CONSTRUCTION DETAILS



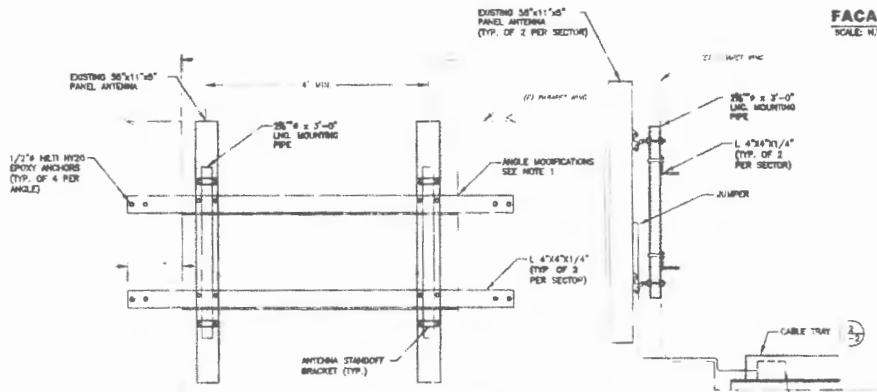
TMA NOTE:
THE REQUIRED NUMBER OF TMAS PER ANTENNA BASED ON RF REQUIREMENTS. CONTRACTOR TO VERIFY PRIOR TO CONSTRUCTION

ANTENNA DETAIL
SCALE: N.T.S.



NOTES:
1. PRIME AND PAINT ALL MOUNTING BRACKETS AND ANCHORS TO MATCH (1) BUILDING FACADE W/CROUT LINES.

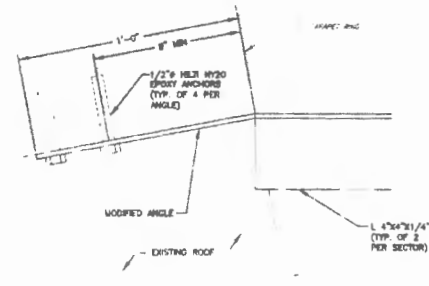
FACADE ANTENNA MOUNTING DETAIL
SCALE: N.T.S.



NOTES:
1. CUT AND BEND ANGLE FLUSH WITH PARAPET W/NG (TYP. OF 2 PER ANGLE)

NOTES:
1. PRIME AND PAINT ALL MOUNTING BRACKETS AND ANCHORS TO MATCH (1) BUILDING FACADE W/CROUT LINES

ANTENNA MOUNTING DETAILS
SCALE: N.T.S.



ANGLE MOUNTING DETAIL
SCALE: N.T.S.



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cingular
WIRELESS
CONSTRUCTION DEPARTMENTS
500 MAIN STREET
BOSTON, MA 02114
PHONE: (781) 942-7422
FAX: (781) 942-7424

DATE	REVISIONS	BY	CHKD BY
AS			



CINGULAR WIRELESS
CONSTRUCTION DETAILS

SCALE	DATE	BY	CHKD BY
C			

 ONE GENERAL WAY PO BOX 373 READING, MA 01867 P: (781) 842-0024 F: (781) 842-0551	CLIENT NAME	DATE: 4/12/06	PAGE: 1/7
	STATE OF MAINE LAW SCHOOL	BY: M. HARTZEL	
		SITE NAME: USM PORTLAND	

NEW LOCATION FOR COLUMNS

CHECK COLUMN 76 f' 75

LOADS:

FROM DESIGN DRAWINGS

ROOF 6.5 #/ft²

7th FLOOR 100 #/ft²

6th FLOOR 100 #/ft²

5th FLOOR 100 #/ft²

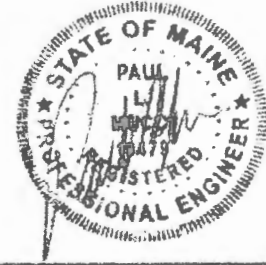
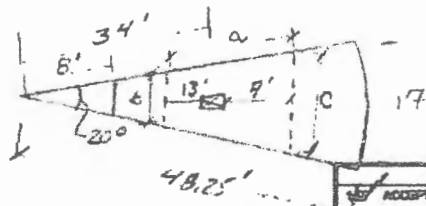
4th FLOOR 100 #/ft² (SEE DRAWING)

LIGHT WT CONCRETE ON ALL FLOORS

115 #/ft²



CALCULATE TRIBUTARY AREA FOR COLUMN



$$C = 2(TAN 10(41)) = 14.4$$

$$b = 2(TAN 10(8)) = 2.8$$

$$a = 20'$$

$$AREA = (C+b)/2 (a) = 172$$


ACCEPTED - NO COMMENTS, PROCEED			
COMMENTS			
A	<input type="checkbox"/> SAC into substructure	F	<input type="checkbox"/> Design deviation from standard
B	<input type="checkbox"/> A/E did not follow drawings provided	G	<input type="checkbox"/> Omissions
C	<input type="checkbox"/> Site owner requested changes	H	<input type="checkbox"/> A/E generated design to design
D	<input type="checkbox"/> Design input changes, i.e., RF, zoning, etc.	I	<input type="checkbox"/> A/EB changed into design
E	<input type="checkbox"/> Reduced site design	J	<input type="checkbox"/> OTHER
<small>Permittee is granted design not complete compliance or approval of design details, calculations, analysis, test methods, or materials developed or selected by the supplier and does not release the supplier from full compliance with applicable regulations.</small>			
Reviewed by: GSEP		Date: 2-12-07	
BY ENGINEER	CA	MARKET LEAD	CONSTRUCTION

SLAB THICKNESS = 8" $\Rightarrow 8/12(172) = 114.7 \text{ ft}^3$

COLUMN LT = $(18" \times 18") / 144 (10') = 22.5 \text{ ft}^3$

LOAD TOTALS:

	LL	DL SLAB	COLUMN
ROOF	10.5'	13.2'	2.6'
7 th FL	17.2'	13.2'	2.6'
6 th FL	17.2'	13.2'	2.6'
5 th FL	17.2'	13.2'	2.6'

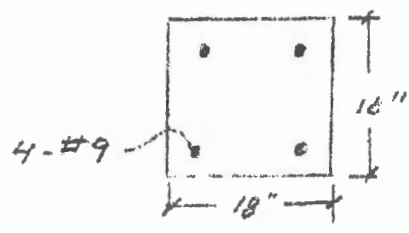
 ONE GENERAL WAY PO BOX 373 READING, MA 01867 P: (781) 942-0024 F: (781) 942-0561	CLIENT NAME:	DATE: 4/12/06	PAGE: 2/-
	STATE OF MAINE LAKE SCHOOL	BY: M. H. [unclear]	
		SITE NAME: [unclear] PAPER MILL'S	

Column Load

MAX COLUMN LOAD @ TOP OF 4TH FLOOR

$$P = 10.5 + (19.2)(3) + (13.2)(4) + (2.6)(4) = 125^k$$

CHECK COLUMN



$K = 0.5$
 $L = 10'$

TOTAL LOAD 4 CABINETS 10/2.5
 $125 + 5 = 130^k$

SEE ATTACHED SPREADSHEET
(MATH CADD)

Input Column Properties

$$f_c = 3000 \text{ psi} \quad A_s = 2 \text{ in}^2 \quad d' := 2.564 \text{ in} \quad b := 18 \text{ in}$$

$$f_y = 60000 \text{ psi} \quad A's = 2 \text{ in}^2 \quad h := 18 \text{ in}$$

$$A_g := b \cdot h \quad A_g = 324 \text{ in}^2 \quad y_{\text{bar}} := \frac{h}{2} \quad y_{\text{bar}} = 9 \text{ in}$$

Maximum Vertical Loading

$$P_o := [0.85 f_c (A_g - A_s - A's) + (A_s + A's) \cdot f_y]$$

$$P_o = 1056 \text{ kip}$$

$$\phi P_o := 0.7 \cdot P_o$$

$$\phi P_o = 739.2 \text{ kip}$$

$$P_{n\text{max}} := 0.8 [0.85 f_c (A_g - A_s - A's) + (A_s + A's) \cdot f_y]$$

$$\phi P_{n\text{max}} := 0.7 \cdot P_{n\text{max}}$$

$$P_{n\text{max}} = 844.8 \text{ kip}$$

$$\phi P_{n\text{max}} = 591.36 \text{ kip}$$

$$\phi M_o := 0$$

Balance Condition

$$d := h - d'$$

$$d = 15.436 \text{ in}$$

$$c_b := \frac{87000}{87000 + \frac{f_y}{\text{psi}}} \cdot d$$

$$c_b = 9.14 \text{ in}$$

$$\epsilon's := 0.003 \left(\frac{c_b - d'}{c_b} \right)$$

$$\epsilon's = 0.00216 \frac{\text{in}}{\text{in}}$$

$$f_s := 29000000 \text{ psi} \cdot \epsilon's$$

$$f_s = 62582.534 \text{ psi}$$

$$\beta_1 := 0.85 - \frac{0.05 \left(\frac{f_c}{\text{psi}} - 4000 \right)}{1000}$$

$$\beta_1 = 0.9$$

$$a_b := \beta_1 \cdot c_b$$

$$a_b = 8.22 \text{ in}$$

$$P_{nb} := 0.85 \cdot f_c \cdot b \cdot a_b + A's \cdot f_s - A_s \cdot f_y$$

$$\phi P_{nb} := 0.7 \cdot P_{nb}$$

$$P_{nb} = 382.556 \text{ kip}$$

$$\phi P_{nb} = 267.789 \text{ kip}$$

$$M_{nb} := 0.85 \cdot f_c \cdot b \cdot a_b \cdot \left(y_{\text{bar}} - \frac{a_b}{2} \right) + A's \cdot f_s \cdot (y_{\text{bar}} - d') + A_s \cdot f_y \cdot (d - y_{\text{bar}})$$

$$\phi M_{nb} := 0.7 \cdot M_{nb}$$

$$M_{nb} = 3422.942 \text{ in-kip}$$

$$\phi M_{nb} = 199.7 \text{ ft-kip}$$

$$e_b := \frac{M_{nb}}{P_{nb}}$$

$$e_b = 8.95 \text{ in}$$

Pure Bending Mno

$$a := \frac{A_s \cdot f_y}{0.85 \cdot f_c \cdot b}$$

$$a = 2.61 \text{ in}$$

$$\beta_1 := \frac{a}{c}$$

$$c = 2.9 \text{ in}$$

$$\epsilon'_{s_m} := 0.003 \cdot \left(\frac{c - d'}{c} \right)$$

$$\epsilon'_{s_m} = 0.00035 \frac{\text{in}}{\text{in}}$$

$$f'_{s_m} := 29000000 \text{ psi} \cdot \epsilon'_{s_m}$$

$$f'_{s_m} = 10208.841 \text{ psi}$$

$$M_{no} := A_s \cdot f_y \cdot \left(d - \frac{a}{2} \right)$$

$$\phi M_{no} := 0.9 \cdot M_{no}$$

$$M_{no} = 1695.5 \text{ in-kip}$$

$$\phi M_{no} = 127.2 \text{ ft-kip}$$

$$\phi P_0 := 0 \text{ kip}$$

Compression Controls

$$c_1 := \frac{c_b + h}{2} \quad c_1 = 13.57 \text{ in}$$

$$\epsilon'_{s_1} := 0.003 \cdot \left(\frac{c_1 - d'}{c_1} \right)$$

$$\epsilon_{y1} := \frac{f_y}{29000000}$$

$$\epsilon_{s1} := 0.003 \cdot \frac{d - c_1}{c_1}$$

$$\epsilon'_{s_1} = 0.00243 \frac{\text{in}}{\text{in}}$$

$$\epsilon_{y1} = 0.00207 \frac{\text{in}}{\text{in}}$$

$$\epsilon_{s1} = 0.00041 \frac{\text{in}}{\text{in}}$$

$$\epsilon'_{s_1} := \min(\epsilon'_{s_1}, \epsilon_{y1})$$

$$f_{s_1} := \epsilon'_{s_1} \cdot 29000000 \text{ psi}$$

$$f_{s_1} := \epsilon'_{s_1} \cdot 29000000 \text{ psi}$$

$$f_{s_1} = 11979.378 \text{ psi}$$

$$f_{s_1} = 60000 \text{ psi}$$

$$a_1 := \beta_1 \cdot c_1$$

$$a_1 = 12.21 \text{ in}$$

$$C_{c1} := 0.85 \cdot f_c \cdot b \cdot a_1$$

$$C_{s1} := A_s \cdot f_y$$

$$T_{s1} := A_s \cdot f_{s_1}$$

$$C_{c1} = 560.49 \text{ kip}$$

$$C_{s1} = 120 \text{ kip}$$

$$T_{s1} = 23.96 \text{ kip}$$

$$P_{n1} := C_{c1} + C_{s1} - T_{s1}$$

$$\phi P_{n1} := 0.7 \cdot P_{n1}$$

$$P_{n1} = 656.53 \text{ kip}$$

$$\phi P_{n1} = 459.57 \text{ kip}$$

$$M_{n1} := C_{c1} \cdot \left(y_{bar} - \frac{a_1}{2} \right) + C_{s1} \cdot (y_{bar} - d') + T_{s1} \cdot (d - y_{bar})$$

$$\phi M_{n1} := 0.7 \cdot M_{n1}$$

$$M_{n1} = 2548.84 \text{ in-kip}$$

$$\phi M_{n1} = 148.682 \text{ ft-kip}$$

$$c_1 := \frac{M_{n1}}{P_{n1}}$$

$$c_1 = 3.88 \text{ in}$$

Tension Controls

$$c_2 := \frac{c_b}{\gamma} \quad c_2 = 4.57 \text{ in}$$

$$a_2 := \beta_1 \cdot c_2$$

$$\epsilon's_2 := 0.003 \cdot \left(\frac{c_2 - d'}{c_2} \right)$$

$$a_2 = 4.11 \text{ in}$$

$$\epsilon's_2 = 0.00132$$

$$f_{s2} := \min(\epsilon's_2 \cdot 29000000 \text{ psi}, 60000 \text{ psi})$$

$$f_{s2} = 38165.069 \text{ psi}$$

$$f_{s2} := f_y$$

$$f_{s2} = 60000 \text{ psi}$$

$$C_{c2} := 0.85 \cdot f_c \cdot b \cdot a_2$$

$$C_{c2} = 188.7 \text{ kip}$$

$$C_{s2} := A_s \cdot f_{s2}$$

$$C_{s2} = 76.33 \text{ kip}$$

$$T_{s2} := A_s \cdot f_y$$

$$T_{s2} = 120 \text{ kip}$$

$$P_{n2} := C_{c2} + C_{s2} - T_{s2}$$

$$\phi P_{n2} := 0.7 \cdot P_{n2}$$

$$P_{n2} = 145.03 \text{ kip}$$

$$\phi P_{n2} = 101.52 \text{ kip}$$

$$M_{n2} := C_{c2} \cdot \left(y_{\text{bar}} - \frac{a_2}{2} \right) + C_{s2} \cdot (y_{\text{bar}} - d') + T_{s2} \cdot (d - y_{\text{bar}})$$

$$\phi M_{n2} := 0.7 \cdot M_{n2}$$

$$M_{n2} = 2573.976 \text{ in-kip}$$

$$\phi M_{n2} = 150.15 \text{ ft-kip}$$

$$e_2 := \frac{M_{n2}}{P_{n2}}$$

$$e_2 = 17.75 \text{ in}$$

Interaction Diagram Loads and Moments

$$\phi M := \begin{pmatrix} \frac{\phi M_0}{ft \cdot kip} \\ \frac{\phi M_{n1}}{ft \cdot kip} \\ \frac{\phi M_{nb}}{ft \cdot kip} \\ \frac{\phi M_{n2}}{ft \cdot kip} \\ \frac{\phi M_{no}}{ft \cdot kip} \end{pmatrix} \quad \phi P := \begin{pmatrix} \frac{\phi P_0}{kip} \\ \frac{\phi P_{n1}}{kip} \\ \frac{\phi P_{nb}}{kip} \\ \frac{\phi P_{n2}}{kip} \\ \frac{\phi P_0}{kip} \end{pmatrix} \quad \phi M1 := \begin{pmatrix} \frac{0}{ft \cdot kip} \\ \frac{\phi M_{nb}}{ft \cdot kip} \end{pmatrix}$$

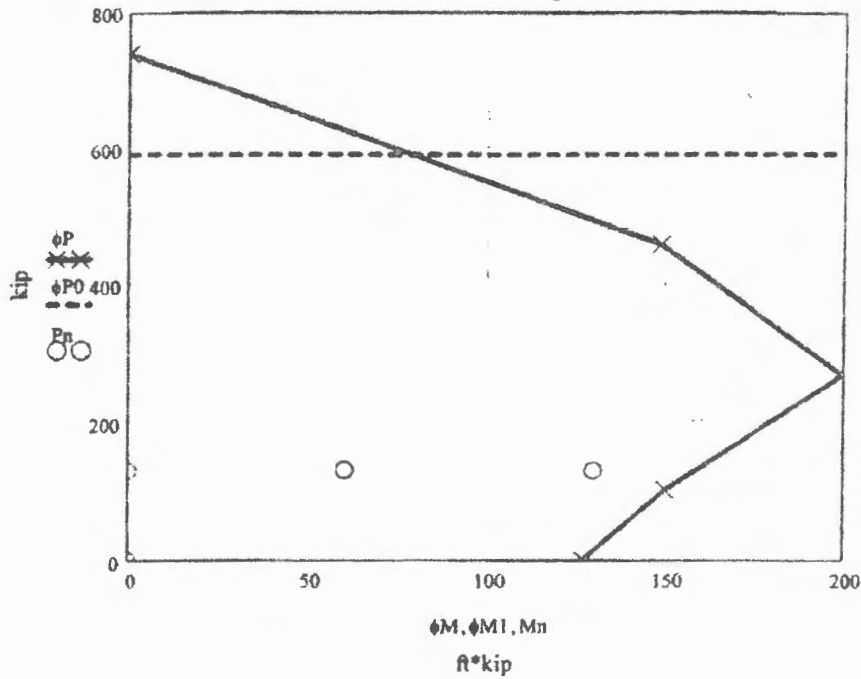
$$\phi P0 := \begin{pmatrix} \frac{\phi P_{nmax}}{kip} \\ \frac{\phi P_{nmax}}{kip} \end{pmatrix}$$


Loads and Moments from Structure

$$P_n := \begin{pmatrix} 130 \\ 130 \\ 130 \\ 0 \end{pmatrix} \quad M_n := \begin{pmatrix} 0 \\ 60 \\ 130 \\ 0 \end{pmatrix}$$

(kip and ft-kip)

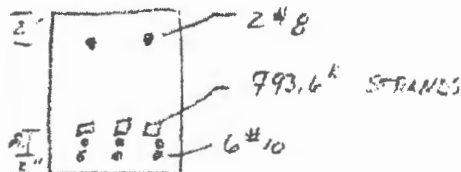
Interaction Diagram



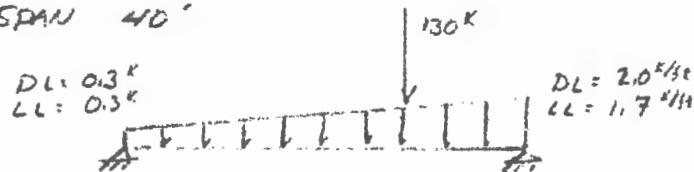
 ONE GENERAL WAY PO BOX 373 READING, MA 01867 P (781) 942-0024 F (781) 942-0551	CLIENT NAME	DATE	PAGE
	STATE OF MAINE LAW SCHOOL	4/12/06	77
		BY M. MASTRI	SITE NAME JSM PORTLAND

CHECK BEAM ON 4th FLOOR

BEAM B-2 & B-2A



SPAN 40'



$$M = 18.31 \text{ ft kips} = 21972 \text{ in kips}$$

$$\begin{aligned}
 f^t &= -\frac{P_c}{AC} \left(1 + \frac{eG}{r^2} \right) + \frac{21972}{S_x} \\
 &= -\frac{793.6}{1260} \left(1 + \frac{17(21)}{12.12^2} \right) + \frac{21972}{8520} = \\
 &= -0.63 \text{ ksi} (1 + 2.43) + 2.49 = 0.324 \text{ ksi } \underline{\underline{OK}}
 \end{aligned}$$

$$f^b = -0.63 (1 - 2.43) - 2.49 = 7.59 \text{ ksi } \underline{\underline{OK}}$$