#### SECTION 023200 - GEOTECHNICAL INVESTIGATIONS

#### PART 1 - GENERAL

#### 1.1 RELATED DOCUMENTS

A. Drawings and general provisions of the Contract, including General and Supplementary Conditions and Division 01 Specification Sections, apply to this Section.

#### 1.2 SUMMARY

A. This Section includes geotechnical investigations.

#### 1.3 DESCRIPTION

- A. Subsurface explorations have been done at the location of the project and soils reports have been compiled for the purpose of guidance in the design of the project facilities. This work can include open excavation test pits, observation wells and soil borings.
- B. The logs are not intended to indicate subsurface conditions except at the locations of the exploration (at the time explorations were made) and any interpretation the Contractor may make is his responsibility.
- C. The subsurface investigations of the site were made in conjunction with design of the facility to be constructed under this Contract. Portions of this investigation are presented in reports which are a part of the Contract Documents. The reports present the opinion of the Geotechnical Engineer and shall not be interpreted to prescribe or dictate construction procedures or relieve the Contractor in any way of his responsibility for the construction. The explorations are shown on the drawings and the logs are include in Appendix A and B.
- D. The water levels shown on the log at the exploration locations are based on observations made by the Field personnel at the same time the explorations were made and may or may not represent the groundwater surface in the immediate vicinity of the explorations. They are presented only as an observation of the free-standing water surface in the exploration on the date noted.
- E. The refusal depths shown at the exploration locations indicate only, that in the drill foreman's opinion, sufficient resistance to the advance of the casing, auger, probe rod or sampler was encountered to render further advance impossible or impractical by the procedures and equipment being used. Although refusal may indicate the encountering of the bedrock surface, it may indicate the striking of large cobbles, boulders, very dense or cemented soil, or other buried natural or man- made objects or it may indicate the encountering of a harder zone after penetrating a considerable depth through a weathered or disintegrated zone of the bedrock.

PART 2 - PRODUCTS (Not Used)

PART 3 - EXECUTION (Not Used)

END OF SECTION 023200



# **GEOTECHNICAL REPORT**

New Apartment Building 665 Congress Street Portland, Maine

Prepared for:

Redfern Properties P.O. Box 8816 Portland, Maine 04104

Prepared by:

Summit Geoengineering Services 145 Lisbon St. Lewiston, Maine

> Project #15040 May 2015



May 1, 2015 SGS #15040

Jonathan Culley Redfern Properties P.O. Box 8816 Portland, Maine 04104

Reference: Geotechnical Report, New Apartment Building 665 Congress Street, Portland, Maine

Dear Jonathan;

Summit Geoengineering Services, Inc. (SGS) has completed a geotechnical investigation for the proposed apartment building at the site reference above. Our scope of services included the drilling of 13 borings and 9 probes and preparing this geotechnical report summarizing our findings and providing geotechnical recommendations.

## 1.0 Project Description

We understand that the project consists of the construction of an 8 story building at the site referenced above. The existing site contains Joe's Smoke Shop abutting Congress Street with a paved parking lot behind. The grade at the site slopes gently down towards the back of the parking lot. The site is bordered by Avon Street on the east and Vernon Street on the west. There used to be a church at the southern portion of the site which was demolished in 1965.

We understand that the newly proposed 8 story building is a steel framed structure which will consist of combined retail space and parking on the first floor and apartment living spaces in the top 7 floors. We also understand there is a proposed full basement for parking. We further understand that the proposed finish floor elevation of the first floor is near existing grade. There will be two elevator shafts on either end of the building (north and south).

We have been provided with preliminary structural loads which include the following:

Columns loads: 200 – 350 kip Line loads: 2 – 15 k/lf Uplift load: 100 kips

# 2.0 Exploration

## 2.1 Exploration

Summit Geoengineering Services (SGS) observed the subsurface conditions at the site with the drilling of 5 borings and six probes (B-1 through B-5 and P-1 through P-6) on March 31, 2015. All of the borings and probes were drilled to refusal, ranging in depth from 0.8 to 15.8 feet below ground surface. Borings and probes were advanced using 2-1/2" hollow stem augers. During the borings, split spoon sampling was conducted in general accordance with ASTM D1586 to collect blow counts and soil samples. Probes were advanced to refusal in order to document the bedrock topography throughout the site. Auger cuttings (if present) and relative drilling resistance were used to estimate the soil types in absence of soil sampling.

SGS performed a second investigation on April 15, 2015 with the drilling of 8 borings and 3 probes (B-101 through B-108 and P-101 through P-103). The drilling was conducted by Great Works Test Boring of Berwick, Maine under the supervision of SGS. All of the borings and probes were drilled to refusal using a Mobile B-53 tracked rig and 4" hollow stem augers. Borings B-105 and B-106 were pre-augered and then cased washed to refusal where rock core samples were collected. Split spoon sampling was conducted in general accordance with ASTM D1586 to collected blow counts and soil samples. Probes were advanced to refusal in order to further document the bedrock topography throughout the site. Auger cuttings (if present) and relative drilling resistance were used to estimate the soil types in absence of soil sampling.

Locations of the borings and probes were marked by SGS prior to drilling by measuring from the existing building and surrounding landmarks. These locations can be seen in the SGS Exploration Plan in Appendix A. The boring and probe logs can be found in Exploration Logs in Appendix B.

## 3.0 Subsurface Conditions

# 3.1 Soil

The soil at the site generally consists of *pavement* overlying *fill* overlying *glacial till* overlying *weathered bedrock* overlying *bedrock*.

The *pavement* at the site was present at the location of all drilled borings and probes. It ranged from 2.5" to 4.0" in thickness.

The *fill* layer was encountered in all borings directly below the pavement and ranged from 4.3 feet to 8.8 feet in thickness, generally increasing in thickness towards the end of the site containing Joe's Smoke Shop. The *fill* is described as dark brown gravelly sand to brown and black sandy silt with varying amounts of ash and brick fragments. It is very loose to compact and humid to frozen. The *fill* located at the southern end of the site nearer to Joe's Smoke Shop

contained large voids and frequent rubble apparent from inspection of the open bore hole and difficult drilling conditions. The *fill* classifies as ML, SP, GP, SM, or SP-SM, in accordance with the Unified Soil Classification System.

The *glacial till* was encountered in borings B-1, B-2, B-3, B-101, B-103, B-104, B-107, and probe P-3 and P-101. *Glacial till* may also be present at the locations of other probes but the cuttings from the layer did not make it to the ground surface for visual inspection. The *glacial till* is described as olive green silt with trace to little clay, sand, and gravel. It is humid to damp, compact to dense, and ranges in thickness from 1.2 feet to 6.8 feet. Standard Penetration Test (SPT-N) blow counts in this layer ranged from 18 to 44 with an average of 28. Pocket penetrometer measurements (a rough estimate of unconfined compressive strength) ranged from 4,000 psf to greater than 9,000 psf. It classifies as ML in accordance with the Unified Soil Classification System.

The *weathered bedrock* was encountered in borings B-4, B-104, B-105, and B-107 and probes P-1, P-2, and P-3. It ranged in thickness from 1.0 feet to 2.9 feet.

Soil profile cross sections of the site can be found in Appendix A titled "Interpretive Soil Profiles".

# 3.2 Groundwater

Groundwater was not encountered in any of the borings or probes. The glacial till recovered in borings B-1, B-2, B-101, B-104, and B-107 from depth 5 feet to 15 feet was slightly to heavily mottled, indicating that groundwater may be confined in this layer during wet periods.

# 3.3 Bedrock

Bedrock was encountered at the site ranging from 4.8 feet to 15.8 feet below existing ground surface. The bedrock elevation ranges from 99.8 feet to 107.3 feet. The table below summarizes the depth to bedrock encountered in the borings and probes and the approximate elevation at each location. Bedrock mapping by the Maine Geologic Survey classifies the bedrock at the site as the Precambrian Z Spring Point Formation consisting of green schist and amphibolites facies ranging from and mafic to felsic volcanic rock.

BEDROCI	<b>BEDROCK DEPTH &amp; ELEVATION</b>									
<b>Boring/Probe</b>	Depth (ft)	Elevation (ft)								
B-1	15.8	100.1								
B-2	11.6	102.4								
B-3	6.2	106.7								
B-4	7.2	105.3								
B-5	4.8	107.7								
B-101	11.9	106.6								
B-102	-	-								
B-103	14.5	100.5								
B-104	9.5	103.6								

*B-105	10.0	103.8
*B-106	10.0	102.0
B-107	10.5	102.4
B-108	8.5	101.7
P-1	10.0	104.9
P-2	10.0	103.9
P-3	9.9	102.9
P-4	-	-
P-5	-	-
P-6	5.0	107.3
P-101	10.8	105.6
P-102	12.1	99.8
P-103	9.6	102.7
* (	Cora complex obtain	

\* = Core samples obtained

Three rock core samples were obtained, one from B-105 and two from B-106. The recovered samples are classified as moderately weathered, very thinly spaced joints/fractures, medium to light gray schist. Rock Quality Designation (RQD) of the samples ranged from 0% (very poor) to 80% (good), increasing in quality as the sample depth increased. A majority of the joints and fractures were  $45^{\circ}$  to vertical. A photograph log of the collected sample can be found in Appendix C.

#### 4.0 Evaluation

The key geotechnical issues at the site include the following:

- Potential for differential settlement of the building supported partially by bedrock and partially by native soil (glacial till)
- Presence of rubble fill in the southern portion of the site presenting excavation difficulty and poor foundation and slab support
- Large uplift loads requiring the use of grouted rock anchors

Based on the preliminary design loads and the proposed building layout, we believe that the new building can be adequately supported by a conventional frost wall on continuous spread footing foundation. The interior columns can be supported by isolated column footings. Based on the finish floor elevations, interior and exterior footings will likely be supported by a combination of glacial till and bedrock. There is also a chance that existing rubble fill will be present at the bottom of footing elevation (near the southern portion of the building). It will be critical to remove all rubble fill from below the footings to ensure that tolerable settlements are not exceeded.

Uplift loading on the new building appears to be significant. We anticipate that rock anchors will be necessary to support the uplift loading on the foundation.

## 5.0 Foundation Recommendations

## 5.1. Allowable Bearing Pressure

We recommend that footings be proportioned using an allowable bearing pressure of 10,000 psf for foundations constructed on bedrock and an allowable bearing pressure of 4,000 psf for footings constructed on glacial till and Structural Fill (SF, see Section 5.2). Total settlement is expected to be less than 1.0" for footings constructed on glacial till and SF. Total settlement will be negligible for footings constructed on bedrock. Differential settlement is not anticipated to exceed 1.0" between footings on bedrock and footings on the native glacial till soil. The allowable bearing pressures above are based on the following conditions:

- All rubble and debris is removed from beneath the footings
- Footings are constructed on glacial till, placed Structural Fill (SF, see Section 5.2), or bedrock. If existing fill is exposed at the bottom of the footing excavation, it should be removed in its entirety down to the glacial till layer and laterally equal to a distance of the footing width on each side of the footing.
- All placed fill within the building footprint consist of SF placed in a maximum of 12" lifts and compacted to 95% of its optimum dry density in accordance with ASTM D1557.
- For footings supported on bedrock, any loose or weathered bedrock is removed to expose hard bedrock.
- Transition zones for footings spanning bedrock to native soil/placed fill be constructed in accordance with the Transition Zone Construction Detail provided in Appendix D.
- Exposed native soil is proofrolled with a minimum of 2 passes in each of two perpendicular directions with a 5 ton minimum (operating weight) vibratory roller or a large vibratory plate compactor. Any soft or unsuitable soil is removed and replaced with <sup>3</sup>/<sub>4</sub>" crushed stone or SF.

## 5.2 Slabs-on-grade

Based on a finish floor elevation of 108 feet for the basement level parking, the slab-on-grade will be supported by a combination of existing rubble fill, glacial till (native), and existing sandy silt fill. Although unlikely, the bedrock surface may rise up to this elevation in some isolated locations. To avoid differential settlement of the slab, we recommend a minimum of 12" of Structural Fill (SF, see table below) be placed under the slab for the entire building footprint to act as a cushion between the slab and underlying soil/bedrock.

Any exposed native soil should be proofrolled with a minimum of 2 passes in each of two perpendicular directions with a 5 ton minimum (operating weight) vibratory roller. Any exposed rubble, debris, or other non-soil materials should be removed and replaced with SF. Any loose or weathered bedrock should be removed to expose a hard bedrock surface.

The slab subgrade soil should be observed by SGS after proofrolling and prior to the placement of SF. A layer of geotextile or other subgrade improvement method may be necessary.

	STRUCTURAL FILL (SF)								
	Sieve Size	Percent finer							
	3 inch	100							
	<sup>1</sup> / <sub>2</sub> inch	38 to 80							
	<sup>1</sup> / <sub>4</sub> inch	25 to 65							
	No. 40	0 to 30							
	No. 200	0 to 7							
<u> </u>									

The portion of SF passing the 3" sieve shall meet the following gradation requirements.

Reference: MDOT Specification 703.06, Type D

The maximum particle size should be limited to 6 inches. Structural Fill should be placed in 6 to 12 inch lifts and should be compacted to a minimum of 95 percent of its maximum dry density, determined in accordance with ASTM D1557.

For the conditions described above, the slab can be designed using a subgrade modulus value of 150 pci.

We anticipate that the existing rubble fill in the southern portion of the site will be difficult to compact and place fill on. Our experience from the geotechnical investigation indicates that there are frequent large voids and large rubble pieces throughout the layer. Flowable fill and/or <sup>3</sup>/<sub>4</sub>" crushed stone can be used to fill the voids and create a flat surface on which to place the SF for the building slab if needed.

## 5.3 Frost Protection and Foundation Backfill

Based on a 10-year design air freezing index of 1,200 degree F days for the Portland, Maine region, all foundation walls exposed to freezing temperatures should be constructed at a minimum depth of 4 feet below finish basement floor grade. However, in locations where the footing is supported by bedrock, footings may be constructed at a minimum depth of 2 feet below finish basement floor grade. We recommend that these elements be backfilled with Foundation Backfill (FB). The portion of FB passing the 3" sieve size should meet the following gradation requirements:

FOUNDATION BACKFILL (FB)							
Sieve Size	Percent finer						
3 inch	100						
<sup>1</sup> /4 inch	25 to 100						
No. 40	0 to 50						
No. 200	0 to 7						

Reference: MDOT Specification 703.06, Type E

Maximum particle size should be limited to 6 inches. Foundation backfill should be placed in 6 to 12 inch lifts and compacted to 95% of its optimum dry density determined in accordance with ASTM D1557.

## 5.4 Seismic Site Class and Design Criteria

Based on the blow counts collected during split spoon sampling and the fractured/jointed condition of the bedrock surface, the site classifies as Site Class C "very dense soil and soft rock" for footings constructed on glacial till and Site Class B "rock" in accordance with the 2009 International Building Code. The site can be conservatively classified entirely as site class C if desired. The following seismic site coefficients should be used:

SEISMIC DESIGN COEFFICIENTS									
Seismic Coefficient	Site Class B	Site Class C							
Short period spectral response $(S_S)$	0.315	0.315							
1 second spectral response $(S_1)$	0.077	0.077							
Maximum factored spectral response (S <sub>MS</sub> )	0.315	0.378							
1 second factored spectral response $(S_{M1})$	0.077	0.131							
Design short period spectral response $(S_{DS})$	0.210	0.252							
Design 1 second spectral response (S <sub>D1</sub> )	0.051	0.087							

No liquefiable soils were encountered in the investigation.

## 5.4 Groundwater Considerations

Groundwater was not encountered in the borings. However, apparent from the mottling of the native glacial till, groundwater is anticipated to fluctuate within the glacial till layer on a seasonal basis. Based on this, we recommend that perimeter underdrains be installed along the entire perimeter of exterior foundations. We recommend that underdrains consist of 4-inch diameter, perforated PVC pipe surrounded by a minimum of 6 inches of crushed stone wrapped in filter fabric. The underdrains should be placed at the base of the foundation and outlet to a free draining location or pumped if necessary. An underdrain or sump pump is highly recommended for the elevator shaft foundation.

## 5.5 Foundation Uplift and Sliding Capacity

Uplift capacity of the foundation includes the dead weight of the foundation, skin friction of the mobilized soil, and weight of soil above the footings. Sliding resistance of the foundation includes the passive resistance of the soil against the side of the foundation wall and the friction between the bottom of the footing and the underlying soil/bedrock. We recommend that the following coefficients be used in the uplift and sliding capacity of the foundation.

PARAMETER	FOUNDATION BACKFILL	BEDROCK	GLACIAL TILL (NATIVE)
Total Natural (moist) Unit Weight ( $\gamma_t$ )	130 pcf <sup>1</sup>	150 pcf	135 pcf
Saturated (buoyant) Unit Weight ( $\gamma_s$ )	68 pcf <sup>1</sup>	-	73 pcf
Friction Coefficient (f)	0.55	0.65	0.45
Active Earth Pressure Coefficient (K <sub>a</sub> )	0.28	-	0.25
Passive Earth Pressure Coefficient (K <sub>p</sub> )	3.57	-	4.0
At Rest Earth Pressure Coefficient (K <sub>o</sub> )	0.47	-	0.41
Uplift Earth Pressure Coefficient (K <sub>u</sub> )	0.92	-	0.94
Friction Angle $(\phi_c)$	34 <sup>0</sup>	37 <sup>0</sup>	36 <sup>0</sup>
Cohesion (c)	0	1000 psi <sup>2</sup>	5.2 psi (750 psf)

<sup>1</sup> Based on 95% compaction of Foundation Backfill by ASTM D1557, Modified Proctor Test Method

<sup>2</sup> For near surface localized shear (i.e., bearing capacity, uplift, and sliding), the rock should be assumed to be cohesionless.

## 5.5.1 Rock Anchors

If additional foundation uplift capacity is needed, rock anchors can be used. Based on the recovered rock core samples at the site, we recommend an ultimate rock-grout bond stress of 120 psi be used in the design of the rock anchors. We recommend that the bonded zone start at a minimum length of 10 feet below the bedrock surface to allow for a free stressing zone. We further recommend that the rock anchors be installed with a Class 1 corrosion protection system. A minimum factor of safety of 2.5 should be used in bond stress calculations. If a 6" diameter hole is used for an anchor, this provides approximately 16 kips of uplift resistance per foot of bonded length.

To ensure adequate rock breakout capacity, we recommend that bond length of the anchors be a minimum of 5 feet. The calculation of the rock breakout was based on a failure cone projected  $45^{\circ}$  from the midpoint of the bonded zone, using a rock unit weight of 150 pcf and a factor of safety of 1.0 on the rock weight resistance. Based on this, we recommend a minimum rock anchor spacing of 5 feet. We recommend a maximum of two rock anchors per footing. In total, the rock anchor tendons should extend a minimum of 15 feet below bedrock surface (free stress zone + bond zone). Centralizers should be used for all installed anchors.

Due to the potential presence of joints in the rock, we recommend that grouting be conducted in two stages. The first stage would comprise pressure grouting in the bond zone to fill in open joints and fractures. Final grouting of the bond zone would occur when pressure grouting had been shown to seal off the bond zone. All installed anchors should be proof tested to a minimum of 120% of the design load, not to exceed 60% of the tensile strength of the steel. We

recommend that the proof testing of all of the anchors be performed in accordance with the Post Tensioning Institute 2014 recommendations.

## 6.0 <u>Construction Consideration</u>

Based on proposed basement floor elevations, we anticipate that shoring will be necessary to excavate for footings and the basement slab. Due to the presence of shallow bedrock, we believe that installed sheeting will need to be braced with either a tie-back system or raker. Steel H-piles socketed into bedrock with timber lagging is also an option. The design of the temporary shoring system should be performed by the shoring contractor.

Based on the groundwater levels observed from our explorations, we do not anticipate that groundwater will be encountered within the building excavations. Diversion and control of surface water should be performed to prevent water flow from adjacent wet areas or from rain or snowmelt from entering the excavations.

All exposed native soil which will be load bearing should be proofrolled with a minimum of 2 passes in each of two perpendicular directions with a 5-ton (operating weight) vibratory roller. All exposed load bearing bedrock surface should be cleared of loose and weathered rock to expose hard, competent bedrock.

All exposed rubble fill below footings should be removed in its entirety down to the native glacial till soil and outwards equal to a distance of the footing width on each side of the footing. Exposed rubble fill below the basement slab should be removed a minimum of 12" below the finished slab elevation. Voids in the rubble fill can be filled with <sup>3</sup>/<sub>4</sub>" crushed stone or flowable fill.

All installed rock anchors will need to be proof tested to 120% of the design uplift load. The procedure for the proof testing is outlined in the Post Tensioning Institute 2014 recommendations.

If controlled blasting is required to construct the building foundations, we recommend that blasting be performed in accordance with the General Blasting Criteria included in Appendix F.

# 7.0 <u>Closure</u>

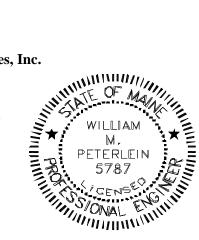
Our recommendations are based on professional judgment and generally accepted principles of geotechnical engineering. Some changes in subsurface conditions from those presented in this report may occur. Should these conditions differ materially from those described in this report, or should building loads and configurations change significantly, SGS should be notified so that we can re-evaluate our recommendations.

We appreciate the opportunity to serve you during this phase of your project. If there are any questions or additional information is required, please do not hesitate to call.

Sincerely, Summit Geoengineering Services, Inc.

Matter Hardesan

Mathew Hardison, EI Geotechnical Engineer

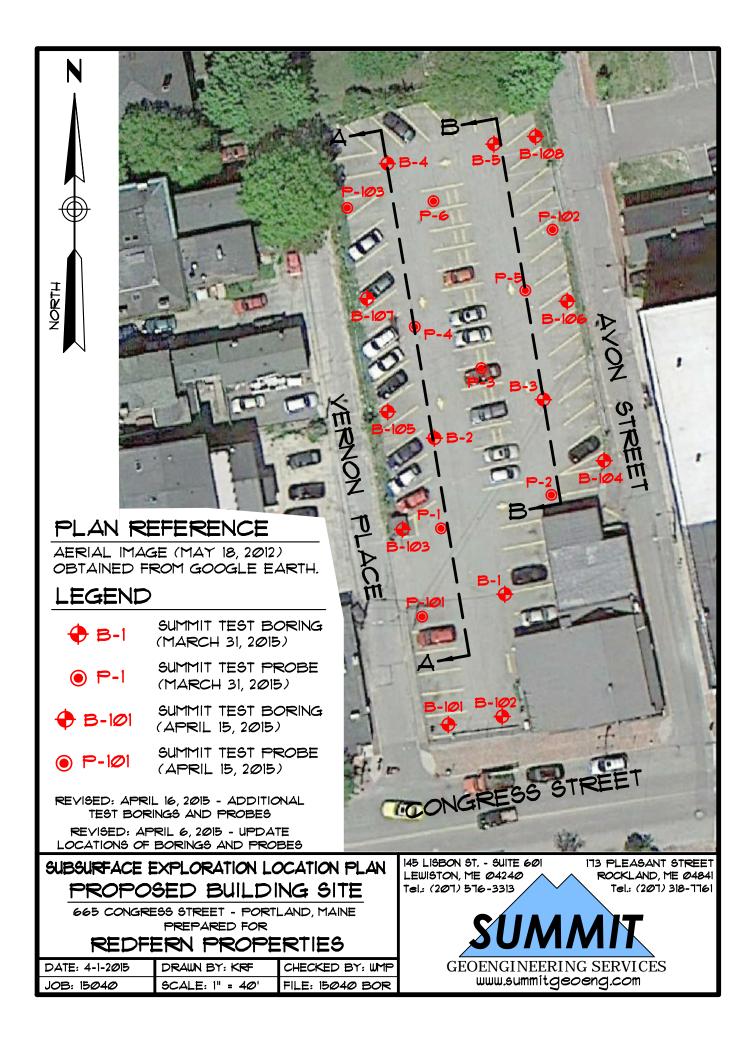


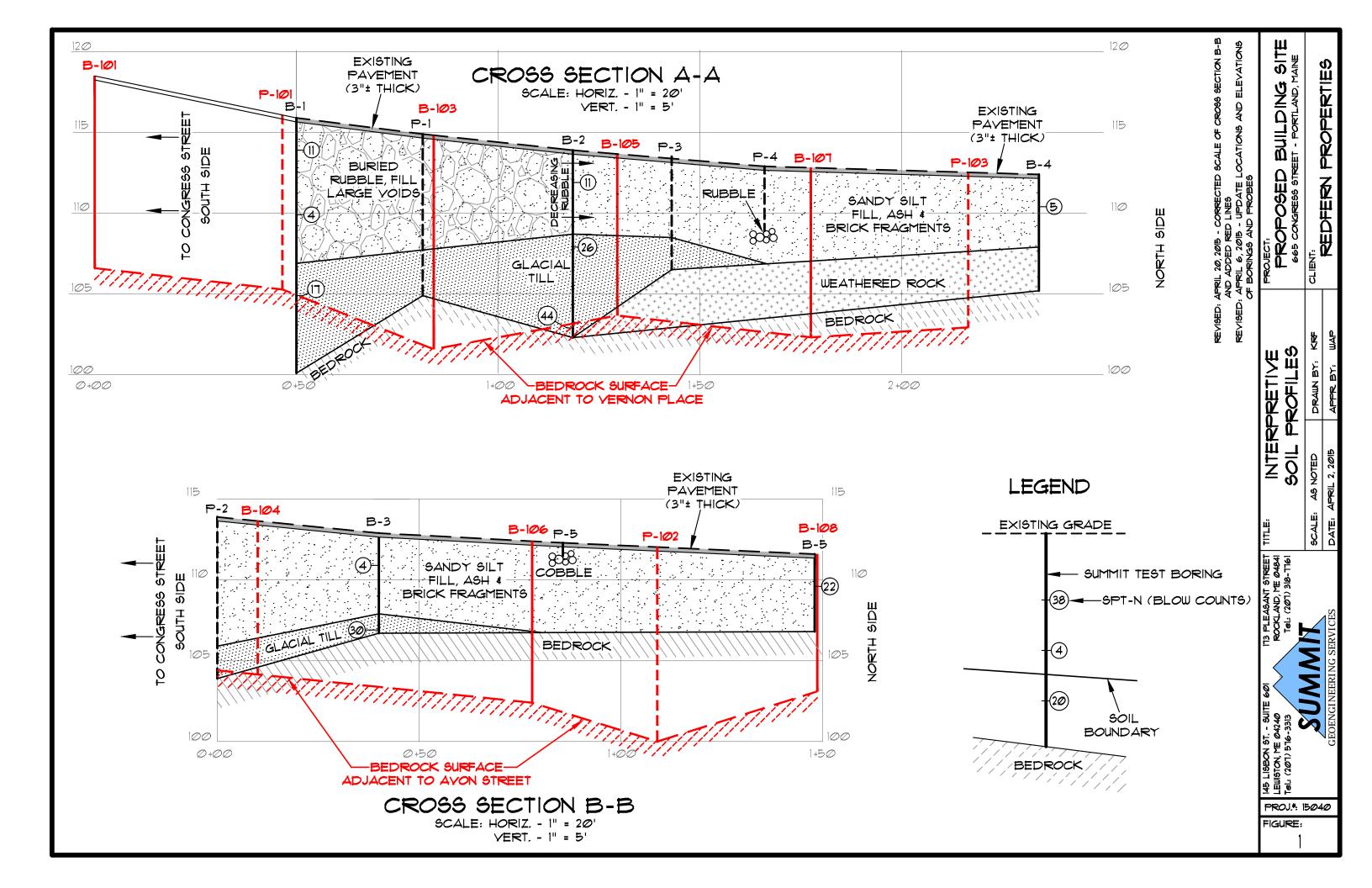
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William M. Peterlein, PE Principal Geotechnical Engineer

# APPENDIX A

# **EXPLORATION PLAN**





# APPENDIX B

# **EXPLORATION LOGS**



# **EXPLORATION COVER SHEET**

The exploration logs are prepared by the geotechnical engineer from both field and laboratory data. Soil descriptions are based upon the Unified Soil Classification System (USCS) per ASTM D2487 and/or ASTM D2488 as applicable. Supplemental descriptive terms for estimated particle percentage, color, density, moisture condition, and bedrock may also be included to further describe conditions.

#### Drilling and Sampling Symbols:

SS = Split Spoon Sample UT = Thin Wall Shelby Tube SSA = Solid Stem Auger HSA = Hollow Stem Auger RW = Rotary Wash SV = Shear Vane PP = Pocket Penetrometer RC = Rock Core Sample Hyd = Hydraulic Advancement of Drilling Rods Push = Direct Push of Drilling Rods WOH = Weight of Hammer WOR = Weight of Rod PI = Plasticity Index LL = Liquid Limit W = Natural Water Content USCS = Unified Soil Classification System

#### Water Level Measurements:

Water levels indicated on the boring logs are the levels measured in the boring at the times indicated. In pervious soils, the indicated elevations are considered reliable groundwater levels. In impervious soils, the accurate determination of groundwater elevations may not be possible, even after several days of observations. Groundwater monitoring wells may be required to record accurate depths and fluctuation.

#### **Gradation Description and Terminology:**

Boulders:	Over 12 inches	Trace:	Less than 5%
Cobbles:	12 inches to 3 inches	Little:	5% to 15%
Gravel:	3 inches to No.4 sieve	Some:	15% to 30%
Sand:	No.4 to No. 200 sieve	Silty, Sandy, etc.:	Greater than 30%
Silt:	No. 200 sieve to 0.005 mm		
Clay:	less than 0.005 mm		

#### Density of Granular Soils and Consistency of Cohesive Soils:

CONSISTENCY OF C	OHESIVE SOILS	DENSITY OF GRANULAR SOILS			
SPT N-value blows/ft	Consistency	SPT N-value blows/ft	<b>Relative Density</b>		
0 to 2	Very Soft	0 to 4	Very Loose		
2 to 4	Soft	5 to 10	Loose		
5 to 8	Firm	11 to 30	Compact		
9 to 15	Stiff	31 to 50	Dense		
16 to 30	Very Stiff	>50	Very Dense		
>30	Hard				

		$\sim$				9	SOIL BORI	NG LOG	Boring #:	B-1	
CITATAT				Project: Proposed Apartment Building			Project #:	15040			
SUMMIT						Location: 665 Congress St.			Sheet: 1 of 1		
	GEOENGINEERING SERVICES City, State: Portland, ME Chkd by:										
Drilling C	co:	Summit Geoen	gineering Serv	vices		Boring Elevation:		115.9'	<u>-</u>		
Driller:		C. Coolidge, P.	0 0			Reference:		Titcomb Associates			
Summit	Staff:	M. Hardison, E				Date started:	3/31/2015	Date Completed:	3/31/2015		
DF	RILLING	METHOD	S	AMPLER				ESTIMATED GROUND W	VATER DEPTH		
Vehicle:	Tracked	1		24" SS		Date	Depth	Elevation	R	eference	
Model:		wer Probe	Diameter:	2"OD/1.5"	ID	3/31/2015	-		None observed		
Method:		" H.S.A.	Hammer:	140 lb							
Hammer	Style: A	Auto	Method:	ASTM D15	86					- · · ·	
Depth			5 11 (0)		N	+	SAMPL		Geological/	Geological	
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	2" to 2 E" of Dov	DESCRIP	TION	Test Data	Stratum PAVEMENT	
1						2" to 2.5" of Pav	ement			0.2'	
· · -	S-1	24/4	1 to 3	6		Dark tan Gravelly	/ SAND, little Sil	t, compact, humid,		FILL	
2				11		SP-SM					
				*				ntally, unable to collect		2.0'	
3_				*		blow counts. Like	ely due to encou	intered rubble			
4						Auger advancem	ent produced n	o cuttings, likely rubble			
1 '-	1	1				fill with large void					
5			_								
ļ ,	S-2	24/3	5 to 7	WH				e pieces, little white Ash			
6_				1		trace Silt, very lo	use, numid, GP				
7				1		t					
-						1					
8						ļ					
9						ł					
9_										9.0'	
10	<u> </u>				<u> </u>	t				GLACIAL TILL	
1 -	S-3	24/20	10 to 12	6				Sand, trace Gravel,			
11				8		compact, humid,	ML		PP = 8,000  to		
12				9 12		+			9,000 psf		
12				12		ł					
13						ł					
-						1					
14						+					
15						+					
15	S-4	24/9	15 to 17	6		Same as above,	slightly mottled				
16				50/3"							
-						End of Exploration	on at 15.8', Auge	er and Spoon refusal		15.8'	
17						ł				BEDROCK	
18						ł					
10						ł					
19						1					
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Granula		Cohesiv		% Comp		NOTES:		etrometer, MC = Moisture C	ontent	Soil Moisture Condition	
Blows/ft.		Blows/ft.	Consistency	ASTM D	02487	4	LL = Liquid Limit	t, PI = Plastic Index		Dry: S = 0%	
0-4	V. Loose		V. soft		<b>-</b>	Bedrock Joints				Humid: $S = 1$ to 25%	
5-10	Loose	2-4	Soft	< 5%		Shallow = 0 to 35	-			Damp: $S = 26 \text{ to } 50\%$	
11-30	Compact		Firm	5-15%		Dipping = $35$ to $55$	-			Moist: $S = 51 \text{ to } 75\%$	
31-50	Dense	9-15	Stiff V Stiff	15-30%		Steep = 55 to 90 c	legrees			Wet: $S = 76 \text{ to } 99\%$	
>50	V. Dense	= 16-30 >30	V. Stiff Hard	> 30%	vvilM	Boulders - diamet	ar > 12 inchas	obbles = diameter < 12 inch	les and > 3 inches	Saturated: S = 100%	
1		>30	пани					$d = \langle No   4 and \rangle No   200, Sil$			
L				1			anu > 110 4, 3d110	a – ≺ אט ד מווע אוע 200, 31	a = 100 200	1	

		$\sim$				S		NG LOG	Boring #:	B-2
						Project: Proposed Apartment Building			Project #:	15040
							Location: 665 Congress St.			1 of 1
							Portland, ME	• •	Sheet: Chkd by:	
Drilling C					Boring Elevation:		114 ft			
Driller:		C. Coolidge, P.				5		Titcomb Associates		
Summit S		M. Hardison, E				Date started:		Date Completed:	3/31/2015	
		METHOD		AMPLER				ESTIMATED GROUND W	ATER DEPTH	
Vehicle:				24" SS		Date	Depth	Elevation		eference
		ver Probe		2"OD/1.5"	ID	3/31/2015	-		None observed	
Method: Hammer		H.S.A.	Hammer: Method:	140 lb ASTM D15	86					
Depth	Jule. P	านเป			00		SAMPL	Г Г	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	+	DESCRIP		Test Data	Stratum
(11.)	110.		Doptil (It)	510113/0	00	2" to 2.5" of Pave			Tost Data	PAVEMENT
1										0.2'
2	S-1	24/20	1 to 3	3				Silt and black/white Ash,		FILL
2_				6 5		loose to compact	, nuzen, SP-SM			
3	E			3		t				
1.						Į				
4_						ł				
5						t				
-	S-2	24/22	5 to 7	10		Same as above				
6				13 13		Olive green slight and Gravel, comp		, little Sand, trace Clay		5.2' GLACIAL TILL
7				13		anu Gravel, comp	acı, uamp, ML			GLACIAL TILL
-						İ				
8_						Į				
9	<u> </u>					ł				
						ł				
10	_			_		1				
11	S-3	24/16	10 to 12	8 12		Same as above, I	neavily mottled	seam at 10.8', dense	PP = 4,000	
11_				32		ł			to 7,000 psf	
12				50/1"		End of Exploratio	n at 11.6', Spoc	on refusal		11.6'
10						ł				BEDROCK
13_						ł				
14						1				
						Į				
15						ł				
16						t				
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18			<u> </u>			ł				
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23						]				
24						ł				
24						t				
25						1				
24						ł				
26_						ł				
27						1				
Granula		Cohesiv		% Comp				etrometer, MC = Moisture Co	ontent	Soil Moisture Condition
Blows/ft. 0-4	Density V. Loose	Blows/ft. <2	Consistency V. soft	ASTM D	2487	Bedrock Joints	LL = LIQUID LIMI	t, PI = Plastic Index		Dry: $S = 0\%$ Humid: $S = 1$ to 25%
0-4 5-10	Loose	<2 2-4	V. Soft	< 5%	Trace	Shallow = 0 to $35$	dearees			Damp: $S = 1 to 25\%$
11-30	Compact	5-8	Firm	5-15%		Dipping = $35$ to $55$	-			Moist: $S = 51$ to 75%
31-50	Dense	9-15	Stiff	15-30%		Steep = $55$ to $90$ d	-			Wet: S = 76 to 99%
>50	V. Dense	16-30	V. Stiff	> 30%	With					Saturated: S = 100%
		>30	Hard					obbles = diameter < 12 inche		
						Gravel = < 3 inch a	and > No 4, Sand	$d = \langle No 4 and \rangle No 200$ , Silt	/Clay = < No 200	

		$\sim$				<b></b>	OIL BORI		Boring #:	B-3
CLIAAAAIT									Project #:	15040
									Sheet: 1 of 1	
									Chkd by:	
						Boring Elevation:				
Driller:		C. Coolidge, P.	0 0			0		Titcomb Associates		
Summit		M. Hardison, E				Date started:		Date Completed:	3/31/2015	
		METHOD	S	AMPLER				ESTIMATED GROUND W	ATER DEPTH	
Vehicle:				24" SS		Date	Depth	Elevation		eference
		ver Probe		2"OD/1.5"	ID	3/31/2015	-		None observed	
Method:		H.S.A.		140 lb	<u>.</u>					
Hammer	Style: A	Auto	Method:	ASTM D15	86		CAMPI	г.	Geological/	Coological
Depth (ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>		SAMPL DESCRIP		Test Data	Geological Stratum
(11.)	NO.	Ten/Rec (in)	Deptil (It)	010003/0	1.400	3" to 3.5" of Pave				PAVEMENT
1										0.3'
	S-1	24/12	1 to 3	4				gment in spoon, small		FILL
2_				11* 4		brick fragment in	spoon tip, loos	e, numia, ML		
3				2		* blow count due	to brick fragme	ent		
-						Į	-			
4_						ļ.				
5						ł				
-	S-2	24/12	5 to 7	12				ce Clay and Gravel,		5' +/-
6				18 50/3"		compact, humid,	ML		PP = 5,000  psf	GLACIAL TILL
7	├			50/3		End of Exploratio	n at 6.2'. Snoor	and Auger refusal	+	6.2'
-							, opoor			BEDROCK
8						ļ				
9						ł				
í-										
10										
11										
- ''										
12										
10										
13_										
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-						1				
27_	<u> </u>					ł				
Granula	ar Soils	Cohesiv	e Soils	% Comp	osition	NOTES:	PP = Pocket Pon	etrometer, MC = Moisture Co	Intent	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	ASTM D				, PI = Plastic Index		Dry: $S = 0\%$
0-4	V. Loose	<2	V. soft			Bedrock Joints	1			Humid: $S = 1$ to 25%
5-10	Loose	2-4	Soft	< 5% 1	race	Shallow = 0 to 35	degrees			Damp: S = 26 to 50%
11-30	Compact	5-8	Firm	5-15%		Dipping = 35 to 55	-			Moist: S = 51 to 75%
31-50	Dense	9-15	Stiff	15-30%		Steep = 55 to 90 d	legrees			Wet: $S = 76 \text{ to } 99\%$
>50	V. Dense	16-30 >30	V. Stiff Hard	> 30%	vvitn	Boulders – diamot	ar > 12 inches	obbles = diameter < 12 inche	as and $> 3$ inchos	Saturated: S = 100%
		~30	naru					$I = \langle No 4 and \rangle No 200, Silt$		
L				1		2.4.0 < 0 molt				I

		$\sim$				S	SOIL BORI	NG LOG	Boring #:	B-4
SUMMIT									Project #:	15040
		SUIVI	IVITY						Sheet: 1 of 1	
		GEOENGINEERI	NG SERVICES						Chkd by:	
Drilling C						Boring Elevation:		112.5 ft	• •	
Driller:		C. Coolidge, P.	0 0			Reference:		Titcomb Associates		
Summit S		M. Hardison, E				Date started:	3/31/2015	Date Completed:	3/31/2015	
DR		METHOD		AMPLER				ESTIMATED GROUND W	ATER DEPTH	
Vehicle:	Tracked			24" SS		Date	Depth	Elevation	R	eference
-		ver Probe	Diameter:	2"OD/1.5"	ID	3/31/2015	-		None observed	
Method:		H.S.A.	Hammer:	140 lb						
Hammer	Style: A	Auto	Method:	ASTM D15	86					
Depth			D 11 (0)		N	-	SAMPL		Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	2.5" of Pavement	DESCRIP	TION	Test Data	Stratum PAVEMENT
1						2.5 OF Pavement	l			0.2'
	S-1	24/10	1 to 3	2		Brown Sandy SIL	T, little fine Gra	vel and black Ash, loose,		FILL
2				2		humid, ML				
3				3		ł				
3				2		Auger cuttings st	now increasing a	ash content with depth		
4						and some brick fi	ragments			
_	S-2	24/2	4.5 to 6.5	50/5"		Weathered rock f		oon tip		
5						Augorality	woothand	k to competent at the set		
6						Augered through	weathered rocl	k to competent refusal		WEATHERED ROCK
<u> </u>						t				
7						<u> </u>				
_						End of Exploratio	on at 7.2', Auger	refusal		7.2'
8						ł				BEDROCK
9						ł				
10										
11						ł				
''-						t				
12						1				
10						ł				
13						ł				
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25	<u> </u>					ł				
25_						ł				
26						t				
						1				
27						ł				
Granula	ar Soile	Cohesiv	e Soils	% Comp	osition	NOTES:	PD - Dockot Don	netrometer, MC = Moisture Co	I	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	ASTM D		NUTES.		t, PI = Plastic Index		Dry: $S = 0\%$
	V. Loose	<2	V. soft	AJTIVIL	-∠TUI	Bedrock Joints	cc – ciquiù ciilli			Humid: $S = 1 \text{ to } 25\%$
5-10	Loose	2-4	Soft	< 5%	Frace	Shallow = 0 to 35	degrees			Damp: $S = 26$ to 50%
	Compact	5-8	Firm	5-15%		Dipping = $35$ to $55$	-			Moist: $S = 51$ to 75%
31-50	Dense	9-15	Stiff	15-30%	Some	Steep = 55 to 90 c	-			Wet: S = 76 to 99%
>50	V. Dense	16-30	V. Stiff	> 30%	With					Saturated: S = 100%
		>30	Hard					cobbles = diameter < 12 inch		
						Gravel = < 3 inch	and > No 4, Sand	$d = \langle No \ 4 \ and \rangle No \ 200, \ Silvert$	t/Clay = < No 200	

		$\sim$				S	OIL BORI	NG LOG	Boring #:	B-5
		CIINA	AAT			Project:	Proposed Apar	tment Building	Project #:	15040
		SUIVI	IVIII				665 Congress S		Sheet:	1 of 1
		GEOENGINEERI	NG SERVICES				Portland, ME		Chkd by:	
Drilling C	0:	Summit Geoen	gineering Serv	vices		Boring Elevation:		112.5 ft		
Driller:		C. Coolidge, P.						Titcomb Associates		
Summit S		M. Hardison, E				Date started:	3/31/2015	Date Completed:	3/31/2015	
		METHOD		AMPLER				ESTIMATED GROUND W		
Vehicle:				24" SS	10	Date	Depth	Elevation		eference
		ver Probe		2"OD/1.5"	ID	3/31/2015	-		None observed	
Method: Hammer			Hammer: Method:	140 lb ASTM D15	86					
Depth	Style. P	lato	Methou.	ASTNI DIG	00		SAMPI	F	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	ł	DESCRIP		Test Data	Stratum
. ,						2.5" of Pavement				PAVEMENT
1										0.2'
2	S-1	24/8	1 to 3	15 16		Dark brown to bl and white Ash, N		, little Gravel and black		FILL
<sup>2</sup> -				6		and white Ash, w	IL			
3				2		1				
1.						ļ				
4						Dense drilling at	4 8'			
5	S-2	24/1	4.8 to 6.8	50/3"		Rock in spoon tip				
1 -								n and Auger refusal		4.8'
6						ļ				BEDROCK
7						ł				
1 '-						t				
8						1				
9						+				
9_						ł				
10						+				
						1				
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_						1				
27_						ł				
Granula	ar Soile	Cohesiv	e Soils	% Comp	osition	NOTES:	PP - Dockot Don	netrometer, MC = Moisture Co	I	Soil Moisture Condition
Blows/ft.		Blows/ft.	e Solis Consistency	% Comp ASTM E		NUTES.		t, PI = Plastic Index	JIICHI	Dry: $S = 0\%$
	V. Loose	<2	V. soft	AJ TIVI L	2-107	Bedrock Joints				Humid: $S = 1$ to 25%
5-10	Loose	2-4	Soft	< 5%	Frace	Shallow = 0 to $35$	degrees			Damp: $S = 26$ to 50%
	Compact	5-8	Firm	5-15%		Dipping = 35 to 55	-			Moist: S = 51 to 75%
31-50	Dense	9-15	Stiff	15-30%		Steep = 55 to 90 c	-			Wet: S = 76 to 99%
>50	V. Dense		V. Stiff	> 30%	With					Saturated: S = 100%
1		>30	Hard					cobbles = diameter < 12 inch		
						Gravel = < 3 inch	and > No 4, Sand	$d = \langle No 4 and \rangle No 200$ , Sil	t/Clay = < No 200	

		$\sim$				S		NG LOG	Boring #:	B-101
1		CIINA	AALT				Proposed Apart		Project #:	15040
		SUIVI	IVIIX				665 Congress S		Sheet:	1 of 1
L		GEOENGINEERI	NG SERVICES				Portland, ME		Chkd by:	
Drilling C	co:	Great Works Te	est Boring			Boring Elevation:		118.5 ft		
Driller:		Jeff Lee						Titcomb Associates		
Summit		M. Hardison, E				Date started:	4/15/2015	Date Completed:	4/15/2015	
		METHOD		AMPLER			_	ESTIMATED GROUND \	1	
Vehicle:			Length:	24" SS	10	Date	Depth	Elevation		eference
	Mobile E	3-53 Stem Auger	Diameter: Hammer:	2"OD/1.5" 140 lb	ID	4/15/2015	-		None observed	
Hammer			Method:	ASTM D15	86					
Depth	5.5.0. 1						SAMPL	LE	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	+	DESCRIP		Test Data	Stratum
						3" Pavement				PAVEMENT
1_	S-1	24/4	0.5 to 2.5	4		Brown Silty SAND	), loose, humid,	SM		0.25'
2				3		ł				FILL
<b>_</b>				3		ł				
3						1				
						Dessible		1 during delline		
4_						Possible rubble e	ncountered at 4	auring drilling		
5						ł				
-	S-2	24/4	5 to 7	7		Brown Silty SAND	), trace Gravel,	compact humid, SM		
6				7		ł				
7				7		ł				
-						1				
8						ļ				
9						ł				
						1				
10						1				
11	S-3	24/12	10 to 12	4 8		Dark olive green dense/very stiff,		and Gravel, trace Clay,	PP = *1,000 to	10.0' +/- GLACIAL TILL
11_	-			8 30		uense/very stiff,	signity mottled	, namia, iviL	PP = *1,000 to *3,000 psf	GLACIAL TILL
12	L			50/5				crack, low clay content	0,000 p3i	
I						End of Exploratio	n at 11.9', Auge	er and Spoon refusal		11.9'
13						ł				BEDROCK
14						ł				
-						1				
15						ļ				
16						ł				
-						1				
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27						ł				
21-						ł				
Granula	ar Soils	Cohesiv	e Soils	% Comp	osition	NOTES:	PP = Pocket Pen	netrometer, MC = Moisture C	Content	Soil Moisture Condition
Blows/ft.	Density	Blows/ft.	Consistency	ASTM D			LL = Liquid Limit	t, PI = Plastic Index		Dry: S = 0%
0-4	V. Loose		V. soft			Bedrock Joints				Humid: S = 1 to 25%
5-10	Loose	2-4	Soft	< 5%		Shallow = 0 to 35	-			Damp: S = 26 to 50%
11-30	Compact		Firm	5-15%		Dipping = $35$ to $55$	-			Moist: $S = 51 \text{ to } 75\%$
31-50 >50	Dense	9-15	Stiff V Stiff	15-30%		Steep = $55$ to $90$ d	legrees			Wet: $S = 76 \text{ to } 99\%$
>50	V. Dense	16-30 >30	V. Stiff Hard	> 30%	vvilli	Boulders = diamote	er > 12 inchae (	obbles = diameter < 12 incl	hes and $> 3$ inches	Saturated: S = 100%
		/30	naru					$d = \langle No   4 \text{ and } \rangle No   200, Si$		
L										1

		$\sim$				S	OIL BORI	NG LOG	Boring #:	B-102		
		CIIN A	INALT				Proposed Apar		Project #:	15040		
1		SUIVI	IVIIA				665 Congress S	*	Sheet:	1 of 1		
		GEOENGINEERI					Portland, ME		Chkd by:			
Drilling C		Great Works Te	est Boring			Boring Elevation:		118.7 ft				
Driller:		Jeff Lee						Titcomb Associates	4/45/2015			
Summit S		M. Hardison, E				Date started:	4/15/2015	Date Completed:	4/15/2015			
DR Vehicle:		METHOD		AMPLER 24" SS		Date	Depth	ESTIMATED GROUND W Elevation		eference		
Model:				24 33 2"OD/1.5"	ID	4/15/2015	-		None observed			
		Stem Auger		140 lb								
Hammer			Method:	ASTM D15	86					1		
Depth	NL.	Den (Den (L.)	Davits (0)	hla - 147	NI	ł	SAMPL		Geological/	Geological		
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	3" Pavement	DESCRIP	IIUN	Test Data	Stratum PAVEMENT		
1	S-1	24/4	0.5 to 2.5	4			SAND, little Gra	vel, Gravel pieces in		0.25'		
				5		spoon tip, loose,				FILL		
2_				5 3		ł						
3				5		Rubble fill, large	voids apparent	from open hole inpection	1			
						Auger encountered refusal at 4.9' during drilling. Moved						
4						over 1' and attempted to drill past, refusal encountered						
5						in second hole at 3.2						
-						End of Exploration at 4.9', Auger refusal on rubble				4.9'		
6						ł						
7						t	1					
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8						ł						
9						ł						
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26						ł						
20						t						
27						Į						
Granula	ar Soile	Cohesiv	e Soils	% Comp	osition	NOTES:	PP - Dockot Dom	netrometer, MC = Moisture Co	Intent	Soil Moisture Condition		
Granula Blows/ft.		Blows/ft.	Consistency	% Comp ASTM D		NUTES.		t, PI = Plastic Index	mem	Dry: $S = 0\%$		
	V. Loose	<2	V. soft			Bedrock Joints				Humid: $S = 1$ to 25%		
5-10	Loose	2-4	Soft	< 5%	race	Shallow = 0 to 35	degrees			Damp: S = 26 to 50%		
	Compact	5-8	Firm	5-15%		Dipping = 35 to 55	-			Moist: S = 51 to 75%		
31-50	Dense	9-15	Stiff	15-30%		Steep = 55 to 90 d	legrees			Wet: S = 76 to 99%		
>50	V. Dense		V. Stiff Hard	> 30%	With	Bouldors - dismit	or > 10 inchos	abblas - diamatar - 12 i	and > 2 inches	Saturated: S = 100%		
		>30	Hard					cobbles = diameter < 12 inch d = < No 4 and >No 200, Silt				
L				1			and - NO +, JdH		J = 100 200	1		

		$\sim$				S	SOIL BORI	NG LOG	Boring #:	B-103
		SIINA	MANT			Project:	Proposed Apar	tment Building	Project #:	15040
		SUIVI	IVIII			Location:	665 Congress S	St.	Sheet:	1 of 1
		GEOENGINEERI	NG SERVICES			City, State:	Portland, ME		Chkd by:	
Drilling C	co:	Great Works Te	est Boring			Boring Elevation:		115.0 ft		
Driller:	o. ~	Jeff Lee				Reference:		Titcomb Associates		
Summit S		M. Hardison, E				Date started:	4/15/2015	Date Completed:	4/15/2015	
		METHOD		AMPLER		Detr	Dent	ESTIMATED GROUND W		oforonoo
Vehicle: Model:			Length: Diameter:	24" SS 2"OD/1.5"	חו	Date 4/15/2015	Depth	Elevation	R None observed	eference
		Stem Auger	Hammer:	2 0D/1.5 140 lb	טו	4/15/2015	-			
Hammer				ASTM D15	86					
Depth						Ì	SAMPI	E	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	[	DESCRIP	TION	Test Data	Stratum
-	0.1	0.1/0	0.5.1.0.5			3" Pavement	CANE	a alla lana di 251 A		PAVEMENT
1_	S-1	24/8	0.5 to 2.5	4				e silt, large brick fragment ent in spoon tip, loose,	[	0.25' FILL
2				7		humid, SP	ne, brick frayffit	2111 11 Spool 11p, 10030,		
-				9		1				
3						ł				
4						ł				
_						İ				
5	0.5	0.1/2	<b>F</b> · -			I				
6	S-2	24/6	5 to 7	5		same as above, r	no brick fragme	nt, some white Ash		
0	1			15		ł				
7				15		1				
0						ł				
8_	-					ł				
9						<u>†</u>				
						 				9.0' +/-
10	S-3	24/20	10 to 12	14		Olive green SILT	little Gravel S	and, and Clay, cobble	PP = 6,000 to	GLACIAL TILL
11	5-5	27120	101012	24		pieces fro 10.5 to			> 9,000 to	
_				20		1				
12				20		ł				
13						ł				
						İ				
14						ł				
15						End of Exploratio	n at 14.5' Δυσ	er refusal		14.5'
10										BEDROCK
16						]				
17	L					ł				
· · · -						t				
18						1				
19						ł				
19						ł				
20						1				
01						ł				
21_						ł				
22						İ				
						ł				
23						ł				
24						t				
-						]				
25						ł				
26						ł				
_						1				
27						ł				
Granula	ar Soile	Cohesiv	a Soils	% Comp	osition	NOTES:	PP - Pockot Pop	etrometer, MC = Moisture Co	Intent	Soil Moisture Condition
Blows/ft.			Consistency	ASTM D		NOTES.		t, PI = Plastic Index	Jinefit	Dry: $S = 0\%$
0-4	V. Loose		V. soft	AGTIN L	,	Bedrock Joints		.,		Humid: $S = 1 \text{ to } 25\%$
5-10	Loose	2-4	Soft	< 5%	Frace	Shallow = 0 to $35$	degrees			Damp: S = 26 to 50%
11-30	Compact	t 5-8	Firm	5-15%	Little	Dipping = 35 to 55	degrees			Moist: S = 51 to 75%
31-50	Dense	9-15	Stiff	15-30%		Steep = 55 to 90 c	legrees			Wet: S = 76 to 99%
>50	V. Dense		V. Stiff	> 30%	With					Saturated: S = 100%
		>30	Hard					obbles = diameter < 12 inch		
						Gravel = < 3 inch	and > No 4, Sand	$d = \langle No 4 and \rangle No 200$ , Silt	t/ciay = < No 200	

		$\sim$				S	OIL BORI	NG LOG	Boring #:	B-104
1		SUM	TINA				Proposed Apart		Project #:	15040
		SUIVI	IVIIX				665 Congress S	Ų	Sheet:	1 of 1
		GEOENGINEERI	NG SERVICES				Portland, ME		Chkd by:	
Drilling C	Co:	Great Works To	est Boring			Boring Elevation:		113.1 ft		
Driller:		Jeff Lee				U U		Titcomb Associates		
Summit	Staff:	M. Hardison, E	.I.			Date started:		Date Completed:	4/15/2015	
DF	RILLING	METHOD	S	AMPLER				ESTIMATED GROUND V	VATER DEPTH	
	Tracked		Length:	24" SS		Date	Depth	Elevation		eference
	Mobile B		Diameter:	2"OD/1.5"	ID	4/15/2015	-		None observed	
		Stem Auger	Hammer:	140 lb	~ ~					
	Style: F	4&C	Method:	ASTM D15	86		SAMPL		Geological/	Geological
Depth (ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	ł	DESCRIP		Test Data	Stratum
(11.)	NO.	Pen/Rec (III)	Deptil (It)	DIOWS/0	1160	4" Pavement	DESCRIP		Test Data	PAVEMENT
1										0.3'
-						Augered to 5', re	latively easy dri	Illing (no rubble)		FILL
2										
3						ł				
						ł				
4						1				
_						ł				
5_	S-1	24/18	5 to 7	7		Olive areen SILT	little Gravel Sa	and, and Clay, mottled,	PP = 5,000 to	5.0' +/-
6		2010	5.07	7				e pieces at 6.5', ML	7,000 psf	GLACIAL TILL
_				17		]				
7_				23		ł				
8						ł				
-										
9										8.5'
10						End of Exploratio	n at 0 E' Augor	rofucal		WEATHERED ROCK 9.5'
10_						End of Exploratio	n at 9.5 , Auger	reiusai		9.5 BEDROCK
11										SEBILOON
						]				
12						-				
13						-				
-						İ				
14										
15						ł				
15						ł				
16										
17						ł				
17						ł				
18						t				
1						Į				
19_						ł				
20						ł				
-						1				
21						ł				
22						ł				
	1					t				
23						Į				
24						ł				
<sup>24</sup>						ł				
25						1				
~						ł				
26						ł				
27	-					t				
						<u> </u>				
Granula		Cohesiv		% Comp		NOTES:		etrometer, MC = Moisture C	ontent	Soil Moisture Condition
Blows/ft.	-	Blows/ft.	Consistency	ASTM D	2487		LL = Liquid Limit	t, PI = Plastic Index		Dry: $S = 0\%$
0-4	V. Loose		V. soft	===	F	Bedrock Joints				Humid: $S = 1 \text{ to } 25\%$
5-10 11-30	Loose	2-4 5.8	Soft	< 5% ] 5 15%		Shallow = 0 to 35 Dipping = $35$ to $55$	-			Damp: $S = 26 \text{ to } 50\%$
11-30 31-50	Compact Dense	5-8 9-15	Firm Stiff	5-15% 15-30%		Dipping = $35$ to $55$ Steep = $55$ to $90$ d	-			Moist: $S = 51$ to 75% Wet: $S = 76$ to 99%
>50	V. Dense		V. Stiff	> 30%		5100p - 55 10 90 0	icgrees			Saturated: S = 100%
- 00		>30	Hard	- 5070		Boulders = diamete	er > 12 inches, C	obbles = diameter < 12 inch	nes and > 3 inches	Sataratoa. 5 = 10076
1								$d = \langle No   4 \text{ and } \rangle No   200, Sil$		
						•			-	

		$\sim$				S	OIL BORI	NG LOG	Boring #:	B-105
1		CI IN A	AALT				Proposed Apar		Project #:	15040
		SUIVI	IVIIX				665 Congress S		Sheet:	1 of 1
		GEOENGINEERIN	IG SERVICES				Portland, ME		Chkd by:	
Drilling C	o:	Great Works To	est Boring			Boring Elevation:		113.8 ft		
Driller:		Jeff Lee	5			Reference:	Site Survey by	Titcomb Associates		
Summit :		M. Hardison, E	.l			Date started:		Date Completed:	4/15/2015	
DF	RILLING	METHOD		SAMPLER				ESTIMATED GROUND \	WATER DEPTH	
Vehicle:			J	24" SS		Date	Depth	Elevation		eference
-	Mobile B			2"OD/1.5"ID	)	4/15/2015	-		None observed	
Method:		ed Wash		140 lb						
Hammer	Style: F	8&C	Method:	ASTM D1586	)		6 A M PI		Caslariaal/	Cooloriaal
Depth (ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>		SAMPL DESCRIP		Geological/ Test Data	Geological Stratum
(11.)	NO.	Pen/Rec (III)	Deptil (It)	DIOWS/0	1160	3" Pavement	DESCRIP	TION	Test Data	PAVEMENT
1										0.25'
_						Augered to refus	al for Rock Core	9		
2_										
3										
4						]				
5	<u> </u>					{				
°-						1				
6						1				
1						]				
7_						4				
8						1				
9_						ļ				0.11/
10	<u> </u>	ROO	ck core da	ТА		{				9.1' +/- WEATHERED ROCK
	RUN	DEPTH	RUN	RECOVERY	RQD					10.0'
11	C-1a	10 to 13.3	40"	70%				ly spaced vertical joints,		BEDROCK
10						very hard, light to	o medium gray	SCHIST		
12									F	
13										
-	C-1b	13.3 to 15	20"	100%	80%	Same as above, i	moderately space	ced joints		
14										
15										
10						End of Exploratio	n at 15.0', rock	core terminated		15.0'
16										
17										
1/_										
18										
1						]				
19						{				
20	<u> </u>					1				
-						]				
21						4				
22	<u> </u>					1				
						1				
23						]				
24	<u> </u>					{				
24						1				
25						]				
<u> </u>										
26						{				
27						1				
						1				
Granula		Cohesive	Soils	% Compo		NOTES:	PP = Pocket Pen	etrometer, MC = Moisture C	Content	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	ASTM D2	2487		LL = Liquid Limit	t, PI = Plastic Index		Dry: S = 0%
0-4	V. Loose	<2	V. soft			Bedrock Joints				Humid: $S = 1$ to 25%
5-10	Loose	2-4	Soft	< 5% Tr		Shallow = 0 to 35	-			Damp: $S = 26 \text{ to } 50\%$
11-30	Compact	5-8	Firm	5-15% L		Dipping = $35$ to $55$	-			Moist: $S = 51 \text{ to } 75\%$
31-50 >50	Dense V. Dense	9-15 16-30	Stiff V. Stiff	15-30% S > 30% V		Steep = 55 to 90 c	iegrees			Wet: $S = 76$ to 99% Saturated: $S = 100\%$
200	V. Delise	>30	V. Still Hard	- 30 /0 V	TVILII	Boulders = diameter	er > 12 inches C	obbles = diameter < 12 incl	hes and $> 3$ inches	3a(u)a(cu, 3 = 100%)
1		~ 50	, la u					$d = \langle No   4 \text{ and } \rangle No   200, Si$		
1						0	17 6411			1

		$\sim$				S	OIL BORI	NG LOG	Boring #:	B-106
		CI IN A	AALT			Project:	Proposed Apart	ment Building	Project #:	15040
		SUIVI	IVIIX				665 Congress S	J J	Sheet:	1 of 1
		GEOENGINEERIN	NG SERVICES			City, State:	Portland, ME		Chkd by:	
Drilling C	0:	Great Works To	est Boring			Boring Elevation:		112.0 ft		
Driller:		Jeff Lee				Reference:	Site Survey by	Titcomb Associates		
Summit S		M. Hardison, E				Date started:		Date Completed:	4/15/2015	
		METHOD		SAMPLER				ESTIMATED GROUND V		
Vehicle:				24" SS		Date	Depth	Elevation		eference
-	Mobile B			2"OD/1.5"ID		4/15/2015	-		None observed	
Method:		sed Wash		140 lb					+	
Hammer	Style: F	KAL	Method:	ASTM D1586	)			r	Coolerial	Coolerial
Depth	No	Don/Doo (ir)	Dopth (ft)	blows///	N	4	SAMPL		Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	3" Pavement	DESCRIPT		Test Data	Stratum PAVEMENT
1						5 Tavement				0.25'
· · -				-		Augered to refuse	al for Rock Core			
2						]				
2						4				
3_						Dense drilling fro	m approximatel	y 2' to 8', frequent		
4						rubble or cobble		J = to o, nequent		
_						]				
5										
L						{				
6						1				
7						1				
I . T						]				
8_						{				
9	<u> </u>					1				
_						1				
10			CK CORE DA		I					
11	RUN	DEPTH	RUN 60"	RECOVERY 66%	RQD	Modoratolywart	arad you thin	w chacod laints work	1	10.0' BEDROCK
11_	C-2	10 to 15	60	60%	33%	hard light gray to		ly spaced joints, very		BEDRUCK
12						nara ngint gruy to				
						most fractures ra	nge from 45° to	vertical		
13						4			A	
14	<u> </u>					1				
- ''						1				
15						]		_	10	
17	C-3	15 to 19	48"	96%	65%	Same as above, r	most joints and	fractures are vertical		
16									-	
17						1			2	
_										
18						4			1	
19						1				
l ''-						End of Exploratio	n at 19.0', rock	core terminated		19.0'
20						1				
0.1						4				
21_						1				
22						1				
						]				
23_						4				
24						1				
27						1				
25						]				
27						4				
26_						1				
27						1				
						1				
Granula	ar Soils	Cohesive	e Soils	% Compo	sition	NOTES:	PP = Pocket Pen	etrometer, MC = Moisture C	ontent	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	ASTM D2		ļ	LL = Liquid Limit	, PI = Plastic Index		Dry: S = 0%
0-4	V. Loose		V. soft			Bedrock Joints				Humid: $S = 1$ to 25%
5-10	Loose	2-4	Soft	< 5% Tr		Shallow = 0 to 35	-			Damp: $S = 26 \text{ to } 50\%$
11-30	Compact	5-8	Firm	5-15% L		Dipping = $35$ to $55$	-			Moist: $S = 51 \text{ to } 75\%$
31-50	Dense	9-15	Stiff	15-30% S		Steep = 55 to 90 d	legrees			Wet: $S = 76 \text{ to } 99\%$
>50	V. Dense	16-30 >30	V. Stiff Hard	> 30% \	ייונו	Boulders – diamote	r > 12 inches C	obbles = diameter < 12 inch	hes and $> 3$ inchos	Saturated: S = 100%
		/30	naiù					$I = \langle No \ 4 \text{ and } \rangle No \ 200, Sil$		
							anu - NU 4, Sano	a – ≤ inu 4 ariu ≥inu 200, Sli	u olay - < NU 200	

		$\wedge$				S	OIL BORI	NG LOG	Boring #:	B-107
		SIIM	IN ALT				Proposed Apar		Project #:	15040
		SUIVI	IVIIX				665 Congress S		Sheet:	1 of 1
		GEOENGINEERI	NG SERVICES				Portland, ME		Chkd by:	
Drilling C	co:	Great Works T	est Boring			Boring Elevation:		112.9 ft		
Driller:		Jeff Lee	5			5	Site Survey by	Titcomb Associates		
Summit	Staff:	M. Hardison, E	.l.			Date started:		Date Completed:	4/15/2015	
		METHOD		AMPLER				ESTIMATED GROUND \	WATER DEPTH	
Vehicle:			Length:	24" SS		Date	Depth	Elevation		eference
	Mobile E		Diameter:	2"OD/1.5"	ID	4/15/2015	-		None observed	
Method: Hammer		Stem Auger	Hammer: Method:	140 lb ASTM D15	86					
Depth	June. 1		METHOU.	AUTO IN LO	00		SAMPI	F	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	ł	DESCRIP		Test Data	Stratum
(10.)	110.		Doptil (ity	510113/0	00	4" Pavement	BEGGI		Tost Data	PAVEMENT
1	S-1	24/6	0.5 to 2.5	3			ly SILT, trace A	sh and Brick fragments,		0.3'
2				4		loose, dry, ML				FILL
2_				4 3		ł				
3						1				
I .						Į				
4_						ł				
5						ł				
-	S-2	24/24	5 to 7	7		Olive green SILT,	, slight mottling	, litte fine Sand, trace		5.0' +/-
6_				10 14		Gravel and Clay,	compact/very s	tiff, humid, ML		GLACIAL TILL
7				14		ł				
-						1				
8						ļ				
9						ł				
7-										9.0' +/-
10								gering, drilled 1.5' into		WEATHERED ROCK
11						rock to hard refu End of Exploratio		ar rafusal		10.5'
11_						LING OF EXPLORATIO	n at iv.5 , Auge	ei i ei usai		BEDROCK
12						1				
						ļ				
13						ł				
14					L	İ				
· · · ·						Į				
15						ł				
16						ł				
-						1				
17_						ł				
18						ł				
-						1				
19_						ł				
20						ł				
20					L	İ				
21						ļ				
22						ł				
						t				
23						Į				
24						ł				
<sup>24</sup> -						ł				
25						Į				
24						ł				
26_						ł				
27						1				
						NOTES				
Granula Blours /ft		Cohesiv Blows /ft		% Comp		NOTES:		etrometer, MC = Moisture C	Content	Soil Moisture Condition
Blows/ft. 0-4	V. Loose	Blows/ft.	Consistency V. soft	ASTM D	02487	Bedrock Joints	LL = LIQUID LIMI	t, PI = Plastic Index		Dry: $S = 0\%$ Humid: $S = 1$ to 25%
0-4 5-10	Loose	2-4	V. SOIT	< 5%	Trace	Shallow = 0 to 35	dearees			Humid: $S = 1 to 25\%$ Damp: $S = 26 to 50\%$
11-30	Compact		Firm	5-15%		Dipping = $35$ to $55$	-			Moist: $S = 51$ to 75%
31-50	Dense	9-15	Stiff	15-30%		Steep = $55$ to $90$ c	-			Wet: S = 76 to 99%
>50	V. Dense	16-30	V. Stiff	> 30%	With					Saturated: S = 100%
		>30	Hard					cobbles = diameter < 12 incl		
L						Gravel = < 3 inch	and > No 4, Sand	$d = \langle No \ 4 \ and \rangle No \ 200, \ Si$	ilt/Clay = < No 200	

		$\wedge$				S		NG LOG	Boring #:	B-108
		SIIM	IN ALT				Proposed Apar		Project #:	15040
		20111					665 Congress S		Sheet:	1 of 1
		GEOENGINEERI	NG SERVICES				Portland, ME		Chkd by:	
Drilling C	co:	Great Works T	est Boring			Boring Elevation:		110.2 ft		
Driller:		Jeff Lee						Titcomb Associates		
Summit		M. Hardison, E		AND: 55		Date started:	4/15/2015	Date Completed:	4/15/2015	
-		METHOD		AMPLER		Detr	Dent	ESTIMATED GROUND		oforonoo
Vehicle: Model:	Mobile E		Length: Diameter:	24" SS 2"OD/1.5"	ID	Date 4/15/2015	Depth	Elevation	None observed	eference
		Stem Auger	Hammer:	140 lb	<u>ч</u>	T/ 13/2013	-			
Hammer			Method:	ASTM D15	86	<u> </u>				
Depth		-					SAMPL		Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>		DESCRIP	TION	Test Data	Stratum
1	S-1	24/10		8		4" Pavement	sand little si	lt, compacy, humid,		PAVEMENT 0.3'
'-	5-1	24/10		9		SW-SM				0.5
2				8		large Brick fragm	ent and white A	ASH		1.1' +/-
3				3		ł				FILL
- <sup>-</sup>						ł				
4						1				
5						ł				
5	S-2	24/4		*50/6"			elly SAND, cobb	ole piece in spoon tip,		
6						humid, SP	3			
7						* high blow coun	t due to cobble	in fill		
í –	L					t				
8_					[	Į				
9	L					End of Exploratio	n at 8.5'. Auger	refusal		8.5'
· -							n at 0.0 , nager	lorusui		BEDROCK
10						ļ				
11						ł				
-						1				
12						ļ				
13	L					ł				
_						1				
14						ł				
15						ł				
-						1				
16_						ł				
17						ł				
						1				
18						ł				
19						ł				
-						1				
20_						ł				
21						ł				
-						1				
22_						ł				
23	<u> </u>					ł				
-						1				
24						ł				
25						ł				
-						1				
26						ł				
27						ł				
Granula Diauna (fit		Cohesiv		% Comp		NOTES:		etrometer, MC = Moisture (	Content	Soil Moisture Condition
Blows/ft. 0-4	Density V. Loose	Blows/ft.	Consistency V. soft	ASTM D	02487	Bedrock Joints	LL = LIQUID LIMI	t, PI = Plastic Index		Dry: $S = 0\%$ Humid: $S = 1$ to 25%
0-4 5-10	Loose	2-4	V. SOIT	< 5%	Frace	Shallow = 0 to $35$	degrees			Damp: $S = 1625\%$
11-30	Compact		Firm	5-15%		Dipping = $35$ to $55$	-			Moist: $S = 51$ to 75%
31-50	Dense	9-15	Stiff	15-30%		Steep = 55 to 90 d	-			Wet: S = 76 to 99%
>50	V. Dense		V. Stiff	> 30%	With					Saturated: S = 100%
1		>30	Hard					abbles = diameter < 12 inc		
L						Graver = < 3 inch	anu > No 4, Sano	$d = \langle No 4 and \rangle No 200, S$	ont/Clay = < No 200	

		$\wedge$					SOIL PRO	BE LOG	Boring #:	P-1
		SUM	NANT			Project:	Proposed Apar	tment Building	Project #:	15040
1		00111				Location:	665 Congress		Sheet:	1 of 1
		GEOENGINEERI				City, State:	Portland, ME		Chkd by:	
Drilling C		Summit Geoen	• •	vices		Boring Elevation:		114.9 ft		
Driller: Summit		C. Coolidge, P. M. Hardison, E				Reference: Date started:	Site Survey by 3/31/2015	Titcomb Associates Date Completed:	3/31/2015	
		METHOD		AMPLER			5/51/2010	ESTIMATED GROUND V		
Vehicle:			Length:	N/A		Date	Depth	Elevation		Reference
	AMS Pov	ver Probe	Diameter:	N/A		3/31/2015				
Method:		H.S.A.	Hammer:	N/A						
Hammer	Style: A	Auto	Method:	N/A					Coolertail	Coolestert
Depth (ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/	6" N <sub>60</sub>	-	SAMPI DESCRIP		Geological/ Test Data	Geological Stratum
(11.)	NO.		Deptil (It)	PROB		2.5" of Pavemen		TION	Test Data	PAVEMENT
1										0.2'
2						4				FILL
2_						1				
3						Dense drilling at	3', likely rubble			
4					_		ent nroduced n	o cuttings, large voids		
4-						apparent from h				
5						1		-		
6					_	4				
<u> </u>		L				1				
7						1				
8				-		4				
						1				
9_	[					Ţ				
10						4				9.0' +/- WEATHERED ROCK
						End of Probe at	10.0', Auger Ret	fusal		10.0'
11						]				BEDROCK
12						+				
						1				
13						4				
14						+				
-						1				
15	<u> </u>					4				
16						+				
_						1				
17					_	4				
18	<u> </u>	ļ				1				
						]				
19_						4				
20						1				
- 21	-					4				
21_						+				
22						1				
23						4				
23						1				
24						1				
25						4				
25						1				
26						]				
27						+				
						<u>†</u>				
Granula		Cohesiv			mposition	NOTES:		netrometer, MC = Moisture C	Content	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	AST	M D2487	De dre de la tra	LL = Liquid Limi	t, PI = Plastic Index		Dry: $S = 0\%$
0-4 5-10	V. Loose Loose	<2 2-4	V. soft Soft		% Trace	Bedrock Joints Shallow = 0 to 35	dearees			Humid: $S = 1$ to 25% Damp: $S = 26$ to 50%
5-10 11-30	Compact	2-4 5-8	Firm		% Trace 5% Little	Dipping = 35  to  55	-			Moist: $S = 51$ to 75%
31-50	Dense	9-15	Stiff		0% Some	Steep = $55$ to $90$ c	-			Wet: S = 76 to 99%
	V. Dense		V. Stiff		0% With		-			Saturated: S = 100%
		>30	Hard					Cobbles = diameter < 12 inch		
						Gravel = < 3 inch	and > No 4, San	$d = \langle No \ 4 \ and \rangle No \ 200, Si$	It/Clay = < No 200	

		$\wedge$						SOIL PRO	BE LOG	Boring #:	P-2
		SUM	MAIT				Project:	Proposed Apar		Project #:	15040
		~~~~					Location:	665 Congress		Sheet:	1 of 1
		GEOENGINEERI					City, State:	Portland, ME		Chkd by:	
Drilling C		Summit Geoen	0 0	vices			Boring Elevation:		113.9 ft		
Driller:		C. Coolidge, P.					Reference:		Titcomb Associates	0/04/0015	
Summit S		M. Hardison, E		AMPLE	D		Date started:	3/31/2015	Date Completed: ESTIMATED GROUND V	3/31/2015	
DR Vehicle:		METHOD		AMPLE N/A	ĸ		Date	Depth	ESTIMATED GROUND V Elevation		Reference
		ver Probe		N/A			3/31/2015	Depth	Elevation	r	
Method:		H.S.A.		N/A			2. 3 . 2010				
Hammer				N/A							
Depth							<b></b>	SAMPI		Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blow		N <sub>60</sub>		DESCRIP	TION	Test Data	Stratum
1				PRC	DRF		2.5" of Pavemen	t			PAVEMENT 0.2'
· -							ł				FILL
2_							Auger cuttings: t	an Sandy SILT,	some brick fragments,		
3				$\left  \right $	-+		ł				
Ŭ –							t				
4					[		Į				
5	┝───			┟──┤			ł				
5							t				
6							1				
7	┝───			┟──┤			ł				
· -		L	ļ		$\rightarrow$		t				
8							]				
9				$\left  \right $			ł				
<sup>7</sup> -				┟─┤	-+						9.0' +/-
10				V	,						WEATHERED ROCK
11				<u> </u>			End of Probe at	10.0', Auger ref	usal		10.0' BEDROCK
''-				<u> </u>	$\rightarrow$		ł				DEDROCK
12							1				
13	<u> </u>			<u> </u>			ł				
13				<u> </u>	$\rightarrow$		ł				
14							1				
15					[		ł				
15							ł				
16							1				
17				<u> </u>	[		ł				
17				<u> </u>	$\rightarrow$		ł				
18							1				
19				<u> </u>			ł				
19				<u> </u>	$\rightarrow$		t				
20							1				
21				<u> </u>			ł				
<u> </u>				<u> </u>	-+		t				
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23	┝───			<u> </u>			ł				
23-	L			L			İ				
24	[			[			Į				
25				<u> </u>			ł				
							İ				
26						-	Į				
27				<u> </u>			ł				
				L			<u>†</u>				
Granula	ar Soils	Cohesiv	e Soils	% (	Compo	sition	NOTES:	PP = Pocket Per	netrometer, MC = Moisture C	Content	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	AS	STM D2			LL = Liquid Limi	t, PI = Plastic Index		Dry: S = 0%
	V. Loose	<2	V. soft		F0/ -		Bedrock Joints				Humid: $S = 1$ to 25%
5-10 11-30	Loose	2-4 5 8	Soft		5% Tr		Shallow = 0 to 35 Dipping = 35 to 55	-			Damp: $S = 26$ to 50% Moist: $S = 51$ to 75%
11-30 31-50	Compact Dense	5-8 9-15	Firm Stiff		15% L 30% S		Dipping = $35$ to $55$ Steep = $55$ to $90$ c	-			Woist: $S = 51 \text{ to } 75\%$ Wet: $S = 76 \text{ to } 99\%$
	V. Dense		V. Stiff		30% V			30			Saturated: S = 100%
	-	>30	Hard				Boulders = diamet	ter > 12 inches, C	Cobbles = diameter < 12 inch	nes and > 3 inches	
							Gravel = < 3 inch	and > No 4, San	d = $<$ No 4 and $>$ No 200, Si	It/Clay = < No 200	

		$\sim$					SOIL PRO	BE LOG	Boring #:	P-3
		CIINA	AAT			Project:	Proposed Apar		Project #:	15040
		SUIVI	IVIII			Location:	665 Congress		Sheet:	1 of 1
		GEOENGINEERI	NG SERVICES			City, State:	Portland, ME		Chkd by:	
Drilling C	: 0:	Summit Geoen	gineering Ser	vices		Boring Elevation:		112.8 ft		
Driller:		C. Coolidge, P.				Reference:		Titcomb Associates		
Summit S		M. Hardison, E				Date started:	3/31/2015	Date Completed:	3/31/2015	
		METHOD		AMPLER		D.I.	D	ESTIMATED GROUND		
Vehicle: Model:		ver Probe	Length: Diameter:	N/A N/A		Date 3/31/2015	Depth	Elevation	R	eference
Model: Method:		' H.S.A.	Diameter: Hammer:	N/A N/A		3/31/2015				
Hammer			Method:	N/A		1			1	
Depth						Ī	SAMP	LE	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows	'6" N <sub>60</sub>	1	DESCRIP		Test Data	Stratum
_	-			PROE	E	3.5" of Pavemen	t			PAVEMENT
1_				$\vdash$		Dense drilling at	8" moved over	and started new hole		0.3' FILL
2						Dense uning at	8, moved over			
-						Auger cuttings: [	Dark tan SAND,	little Silt and Gravel		
3_				$+$ $\mp$		4				
4						+				
_						1				
5				$\vdash$						F.O /
6				$\vdash$		Auger cuttings: s	similar to above	. little Clav		5.0' +/- GLACIAL TILL
Ŭ –	L							, inter only		
7						1			_	7.01 (
8				$\vdash$		4				7.0' +/- WEATHERED ROCK
- U						Auger cuttings: I	ight tan fine SA	ND (rock dust)		WEATHERED ROOK
9_						] -				
10						4				
	L					End of Probe at	9.9', Auger refu	sal		9.9'
11						]	-			BEDROCK
12						4				
12-						1				
13						]				
14						+				
14-						1				
15						1				
16						4				
10						†				
17						1				
18						4				
10						1				
19						1				
20	<u> </u>					4				
20_						†				
21						1				
22						4				
22_						1				
23						1				
24						4				
24_						†				
25						1				
24						4				
26_						+				
27						1				
		<u> </u>		<u></u>		NOTEC	DD D			0.111
Granula Blows/ft.		Cohesiv Blows/ft.			mposition M D2487	NOTES:		netrometer, MC = Moisture ( t. PL = Plastic Index	Jontent	Soil Moisture Condition Dry: S = 0%
0-4	V. Loose	<2 BIOWS/TT.	Consistency V. soft	ASI	IVI UZ40/	Bedrock Joints	LL = LIQUIO LIMI	t, PI = Plastic Index		Dry: $S = 0\%$ Humid: $S = 1$ to 25%
5-10	Loose	2-4	Soft	< 5	% Trace	Shallow = 0 to $35$	degrees			Damp: $S = 26$ to 50%
	Compact	5-8	Firm		5% Little	Dipping = 35 to 55	-			Moist: $S = 51$ to 75%
31-50	Dense	9-15	Stiff		0% Some	Steep = 55 to 90 d	degrees			Wet: S = 76 to 99%
>50	V. Dense	16-30	V. Stiff	> 3	0% With					Saturated: S = 100%
1		>30	Hard					Cobbles = diameter < 12 inc d = $< No.4$ and $> No.200$ S		
				I			anu > NU 4, Sah	$d = \langle No 4 and \rangle No 200, S$	ni/ Glay = < NU 200	

						SOIL PRO	BE LOG	Boring #:	P-4	
		CIINA	AAT			Project:	Proposed Apar		Project #:	15040
	SUIVIIVII		Location:	665 Congress S		Sheet:	1 of 1			
		GEOENGINEERI	NG SERVICES			City, State:	Portland, ME		Chkd by:	
Drilling C				Boring Elevation:	-	112.9 ft	•			
Driller:				Reference:	Site Survey by	Titcomb Associates				
Summit S	Staff:	M. Hardison, E	.l.			Date started:	3/31/2015	Date Completed:	3/31/2015	
		METHOD		AMPLER				ESTIMATED GROUND W		
Vehicle:				N/A		Date	Depth	Elevation	Re	eference
		ver Probe		N/A		3/31/2015				
Method:		H.S.A.	Hammer: Method:	N/A N/A		}			+	
Hammer	Style: F	AULO	Method:	N/A			SAMPI	F	Geological/	Geological
Depth (ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	4	DESCRIP		Test Data	Stratum
(11.)	NO.	Ten/Rec (II)	Deptil (It)	PROBE	1 400	3.5" of Pavemen		TION		PAVEMENT
1							-			0.3'
						Auger refusal at	2', moved over	and started new hole		FILL
2_					1	Encountered den	se drilling at 2'	again in second hole,		
3	-					drilled past it. De	ense driilling eco	ountered again at 4'.		
_						Likely rubble	Ū.	0		
4				V			1.01.4			4.01
5						End of Probe at 4	4.0°, Auger refu	sai		4.0' RUBBLE
- J						1				NODDEL
6						]				
7	<u> </u>					+				
						ł				
8						1				
						]				
9_					1	+				
10						4				
_						1				
11_					-	4				
12						+				
						1				
13						]				
14						+				
14						4				
15						1				
1/						-				
16	-				+	+				
17						1				
18						+				
19						4				
_						1				
20						4				
21						+				
_						1				
22						4				
23						4				
23					1	1				
24						1				
25						+				
25_						ł				
26						1				
						4				
27						4				
Granula	ar Soils	Cohesiv	e Soils	% Com	osition	NOTES:	PP = Pocket Per	netrometer, MC = Moisture C	ontent	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	ASTM I				t, PI = Plastic Index		Dry: $S = 0\%$
	V. Loose	<2	V. soft			Bedrock Joints				Humid: $S = 1 \text{ to } 25\%$
5-10	Loose	2-4	Soft	< 5%	Trace	Shallow = 0 to 35	degrees			Damp: S = 26 to 50%
	Compact	5-8	Firm	5-15%		Dipping = 35 to 55	5 degrees			Moist: S = 51 to 75%
31-50	Dense	9-15	Stiff	15-30%		Steep = 55 to 90 c	degrees			Wet: S = 76 to 99%
>50	V. Dense		V. Stiff	> 30%	With					Saturated: S = 100%
1		>30	Hard					cobbles = diameter < 12 inch		
L						Gravel = < 3 inch	ana > No 4, Sano	$d = \langle No \ 4 \ and \rangle No \ 200$ , Sil	ı/∪lay = < No 200	

		$\wedge$					SOIL PRO	BE LOG	Boring #:	P-5
		SUM	NAN			Project:	Proposed Apar	tment Building	Project #:	15040
			Location:	665 Congress	St.	Sheet:	1 of 1			
						City, State:	Portland, ME		Chkd by:	
					Boring Elevation:	Boring Elevation: 112.3 ft				
Driller:					Reference:		Titcomb Associates	3/31/2015		
		M. Hardison, E METHOD		AMPLER		Date started:	3/31/2015	Date Completed: ESTIMATED GROUND V		
Vehicle:				N/A		Date	Depth	ESTIMATED GROUND V		eference
		ver Probe		N/A		3/31/2015	Jopin	Liovation		
Method:	2-1/2"	H.S.A.	Hammer:	N/A						
Hammer	Style: A	Nuto	Method:	N/A						
Depth					NI	-	SAMP		Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6" PROBE	N <sub>60</sub>	3" of Pavement	DESCRIP	TION	Test Data	Stratum PAVEMENT
1				I			9"', moved over	and started new hole,		0.3'
				Ŵ		encounered same	e refusal. Likely	cobble		
2_						End of Probe at (	0.8', Auger refu	sal		0.8' COBBLE
3										COBBEE
						Į				
4_						ł				
5						t				
						Į				
6						ł				
7						İ				
						Į				
8_						ł				
9						İ				
10						ł				
10_						-				
11						1				
12						ł				
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13						]				
14						ł				
						t				
15						Į				
16						ł				
						1				
17						ł				
18						ł				
-						1				
19						ł				
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21_						ł				
22						1				
22						ł				
23						ł				
24						1				
25						ł				
2.5						t				
26						Į				
27						ł				
						<u> </u>				
Granula		Cohesiv		% Comp		NOTES:		netrometer, MC = Moisture C	Content	Soil Moisture Condition
Blows/ft.	-	Blows/ft.	Consistency	ASTM D			LL = Liquid Limi	t, PI = Plastic Index		Dry: $S = 0\%$
0-4 5-10	V. Loose Loose	<2 2-4	V. soft Soft	- F0/ 7		Bedrock Joints	dogroes			Humid: $S = 1 \text{ to } 25\%$
	Compact	2-4 5-8	Firm	< 5% 1 5-15%		Shallow = 0 to $35$ Dipping = $35$ to $55$	-			Damp: $S = 26$ to 50% Moist: $S = 51$ to 75%
31-50	Dense	9-15	Stiff	15-30%		Steep = $55$ to $90$ c	-			Wet: $S = 76 \text{ to } 99\%$
	V. Dense		V. Stiff	> 30%			-			Saturated: S = 100%
		>30	Hard					Cobbles = diameter < 12 inch		
						Gravel = < 3 inch	and > No 4, San	$d = \langle No \ 4 \ and \rangle No \ 200$ , Si	t/Clay = < No 200	

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Line         Description         66 Congress S1. (r) State:         Struct         1 of 1           Dulling Co.         Scored S4. (r) State:         Provide (Million Constructions)         12.3 ff         Hold by:         12.3 ff           Dulling Co.         Scored S4. (r) State:         Provide (Million Constructions)         21.2 ff         12.3 ff         Hold by:         12.3 ff           State:         State:         Data Science:         12.3 ff         Hold by:         12.3 ff           State:         State:         State:         Data Science:         12.3 ff         Hold by:         12.3 ff           State:         State:         State:         State:         Data Science:         12.3 ff         Hold by:         12.5 Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by:         Hold by: <td< td=""><td colspan="3">SIINANAH</td><td>Project:</td><td>Proposed Apar</td><td>tment Building</td><td></td><td>15040</td></td<>	SIINANAH			Project:	Proposed Apar	tment Building		15040				
Diffing Co:         Summit Geoing/Intering Stratus         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co:         Diff Co: <thdiff co:<="" th="">         &lt;</thdiff>			~~~~									
Teller:         C. Couldige, P.T.         Bergeren:         Site Survey by Thome Associated           Monte Staff, M. Mardson, E.I.         Mardson, E.I.         Data started 0: 3/31/2015         Site Survey by Thome Associated           Monte:         Site Survey by Thome Associated         3/31/2015         Site Survey by Thome Associated         3/31/2015           Monte:         Mardson, E.I.         Site Survey by Thome Associated         3/31/2015         Site Survey by Thome Associated         3/31/2015           Monte:         Mardson, E.I.         Site Survey by Thome Associated         Site Survey by Thome Associated         3/31/2015           Monte:         Mardson, E.I.         Mardson, E.I.         Site Survey by Thome Associated         Site Survey by Thome Associated         Site Survey by Thome Associated           Monte:         Site Survey by Thome Associated         Site Survey by Thome Associated         Site Survey by Thome Associated         Site Survey by Thome Associated           Monte:         Site Survey by Thome Associated         Site Survey by Thome Associated         Site Survey by Thome Associated         Site Survey by Thome Associated           Monte:         Markson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson Barkson B			GEOENGINEERI	NG SERVICES				City, State:	Portland, ME		Chkd by:	
Summit Staff:         M. Hardson, E. J.         Date transf.         3/3/2/015         Late Completed:         3/3/2/015           DBHLLING MENDOR         SAMPLER         CESTMATED GRUBUN/RETURPTIN         Reference           Matcher         Franker         Barnet Staff.         MARK         Date         Depth         Franker           Matcher         Sampt Staff.         MARK         Date         Depth         Franker         Reference           Matcher         Sampt Staff.         MARK         Date         Depth         Franker         Reference           Matcher         Sampt Staff.         MARK         Date         Depth         Franker         Reference           Appl         Reference         Sampt Staff.         Marker         Reference         Sampt Staff.           2         Reference         Reference         Sampt Staff.         Reference         Sampt Staff.           2         Reference         Reference         Sampt Staff.         Reference         Sampt Staff.           2         Reference         Reference         Sampt Staff.         Reference         Sampt Staff.           2         Reference         Reference         Sampt Staff.         Reference         Sampt Staff.           2				U U								
DBULLING METHOD         SAMPLER         ESTIMATE OROUND WATE DEPTH           Model:         MAX         Duel         Depth         Exvalion         Reference           Model:         MAX         Damater:         N/A         3/37/2015         Exvalion         Reference           Model:         MAX         Damater:         N/A         3/37/2015         Exvalion         Reference           Model:         MAX         Damater:         N/A         3/37/2015         Exvalion         Reference           Model:         Max         Depth         Exvalion         Reference         Sample:           (1)         Mo         PerroRec (n)         Depth         Description         Description         Sample:           2         Image: Internet (n)         PerroRec (n)         Description         Sample:         Description         Sample:           3         Image: Internet (n)         PerroRec (n)         Description         Sample:         Description         Sample:         Sample:           4         Image: Internet (n)         Image: Internet (n)         PerroRec (n)         PerroRec (n)         Sample: Internet (n)         Sample: Internet (n)         Sample: Internet (n)           3         Image: Internet (n)         Image: Intern											0.000.00005	
Multice:         Translat         Complex         N/A         Date         Daph         Elevation         Reference           Method:         31/27 HS.A.         Hammers:         N/A         32/3/2015         Image: Status         Status         Image: Status         Status         Status         Status         Status         Status         PAVENDUR         Status         PAVENDUR         Status         PAVENDUR         Status         PAVENDUR         Status         PAVENDUR         Status         PAVENDUR         Status         PAVENDUR         Status         PAVENDUR         Status         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR         PAVENDUR						D		Date started:	3/31/2015			
Bodd:         MAX         3/31/2015         Home           Hammer Sylv:         Auto         SAMULE         Geological         Geological         Geological         Statum           1         Hammer Sylv:         Rule         David         SAMULE         Geological         Geological         Statum           1         Hammer Sylv:         Rule         David         NA         Description         Test Data         Statum           1         Hammer Sylv:         Rule         Description         Cological         Geological         Geological         Statum           2         Hammer Sylv:         Rule         Hammer Sylv:         Rule         Description         Description         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum         Statum<						-R		Data	Dopth			foronco
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(ft)         No.         Description         Test Data         Stratum           1         -         -         PROBE         2.3' of Parement         -         PROBE         2.2''         -         PROBE         0.2''         FILL         -         PROBE         0.2''         FILL         -         PROBE         0.2''         FILL         -         PROBE         0.2''         FILL         -         -         -         PROBE         0.2''         FILL         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -	Hammer			Method:	N/A							
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3         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -	2											
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6         End of Probe at 5.0; Auger refusal         5.0°           7         End of Probe at 5.0; Auger refusal         5.0°           8         End of Probe at 5.0; Auger refusal         5.0°           9         End of Probe at 5.0; Auger refusal         5.0°           10         End of Probe at 5.0; Auger refusal         5.0°           11         End of Probe at 5.0; Auger refusal         5.0°           12         End of Probe at 5.0; Auger refusal         5.0°           13         End of Probe at 5.0; Auger refusal         5.0°           14         End of Probe at 5.0; Auger refusal         5.0°           14         End of Probe at 5.0; Auger refusal         5.0°           15         End of Probe at 5.0; Auger refusal         5.0°           14         End of Probe at 5.0; Auger refusal         5.0°           15         End of Probe at 5.0; Auger refusal         5.0°           16         End of Probe at 5.0; Auger refusal         5.0°           17         End of Probe at 5.0; Auger refusal         5.0°           18         End of Probe at 5.0; Auger refusal         5.0°           19         End of Probe at 5.0; Auger refusal         5.0°           20         End of Probe at 5.0; Auger refusal         5.0°	4							ł				
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16       Image: Solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the solity of the so	14 -											
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17       Image: Construct on the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second												
18       Image: Construct of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second	16							ł				
19       Image: Construct of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second	17							t				
19       Image: Construct of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second								Į				
20         Image: Consistency of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second sec	18							ł				
21	19							ł				
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22       23       24       23       24       24       24       25       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       26       27       27       27       27       27       27       27       27       27       27       27       27       27       27       27       27       27       27       27       28       27       28       27       28       27       28       27       28       27       28       27 <td< td=""><td>20</td><td></td><td></td><td></td><td> </td><td></td><td></td><td>ł</td><td></td><td></td><td></td><td></td></td<>	20							ł				
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23								[				
24	22_							ł				
24	23							ł				
25       26       26       26       27       26       27       27       28       28       27       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       26       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28       28 <th28< th="">       28       28       <th2< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td></th2<></th28<>								1				
26	24							ł				
26	25							ł				
27       Image: Construct of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the structure of the s								1				
Granular Soils       Cohesive Soils       % Composition       NOTES:       PP = Pocket Penetrometer, MC = Moisture Content       Soil Moisture Concent         Blows/ft.       Density       Blows/ft.       Consistency       ASTM D2487       LL = Liquid Limit, PI = Plastic Index       Dry: S = 0%         0-4       V. Loose       <2	26							ł				
Granular Soils       Cohesive Soils       % Composition       NOTES:       PP = Pocket Penetrometer, MC = Moisture Content       Soil Moisture Concent         Blows/ft.       Density       Blows/ft.       Consistency       ASTM D2487       LL = Liquid Limit, PI = Plastic Index       Dry: S = 0%         0-4       V. Loose       <2	27							ł				
Blows/ft.       Density       Blows/ft.       Consistency       ASTM D2487       LL = Liquid Limit, PI = Plastic Index       Dry: S = 0%         0-4       V. Loose       <2								<u> </u>				
0-4         V. Loose         <2         V. soft         Bedrock Joints         Humid: S = 1 to           5-10         Loose         2-4         Soft         < 5% Trace								NOTES:			ontent	Soil Moisture Condition
5-10         Loose         2-4         Soft         < 5% Trace         Shallow = 0 to 35 degrees         Damp: S = 26 to           11-30         Compact         5-8         Firm         5-15% Little         Dipping = 35 to 55 degrees         Moist: S = 51 to           31-50         Dense         9-15         Stiff         15-30% Some         Steep = 55 to 90 degrees         Wet: S = 76 to 9           >50         V. Dense         16-30         V. Stiff         > 30% With         Boulders = diameter > 12 inches, Cobbles = diameter < 12 inches and > 3 inches         Saturated: S = 10		-		-	AS	STM D	2487		LL = Liquid Limi	t, PI = Plastic Index		Dry: S = 0%
11-30         Compact         5-8         Firm         5-15% Little         Dipping = 35 to 55 degrees         Moist: S = 51 to           31-50         Dense         9-15         Stiff         15-30% Some         Steep = 55 to 90 degrees         Wet: S = 76 to 90           >50         V. Dense         16-30         V. Stiff         > 30% With         Source of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second se						F0/ -	·					Humid: $S = 1$ to 25%
31-50         Dense         9-15         Stiff         15-30% Some         Steep = 55 to 90 degrees         Wet: S = 76 to 90 Saturated: S = 10           >50         V. Dense         16-30         V. Stiff         > 30% With         Saturated: S = 10         Saturated: S = 10           >30         Hard         Boulders = diameter > 12 inches, Cobbles = diameter < 12 inches and > 3 inches         Saturated: S = 10									-			Damp: $S = 26 \text{ to } 50\%$
>50     V. Dense     16-30     V. Stiff     > 30% With     Saturated: S = 1       >30     Hard     Boulders = diameter > 12 inches, Cobbles = diameter < 12 inches and > 3 inches     Saturated: S = 1									-			
>30 Hard Boulders = diameter > 12 inches, Cobbles = diameter < 12 inches and > 3 inches								Siech = 33 10 40 (	acylees			Saturated: S = 100%
		. 201100				2070		Boulders = diamet	ter > 12 inches, C	Cobbles = diameter < 12 inch	es and > 3 inches	
Gravel = < 3 inch and > No 4, Sand = < No 4 and >No 200, Silt/Clay = < No 200					L							

		$\sim$					SOIL PRO	BE LOG	Boring #:	P-101	
		SUM	AAT			Project: Proposed Apartment Building			Project #:	15040	
		~~~~				Location: 665 Congress St. Sheet:			1 of 1		
		GEOENGINEERI	NG SERVICES			City, State:	Portland, ME		Chkd by:		
Drilling C	co:	Great Works Te	est Boring			Boring Elevation:					
Driller:	Driller: Jeff Lee			Reference:	Site Survey by	Titcomb Associates					
Summit		M. Hardison, E				Date started:	4/15/2015	Date Completed:	4/15/2015		
		METHOD		AMPLER				ESTIMATED GROUND W			
Vehicle:			Length:	N/A		Date	Depth	Elevation		eference	
Model:			Diameter:	N/A		4/15/2015	-		None observed		
Method Hammer		Stem Auger	Hammer: Method:	N/A N/A					+		
Depth	June. I		Metriou.				SAMPI	l F	Geological/	Geological	
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/	5" N <sub>60</sub>	1	DESCRIP		Test Data	Stratum	
,			· • • • • • • •	PROB		3" Pavement				PAVEMENT	
1										0.25' +/-	
2						Very difficult drill	ing, frequent ru	bbe encountered, refusal		FILL	
2_	-			-	-	new hole	iist nole at 4.5',	moved over 1' to start			
3						1					
-						]					
4_				-	_	4					
5						+					
Ŭ –	L					1					
6						]					
7				-	_	+					
'-						1					
8						1					
						4					
9_				$\vdash$	-	Smoother drilling	started around	9', assumed transizion	+	9' +/-	
10	<u> </u>					zone into native				GLACIAL TILL	
I				V							
11_						End of Probe at 7	10.8', Auger refi	usal		10.8' BEDROCK	
12						+				DEDRUCK	
-						1					
13						]					
14					_	+					
14						1					
15						1					
						4					
16_						4					
17						1					
_						]					
18_						4					
19					-	1					
-						1					
20_						4					
21						+					
_						1					
22						4					
23						4					
23_	L					1					
24						]					
25	L					+					
20						1					
26						1					
07						4					
27_						4					
Granula	ar Soils	Cohesiv	e Soils	% Coi	nposition	NOTES:	PP = Pocket Per	netrometer, MC = Moisture Co	Intent	Soil Moisture Condition	
Blows/ft.		Blows/ft.	Consistency		1 D2487			t, PI = Plastic Index		Dry: $S = 0\%$	
0-4	V. Loose		V. soft	İ		Bedrock Joints				Humid: $S = 1$ to 25%	
5-10	Loose	2-4	Soft	< 59	6 Trace	Shallow = 0 to 35	degrees			Damp: S = 26 to 50%	
11-30	Compact		Firm		% Little	Dipping = 35 to 55	-			Moist: S = 51 to 75%	
31-50	Dense	9-15	Stiff		% Some	Steep = 55 to 90 c	degrees			Wet: S = 76 to 99%	
>50	V. Dense		V. Stiff	> 30	% With	Devide :: "	10 ! . !	Andrea alternation and the	and a first	Saturated: S = 100%	
1		>30	Hard					Cobbles = diameter < 12 inche			
L						Glavel = < 3 Inch	ariu > ivo 4, Sano	$d = \langle No 4 and \rangle No 200$ , Silt	/Gay = < NO 200		

		$\sim$						SOIL PRO	BE LOG	Boring #:	P-102
		SIINA	NANT				Project:	Proposed Apart	tment Building	Project #:	15040
		SUIVI	IVIIA				Location:	665 Congress S		Sheet:	1 of 1
		GEOENGINEERI	NG SERVICES				City, State:	Portland, ME		Chkd by:	
Drilling C				Boring Elevation: 111.9 ft							
Driller: Jeff Lee				Reference:		Titcomb Associates					
Summit S		M. Hardison, E					Date started:	4/15/2015	Date Completed:	4/15/2015	
		METHOD		AMPL					ESTIMATED GROUND V		
Vehicle:			Length:	24" 3			Date	Depth	Elevation		eference
Model:			Diameter:		D/1.5"	ID	4/15/2015	-		None observed	
Method Hammer		Stem Auger	Hammer: Method:	140	lb M D15	86				+	
Depth	June. M		MELIUU.	лJII	כוס ואו	00		SAMPL	F	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blov	ws/6"	N <sub>60</sub>	ł	DESCRIP		Test Data	Stratum
(11.)	110.		Deptil (It)		OBE	••00	3" Pavement	DESORT		Test Data	PAVEMENT
1	-										
_											
2_				-			Smooth drilling t	hroughout fill lo	yer (no rubble/cobbles)		
3	$\vdash$			<u> </u>				noughout III la	yer (no rubble/cobbles)		
							t				
4							Į				
-	$\mid$				<u> </u>		ł				
5_				-			Increased resista	nce at 4.8 note	ential till or soft rock		
6											
7_				<u> </u>			ł				
8				-			ł				
				L			t				
9							Į				
10				-			Ļ				
10				<u> </u>			ł				
11				L			t				
							Į				
12_				``	$\checkmark$		End of Droha at 1	10.1' Augor rofe	uppel .		10.1
13	$\vdash$			<u> </u>			End of Probe at ?	12.1, Auger rett	וסכו		12.1' BEDROCK
											DEDITOOK
14											
15											
15											
16											
17											
18							-				
10_							t				
19							Į				
20							ļ				
20				-			ł				
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23	<u> </u>			<u> </u>			Ļ				
20							t				
24							[				
25							ł				
25				<u> </u>			ł				
26							t				
							1				
27							ļ				
Crock	yr Soile	0-L'	o Soile	07	Com	ocition	NOTES:	DD - Docket D	otromotor MC	ontont	Soil Meisture Caralities
Granula Blows/ft.		Cohesiv Blows/ft.	Consistency		Compo STM D		NUTES:		etrometer, MC = Moisture C ;, PI = Plastic Index	oment	Soil Moisture Condition Dry: S = 0%
	V. Loose	<2	V. soft			2401	Bedrock Joints	בב – בוקטוט בווחונ			Humid: $S = 1$ to 25%
0-4 5-10	Loose	2-4	Soft		< 5% T	race	Shallow = 0 to 35	dearees			Damp: $S = 26$ to 50%
	Compact	5-8	Firm		5-15%		Dipping = $35$ to $55$	-			Moist: $S = 51$ to 75%
31-50	Dense	9-15	Stiff		5-30%		Steep = $55$ to $90$ c	-			Wet: S = 76 to 99%
		16-30	V. Stiff		> 30%			-			Saturated: S = 100%
	V. Dense	10-30									
	V. Dense	>30	Hard				Boulders = diamet	er > 12 inches, C	obbles = diameter < 12 inch	nes and > 3 inches	

		$\sim$					SOIL PRO	BE LOG	Boring #:	P-103
		SUM	AALT			Project: Proposed Apartment Building			Project #:	15040
		~ ~ …				Location:	665 Congress	•	Sheet:	1 of 1
		GEOENGINEERI	NG SERVICES			City, State:	Portland, ME		Chkd by:	
			Boring Elevation:		112.3 ft					
Driller:		Jeff Lee				Reference:		Titcomb Associates	14510045	
Summit S		M. Hardison, E			D	Date started:	4/15/2015	Date Completed:	4/15/2015	
DR Vehicle:		VETHOD		AMPLEI 24" SS		Date	Depth	ESTIMATED GROUND \ Elevation		eference
Model:					) 1.5"ID	4/15/2015	- Depth	Elevation	None observed	
Method	4" Solid	Stem Auger	Hammer:	140 lb			<u> </u>			
Hammer				ASTM	D1586					
Depth						↓	SAMPI		Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows		4" Pavement	DESCRIP	TION	Test Data	Stratum PAVEMENT
1				PRO	DE	4 Pavement				0.3'
· -						4				0.0
2							ulling a set of	/aabblaa aasta staat t		
3				$\left  \right $		Relatively easy d	rilling, no rubbe	cobbles encountered		
Ŭ						1				
4						1				
5						4				
5						1				
6						1				
7						4				
í –						1				
8						1				
9						4				
7-						4				
10				Ľ		End of Probe at	9.6', Auger refu	sal		9.6'
11						4				BEDROCK
· ''-						4				
12						1				
13						4				
13						4				
14						1				
15				<u> </u>		4				
10						4				
16						1				
17						4				
17						4				
18						1				
19						4				
19						4				
20						1				
21						4				
21						4				
22						1				
23						4				
23						4				
24						1				
25						4				
25						1				
26						1				
27						4				
<i>21</i>						4				
Granula	ar Soils	Cohesiv	e Soils	% C	omposition	NOTES:	PP = Pocket Per	netrometer, MC = Moisture C	Content	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	AS	TM D2487	4	LL = Liquid Limi	t, PI = Plastic Index		Dry: S = 0%
	V. Loose	<2	V. soft			Bedrock Joints				Humid: $S = 1$ to 25%
5-10	Loose	2-4	Soft		5% Trace	Shallow = 0 to $35$	-			Damp: $S = 26$ to 50%
11-30 31-50	Compact Dense	5-8 9-15	Firm Stiff		15% Little 30% Some	Dipping = $35$ to $55$ Steep = $55$ to $90$ d	-			Moist: $S = 51$ to 75% Wet: $S = 76$ to 99%
	V. Dense	9-15 16-30	V. Stiff		30% With	51000 - 55 10 70 1	aogi 003			Saturated: $S = 100\%$
		>30	Hard			Boulders = diamet	ter > 12 inches, C	cobbles = diameter < 12 inc	hes and > 3 inches	

# APPENDIX C

# **ROCK CORE PHOTOS**



# PHOTOGRAPHIC LOG

Project:		Project No.
Proposed Apartment Buil	lding – 665 Congress St., Portland ME	15040
Photo No. 1		I
<b>Date:</b> 4-16-2015		
Site Location:	-	
665 Congress Street Portland, Maine		
Description:		
Rock Core C-1 in Boring B-105 from depth 10 feet to 15 feet		
Elevation 103.8 feet to Elevation 98.8 feet		
Description:		
Schist	Bottom	



# PHOTOGRAPHIC LOG

Project:		Project No.
Proposed Apartment Buil	ding – 665 Congress St., Portland ME	15040
Photo No. 1		-
<b>Date:</b> 4-16-2015		
Site Location:		
665 Congress Street Portland, Maine		
Description:		
Rock Core C-2 in Boring B-106 from depth 10 feet to 15 feet		
Elevation 102 feet to Elevation 97 feet		
Description:		
Schist	<image/>	

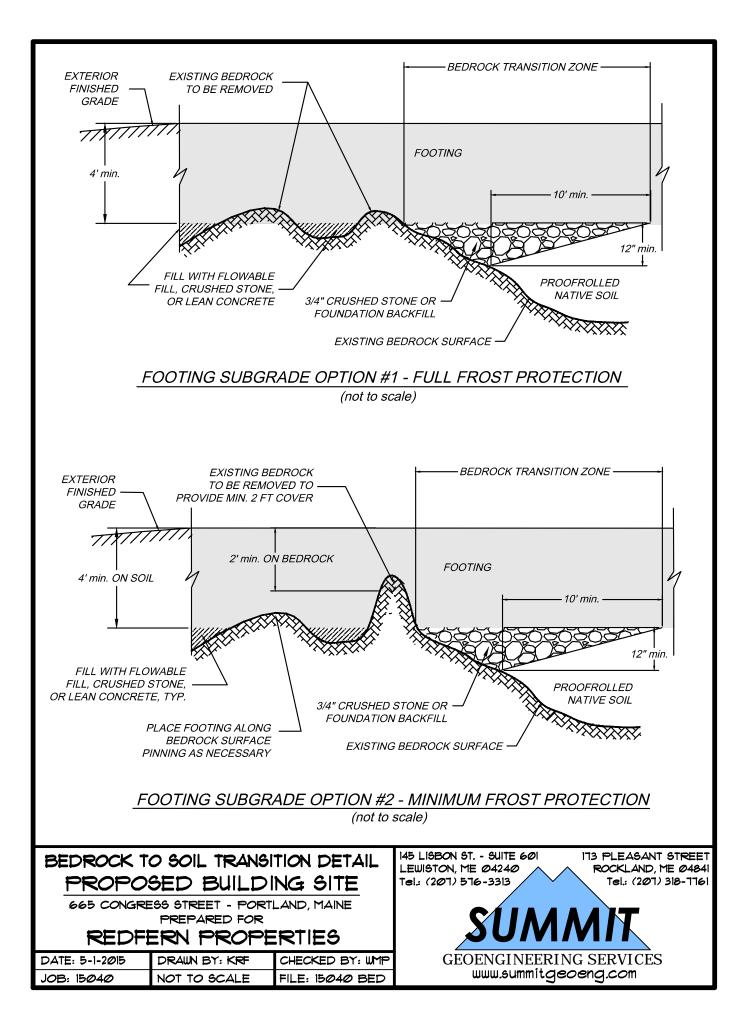


# PHOTOGRAPHIC LOG

Project:		Project No.
Proposed Apartment Buil	ding – 665 Congress St., Portland ME	15040
Photo No. 1		-
<b>Date:</b> 4-16-2015		
Site Location:		
665 Congress Street Portland, Maine		
Description:		
Rock Core C-3 in Boring B-106 from depth 15 feet to 19 feet		
Elevation 97 feet to Elevation 93 feet		
Description:		
Schist	Bottom         Bottom         Contraction         Contrest         Cont	

# APPENDIX D

# TRANSITION ZONE CONSTRUCTION DETAIL



# APPENDIX E

# GENERAL BLASTING CRITERIA

# GENERAL BLASTING RECOMMENDATIONS

# **Introduction**

Blasting operations will be performed in general accordance with the applicable Maine Revised Statute Title 125 and Title 38, U.S. Department of the Interior Rules, the recommendations provided below, and a normal standard of care.

# <u>Blast Design</u>

The blasting contractor shall submit a blasting plan to the Owner for approval prior to blasting operations. The blasting plan shall include a schedule, sketches of the drill patterns (hole spacing and depth), type and amount of explosives, number and sequence of delays, methods for minimizing flyrock, and any other information pertinent to demonstrating compliance with the applicable U.S. Department of the Interior Rules and the requirements of the applicable Statute requirements of 38 MRSA.

# **Notification**

Oral notification to the abutters within one-half mile of the blast area shall be provided prior to blasting. Warning and all clear signals of different character or pattern that are audible within one-half mile from the point of the blast shall be given. The meaning of the signals shall be conveyed to the abutters at the time they are notified.

# **Pre-blast Surveys**

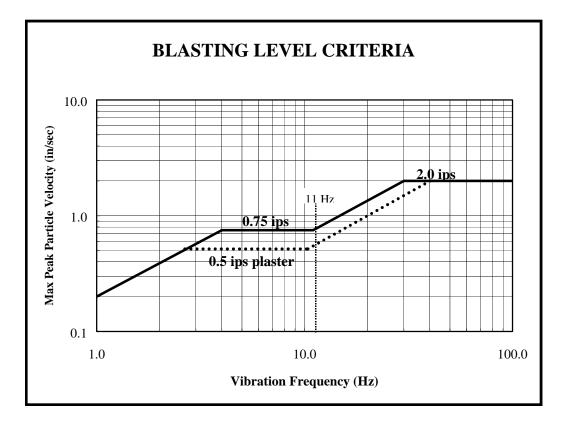
All blasting operations are the direct responsibility of the Blasting Contractor. Reports of damage to structures caused by blasting operations are the sole responsibility of the Blasting Contractor. Therefore, it is incumbent upon the Blasting Contractor to perform pre-blast surveys as they deem necessary.

# Airblast Limits

Airblast overpressure shall not exceed the limits stipulated in 38 MRSA 490-Z(14)(H) at the nearest structure. This currently requires sound from blasting to not exceed 129 decibels peak at inhabited structures and 140 decibels peak at uninhabited structures.

# **Ground Vibration Limits**

The maximum ground vibration at any structure shall not exceed the limits presented in the following chart:



REFERENCE: OSM alternative blasting criteria (Modified from figure B-1, Bureau of Mines, RI 8507)

The Blasting Contractor shall provide a seismographic record to the Owner for each blast event at the nearest off-site structure. The record shall include the date and time of the blast, peak and resultant particle velocities and associated frequencies, and the airblast overpressure.

# <u>Flyrock</u>

Sufficient stemming, matting, or natural protective cover shall be provided to prevent flyrock from leaving property owned or under control of the operator or from entering protected natural resources or natural buffer strips.

# **Records**

Records of blasts shall be recorded in accordance with Maine Statute 38 MRSA 490-Z(14)(L). The current requirements are as follows.

- Name of blasting company or blasting contractor
- Location, date and time of blast
- Name, signature and social security number of blaster
- Type of material blasted
- Number and spacing of holes and depth of burden or stemming
- Diameter and depth of holes
- Type of explosives used
- Total amount of explosives used
- Maximum amount of explosives used per delay period of 8 milliseconds or greater
- Maximum number of holes per delay period of 8 milliseconds or greater
- Method of firing and type of circuit
- Direction and distance in feet to the nearest dwelling, public building, school, church or commercial or institutional building neither owned nor controlled by the developer
- Weather conditions, including factors such as wind direction and cloud cover
- Height or length of stemming
- Amount of mats or other protection used
- Type of detonators used and delay periods used
- The exact location of each seismograph and the distance of each seismograph from the blast
- Seismographic readings
- Name and signature of the person operating each seismograph
- Names of the person and the firm analyzing the seismographic data

# MAXIMUM PARTICLE VELOCITY/DISTANCE CRITERIA FOR BLASTING NEAR UNCURED CONCRETE

Time From Batching (hr)	Non-Structural Concrete	Structural Concrete
0-4	4D	2D
4 - 24	1D	0.25D
24 – 72	1.5D	1D
72 – 168	3D	2D
168 - 240	8D	5D
Over 240	15D	10D

Distance (ft)	D (in/sec)
0 to 50	1.0
50 to 150	0.8
150 to 250	0.7
Over 250	0.6

<u>NOTE</u>: Allowable vibration levels are reduced with increasing distance since concrete can withstand higher vibration levels at higher frequencies. Vibration frequencies decrease as the distance from the blast increases because there is an attenuation of frequency with distance.

**Reference:** Wyllie, Duncan C. <u>Foundations on Rock</u>, 1<sup>st</sup> Ed, Chapman & Hall, London, 1992

# SECTION 024116 - STRUCTURE DEMOLITION

## PART 1 - GENERAL

#### 1.1 RELATED DOCUMENTS

A. Drawings and general provisions of the Contract, including General and Supplementary Conditions and Division 01 Specification Sections, apply to this Section.

### 1.2 SUMMARY

- A. This Section includes the following:
  - 1. Demolition and removal of buildings and site improvements.
  - 2. Removing below-grade construction.
  - 3. Disconnecting, capping or sealing, and removing site utilities.

#### 1.3 DEFINITIONS

- A. Demolish: Completely remove and legally dispose of off-site.
- B. Recycle: Recovery of demolition waste for subsequent processing in preparation for reuse.

### 1.4 MATERIALS OWNERSHIP

A. Unless otherwise indicated, demolition waste becomes property of Contractor.

## 1.5 SUBMITTALS

- A. Qualification Data: For refrigerant recovery technician.
- B. Proposed Protection Measures: Submit informational report, including drawings, that indicates the measures proposed for protecting individuals and property, for environmental protection, for dust control and for noise control. Indicate proposed locations and construction of barriers.
  - 1. Adjacent Buildings: Detail special measures proposed to protect adjacent buildings to remain.
- C. Predemolition Photographs or Video: Show existing conditions of adjoining construction and site improvements, including finish surfaces, that might be misconstrued as damage caused by building demolition operations.

## 1.6 QUALITY ASSURANCE

- A. Regulatory Requirements: Comply with governing EPA notification regulations before beginning demolition. Comply with hauling and disposal regulations of authorities having jurisdiction.
- B. Standards: Comply with ANSI A10.6 and NFPA 241.

#### 1.7 PROJECT CONDITIONS

- A. Buildings to be demolished will be vacated and their use discontinued before start of the Work.
- B. Buildings immediately adjacent to demolition area will be occupied. Conduct building demolition so operations of occupied buildings will not be disrupted.
  - 1. Provide not less than 72 hours' notice of activities that will affect operations of adjacent occupied buildings.
  - 2. Maintain access to existing walkways, exits, and other facilities used by occupants of adjacent buildings.
    - a. Do not close or obstruct walkways, exits, or other facilities used by occupants of adjacent buildings without written permission from authorities having jurisdiction.
- C. Owner assumes no responsibility for buildings and structures to be demolished.
  - 1. Conditions existing at time of inspection for bidding purpose will be maintained by Owner as far as practical.
- D. Hazardous Materials: It is not expected that hazardous materials will be encountered in the Work.
  - 1. If materials suspected of containing hazardous materials are encountered, do not disturb; immediately notify Architect and Owner. Hazardous materials will be removed by Owner under a separate contract.

## PART 2 - PRODUCTS

#### 2.1 SOIL MATERIALS

A. Satisfactory Soils: Comply with requirements in Division 31 Section "Earth Moving."

## PART 3 - EXECUTION

#### 3.1 EXAMINATION

A. Verify that utilities have been disconnected and capped before starting demolition operations.

- B. Review Project Record Documents of existing construction provided by Owner. Owner does not guarantee that existing conditions are same as those indicated in Project Record Documents.
- C. Inventory and record the condition of items to be removed and salvaged. Provide photographs or video of conditions that might be misconstrued as damage caused by salvage operations.
- D. Verify that hazardous materials have been remediated before proceeding with building demolition operations.

## 3.2 PREPARATION

- A. Existing Utilities: Locate, identify, disconnect, and seal or cap off indicated utilities serving buildings and structures to be demolished.
  - 1. Owner will arrange to shut off indicated utilities when requested by Contractor.
  - 2. Arrange to shut off indicated utilities with utility companies.
  - 3. If removal, relocation, or abandonment of utility services will affect adjacent occupied buildings, then provide temporary utilities that bypass buildings and structures to be demolished and that maintain continuity of service to other buildings and structures.
  - 4. Cut off pipe or conduit a minimum of 24 inches below grade. Cap, valve, or plug and seal remaining portion of pipe or conduit after bypassing according to requirements of authorities having jurisdiction.
- B. Existing Utilities: Refer to Divisions 22 and 26 Sections for shutting off, disconnecting, removing, and sealing or capping utilities. Do not start demolition work until utility disconnecting and sealing have been completed and verified in writing.

## 3.3 PROTECTION

- A. Existing Facilities: Protect adjacent walkways, building entries, and other building facilities during demolition operations. Maintain exits from existing buildings.
- B. Existing Utilities: Maintain utility services to remain and protect from damage during demolition operations.
  - 1. Do not interrupt existing utilities serving adjacent occupied or operating facilities unless authorized in writing by Owner and authorities having jurisdiction.
  - 2. Provide temporary services during interruptions to existing utilities, as acceptable to Owner and authorities having jurisdiction.
    - a. Provide at least 72 hours' notice to occupants of affected buildings if shutdown of service is required during changeover.
- C. Temporary Protection: Erect temporary protection, such as walks, fences, railings, canopies, and covered passageways, where required by authorities having jurisdiction and as indicated. Comply with requirements in Division 01 Section "Temporary Facilities and Controls."
  - 1. Protect adjacent buildings and facilities from damage due to demolition activities.
  - 2. Protect existing site improvements, appurtenances, and landscaping to remain.

- 3. Erect a plainly visible fence around drip line of individual trees or around perimeter drip line of groups of trees to remain.
- 4. Provide temporary barricades and other protection required to prevent injury to people and damage to adjacent buildings and facilities to remain.
- 5. Provide protection to ensure safe passage of people around building demolition area and to and from occupied portions of adjacent buildings and structures.
- 6. Protect walls, windows, roofs, and other adjacent exterior construction that are to remain and that are exposed to building demolition operations.
- 7. Erect and maintain dustproof partitions and temporary enclosures to limit dust, noise, and dirt migration to occupied portions of adjacent buildings.
- D. Remove temporary barriers and protections where hazards no longer exist. Where open excavations or other hazardous conditions remain, leave temporary barriers and protections in place.

## 3.4 DEMOLITION, GENERAL

- A. General: Demolish indicated existing buildings and site improvements completely. Use methods required to complete the Work within limitations of governing regulations and as follows:
  - 1. Do not use cutting torches until work area is cleared of flammable materials. Maintain portable fire-suppression devices during flame-cutting operations.
  - 2. Maintain fire watch during and for at least one hour after flame cutting operations.
  - 3. Maintain adequate ventilation when using cutting torches.
  - 4. Locate building demolition equipment and remove debris and materials so as not to impose excessive loads on supporting walls, floors, or framing.
- B. Site Access and Temporary Controls: Conduct building demolition and debris-removal operations to ensure minimum interference with roads, streets, walks, walkways, and other adjacent occupied and used facilities.
  - 1. Do not close or obstruct streets, walks, walkways, or other adjacent occupied or used facilities without permission from Owner and authorities having jurisdiction. Provide alternate routes around closed or obstructed traffic ways if required by authorities having jurisdiction.
  - 2. Use water mist and other suitable methods to limit spread of dust and dirt. Comply with governing environmental-protection regulations. Do not use water when it may damage adjacent construction or create hazardous or objectionable conditions, such as ice, flooding, and pollution.
- C. Explosives: Use of explosives is not permitted.

## 3.5 DEMOLITION BY MECHANICAL MEANS

A. Proceed with demolition of structural framing members systematically, from higher to lower level. Complete building demolition operations above each floor or tier before disturbing supporting members on the next lower level.

- B. Remove debris from elevated portions of the building by chute, hoist, or other device that will convey debris to grade level in a controlled descent.
  - 1. Remove structural framing members and lower to ground by method suitable to minimize ground impact and dust generation.
- C. Below-Grade Construction: Demolish foundation walls and other below-grade construction.
  - 1. Remove below-grade construction, including basements, foundation walls, and footings, completely.
- D. Existing Utilities: Demolish and remove existing utilities and below-grade utility structures.
  - 1. Piping: Disconnect piping at unions, flanges, valves, or fittings.
  - 2. Wiring Ducts: Disassemble into unit lengths and remove plug-in and disconnecting devices.

#### 3.6 SITE RESTORATION

- A. Below-Grade Areas: Rough grade below-grade areas ready for further excavation or new construction.
- B. Site Grading: Uniformly rough grade area of demolished construction to a smooth surface, free from irregular surface changes. Provide a smooth transition between adjacent existing grades and new grades.

#### 3.7 REPAIRS

A. Promptly repair damage to adjacent buildings caused by demolition operations.

## 3.8 DISPOSAL OF DEMOLISHED MATERIALS

- A. Remove demolition waste materials from Project site. See Division 01 Section "Construction Waste Management and Disposal" for recycling and disposal of demolition waste.
  - 1. Do not allow demolished materials to accumulate on-site.
  - 2. Remove and transport debris in a manner that will prevent spillage on adjacent surfaces and areas.
- B. Do not burn demolished materials.

# 3.9 CLEANING

A. Clean adjacent structures and improvements of dust, dirt, and debris caused by building demolition operations. Return adjacent areas to condition existing before building demolition operations began.

END OF SECTION 024116

## SECTION 033000 - CAST-IN-PLACE CONCRETE

## PART 1 - GENERAL

#### 1.1 SUMMARY

- A. This Section specifies cast-in place concrete, including formwork, reinforcing, mix design, placement procedures, and finishes.
- B. Cast-in-place concrete includes the following:
  - 1. Foundations and footings.
  - 2. Slabs-on-grade.
  - 3. Foundation walls.
  - 4. Slabs on metal decking.
  - 5. Exposed Finished Interior Slabs (-Provide mockup for architect and owner's approval prior to placement)

#### 1.2 SUBMITTALS

- A. General: Submit the following according to Conditions of the Contract and Division 1 Specification Sections.
- B. Product data for proprietary materials and items, including reinforcement and forming accessories, pour stops, admixtures, patching compounds, waterstops, joint systems, curing compounds, dry-shake finish materials, and others if requested by Architect.
- C. Shop drawings for reinforcement detailing fabricating, bending, and placing concrete reinforcement. Comply with ACI 315 "Manual of Standard Practice for Detailing Reinforced Concrete Structures" showing bar schedules, stirrup spacing, bent bar diagrams, and arrangement of concrete reinforcement. Include special reinforcing required for openings through concrete structures.
- D. Shop drawings for formwork indicating fabrication and erection of forms for specific finished concrete surfaces. Show form construction including jointing, special form joints or reveals, location and pattern of form tie placement, and other items that affect exposed concrete visually.
  - 1. Architect's review is for general architectural applications and features only. Designing formwork for structural stability and efficiency is Contractor's responsibility.
- E. Samples of materials as requested by Architect, including names, sources, and descriptions, as follows:
  - 1. Normal weight aggregates.
  - 2. Fiber reinforcement.
  - 3. Reglets.
  - 4. Waterstops.
  - 5. Form liners.
- F. Laboratory test reports for concrete materials and mix design test.

- G. Material certificates in lieu of material laboratory test reports when permitted by Architect. Material certificates shall be signed by manufacturer and Contractor, certifying that each material item complies with or exceeds specified requirements. Provide certification from admixture manufacturers that chloride content complies with specification requirements.
- H. Minutes of pre-installation conference.

### 1.3 QUALITY ASSURANCE

- A. Codes and Standards: Comply with provisions of the following codes, specifications, and standards, except where more stringent requirements are shown or specified:
  - 1. American Concrete Institute (ACI) 301, "Specifications for Structural Concrete for Buildings."
  - 2. ACI 318, "Building Code Requirements for Reinforced Concrete."
  - 3. Concrete Reinforcing Steel Institute (CRSI) "Manual of Standard Practice."
- B. Concrete Testing Service: Engage a testing agency acceptable to Architect to perform material evaluation tests and to design concrete mixes per the requirements of chapter 17 of the IBC.
- C. Materials and installed work may require testing and retesting at any time during progress of Work. Tests, including retesting of rejected materials for installed Work, shall be done at Contractor's expense.
- D. Mockup: At the architects request cast mockup of size indicated or as required to demonstrate typical joints, form tie spacing, and proposed surface finish, texture, and color. Maintain sample panel exposed to view for duration of Project, after Architect's acceptance of visual qualities.
  - 1. Demolish mockup and remove from site when directed by Architect.
- E. Pre-installation Conference: Conduct conference at Project site to comply with requirements in Division 1 Section "Project Management and Coordination."
  - 1. At least 7 days prior to submitting design mixes, conduct a meeting to review detailed requirements for preparing concrete design mixes and to determine procedures for satisfactory concrete operations. Review requirements for submittals, status of coordinating work, and availability of materials. Establish preliminary work progress schedule and procedures for materials inspection, testing, and certifications. Require representatives of each entity directly concerned with cast-in-place concrete to attend conference, including, but not limited to, the following:
    - a. Contractor's superintendent.
    - b. Agency responsible for concrete design mixes.
    - c. Agency responsible for field quality control.
    - d. Agency responsible for quality assurance testing.
    - e. Ready-mix concrete producer.
    - f. Concrete subcontractor.
    - g. Primary admixture manufacturers.

## PART 2 - PRODUCTS

### 2.1 FORM MATERIALS

- A. Forms for Exposed Finish Concrete: Plywood, metal, metal-framed plywood faced, or other acceptable panel-type materials to provide continuous, straight, smooth, exposed surfaces. Furnish in largest practicable sizes to minimize number of joints and to conform to joint system shown on drawings.
  - 1. Use overlaid plywood complying with U.S. Product Standard PS-1 "A-C or B-B High Density Overlaid Concrete Form," Class I.
  - 2. Use plywood complying with U.S. Product Standard PS-1 "B-B (Concrete Form) Plywood," Class I, Exterior Grade or better, mill-oiled and edge-sealed, with each piece bearing legible inspection trademark.
- B. Forms for Unexposed Finish Concrete: Plywood, lumber, metal, or another acceptable material. Provide lumber dressed on at least two edges and one side for tight fit.
- C. Forms for Textured Finish Concrete: Units of face design, size, arrangement, and configuration to match Architect's control sample. Provide solid backing and form supports to ensure stability of textured form liners.
- D. Forms for Cylindrical Columns and Supports: Metal, glass-fiber-reinforced plastic, or paper or fiber tubes that will produce smooth surfaces without joint indications. Provide units with sufficient wall thickness to resist wet concrete loads without deformation.
- G. Form Release Agent: Provide commercial formulation form release agent with a maximum of 350 g/L volatile organic compounds (VOCs) that will not bond with, stain, or adversely affect concrete surfaces and will not impair subsequent treatments of concrete surfaces. Do not allow form release agent to be applied on reinforcing steel.
- H. Form Ties: Factory-fabricated, adjustable-length, removable or snap-off metal form ties designed to prevent form deflection and to prevent spalling of concrete upon removal. Provide units that will leave no metal closer than 1-1/2 inches (38 mm) to the plane of the exposed concrete surface.
  - 1. Provide ties that, when removed, will leave holes not larger than 1 inch (25 mm) in diameter in the concrete surface.

#### 2.2 REINFORCING MATERIALS

- A. Reinforcing Bars: ASTM A 615 Grade 60 (ASTM A 615M Grade 400), deformed.
- B. Steel Wire: ASTM A 82, plain, cold-drawn steel.
- C. Welded Wire Fabric: ASTM A 185, welded steel wire fabric.
- D. Deformed-Steel Welded Wire Fabric: ASTM A 497.
- E. Supports for Reinforcement: Bolsters, chairs, spacers, and other devices for spacing, supporting, and fastening reinforcing bars and welded wire fabric in place. Use wire bar-type supports complying with CRSI specifications.

- 1. For slabs-on-grade, use supports with sand plates or horizontal runners where base material will not support chair legs.
- 2. For exposed-to-view concrete surfaces where legs of supports are in contact with forms, provide supports with legs that are protected by plastic (CRSI, Class 1) or stainless steel (CRSI, Class 2).

### 2.3 CONCRETE MATERIALS

- A. Portland Cement: ASTM C 150, Type I, use Type II at all concrete in contact with soils.
  - 1. Use one brand of cement throughout Project unless otherwise acceptable to Architect.
- B. Fly Ash: ASTM C 618, Type F. The use of Fly Ash and/or Blast Furnace Slag is <u>encouraged</u>. Do not exceed 35% of cement weight.
- C. Normal-Weight Aggregates: ASTM C 33 and as specified. Provide aggregates from a single source for exposed concrete.
  - 1. For exposed exterior surfaces, do not use fine or coarse aggregates that contain substances that cause spalling.
  - 2. Local aggregates not complying with ASTM C 33 that have been shown to produce concrete of adequate strength and durability by special tests or actual service may be used when acceptable to Architect and Engineer.
- D. Water: Potable.
- E. Fiber Reinforcement: Polypropylene fibrillated fibers engineered and designed for secondary reinforcement of concrete slabs, complying with ASTM C 1116, Type III, not less than 3/4 inch long.
  - 1. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Products: Subject to compliance with requirements, provide one of the following:
    - a. Gilco Fibers, Cormix Construction Chemicals.
    - b. Durafiber, Durafiber Corp.
    - c. Fiberstrand 100, Euclid Chemical Co.
    - d. Fibermesh, Fibermesh Co., Div. Synthetic Industries, Inc.
    - e. Forta, Forta Corp.
    - f. Grace Fibers, W.R. Grace & Co.
    - g. Polystrand, Metalcrete Industries
- F. Admixtures, General: Provide concrete admixtures that contain <u>not</u> more than 0.1 percent chloride ions.

- G. Air-Entraining Admixture: ASTM C 260, certified by manufacturer to be compatible with other required admixtures.
  - 1. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Products: Subject to compliance with requirements, provide one of the following:
    - a. Air-Tite, Cormix Construction Chemicals.
    - b. Air-Mix or Perma-Air, Euclid Chemical Co.
    - c. Darex AEA or Daravair, W.R. Grace & Co.
    - d. MB-VR or Micro-Air, Master Builders, Inc.
    - e. Sealtight AEA, W.R. Meadows, Inc.
    - f. Sika AER, Sika Corp.
- H. Water-Reducing Admixture: ASTM C 494, Type A.
  - 1. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Products: Subject to compliance with requirements, provide one of the following:
    - a. Chemtard, ChemMasters Corp.
    - b. PSI N, Cormix Construction Chemicals.
    - c. Eucon WR-75, Euclid Chemical Co.
    - d. WRDA, W.R. Grace & Co.
    - e. Pozzolith Normal or Polyheed, Master Builders, Inc.
    - f. Metco W.R., Metalcrete Industries.
    - g. Prokrete-N, Prokrete Industries.
    - h. Plastocrete 161, Sika Corp.
- I. High-Range Water-Reducing Admixture: ASTM C 494, Type F or Type G.
  - 1. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Products: Subject to compliance with requirements, provide one of the following:
    - a. Super P, Anti-Hydro Co., Inc.
    - b. Cormix 200, Cormix Construction Chemicals.

- c. Eucon 37, Euclid Chemical Co.
- d. WRDA 19 or Daracem, W.R. Grace & Co.
- e. Rheobuild or Polyheed, Master Builders, Inc.
- f. Superslump, Metalcrete Industries.
- g. PSPL, Prokrete Industries.
- h. Sikament 300, Sika Corp.
- J. Water-Reducing, Accelerating Admixture: ASTM C 494, Type E.
  - 1. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Products: Subject to compliance with requirements, provide one of the following:
    - a. Q-Set, Conspec Marketing & Manufacturing Co.
    - b. Lubricon NCA, Cormix Construction Chemicals.
    - c. Accelguard 80, Euclid Chemical Co.
    - d. Daraset, W.R. Grace & Co.
    - e. Pozzutec 20, Master Builders, Inc.
    - f. Accel-Set, Metalcrete Industries.
- K. Water-Reducing, Retarding Admixture: ASTM C 494, Type D.
  - 1. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Products: Subject to compliance with requirements, provide one of the following:
    - a. PSI-R Plus, Cormix Construction Chemicals.
    - b. Eucon Retarder 75, Euclid Chemical Co.
    - c. Daratard-17, W.R. Grace & Co.
    - d. Pozzolith R, Master Builders, Inc.
    - e. Protard, Prokrete Industries.
    - f. Plastiment, Sika Corporation.

## 2.4 RELATED MATERIALS

- A. Reglets: Where sheet flashing or bituminous membranes are terminated in reglets, provide reglets of not less than 0.0217- inch- (0.46-mm-) thick galvanized sheet steel. Fill reglet or cover face opening to prevent intrusion of concrete or debris.
- B. Waterstops: Provide flat, dumbbell-type or centerbulb-type waterstops at construction joints and other joints as indicated. Size to suit joints.
- C. Rubber Waterstops: Corps of Engineers CRD-C 513.
  - 1. Available Manufacturers: Subject to compliance with requirements, manufacturers offering products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Manufacturers: Subject to compliance with requirements, provide products of one of the following:
    - a. The Burke Co.
    - b. Progress Unlimited.
    - c. Williams Products, Inc.
- D. Polyvinyl Chloride Waterstops: Corps of Engineers CRD-C 572.
  - 1. Available Manufacturers: Subject to compliance with requirements, manufacturers offering products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Manufacturers: Subject to compliance with requirements, provide products of one of the following:
    - a. The Burke Co.
    - b. Greenstreak Plastic Products Co.
    - c. W.R. Meadows, Inc.
    - d. Progress Unlimited.
    - e. Schlegel Corp.
    - f. Vinylex Corp.
- E. Nonslip Aggregate Finish: Provide fused aluminum oxide granules or crushed emery as the abrasive aggregate for a nonslip finish, with emery aggregate containing not less than 50 percent aluminum oxide and not less than 25 percent ferric oxide. Use material that is factory-graded, packaged, rustproof, nonglazing, and unaffected by freezing, moisture, and cleaning materials.

- F. Absorptive Cover: Burlap cloth made from jute or kenaf, weighing approximately 9 oz./sq. yd. (305 g/sq. m), complying with AASHTO M 182, Class 2.
- G. Moisture-Retaining Cover: One of the following, complying with ASTM C 171.
  - 1. Waterproof paper.
  - 2. Polyethylene film.
  - 3. Polyethylene-coated burlap.
- H. Liquid Membrane-Forming Curing Compound: Liquid-type membrane-forming curing compound complying with ASTM C 309, Type I, Class A. Moisture loss not more than 0.55 kg/sq. m when applied at 200 sq. ft./gal (4.9 sq. m/L).
  - 1. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Products: Subject to compliance with requirements, provide one of the following:
    - a. A-H 3 Way Sealer, Anti-Hydro Co., Inc.
    - b. Spartan-Cote, The Burke Co.
    - c. Conspec #1, Conspec Marketing & Mfg. Co.
    - d. Sealco 309, Cormix Construction Chemicals.
    - e. Day-Chem Cure and Seal, Dayton Superior Corp.
    - f. Eucocure, Euclid Chemical Co.
    - g. Horn Clear Seal, A.C. Horn, Inc.
    - h. L&M Cure R, L&M Construction Chemicals, Inc.
    - i. Masterkure, Master Builders, Inc.
    - j. CS-309, W.R. Meadows, Inc.
    - k. Seal N Kure, Metalcrete Industries.
    - l. Kure-N-Seal, Sonneborn-Chemrex.
    - m. Stontop CS2, Stonhard, Inc.
- I. Water-Based Acrylic Membrane Curing Compound: ASTM C 309, Type I, Class B.
  - 1. Provide material that has a maximum volatile organic compound (VOC) rating of 350 g/L.
  - 2. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:

- 3. Products: Subject to compliance with requirements, provide one of the following:
  - a. Highseal, Conspec Marketing and Mfg. Co.
  - b. Sealco VOC, Cormix Construction Chemicals.
  - c. Safe Cure and Seal, Dayton Superior Corp.
  - d. Aqua-Cure, Euclid Chemical Co.
  - e. Dress & Seal WB, L&M Construction Chemicals, Inc.
  - f. Masterkure 100W, Master Builders, Inc.
  - g. Vocomp-20, W.R. Meadows, Inc.
  - h. Metcure, Metalcrete Industries.
  - i. Stontop CS1, Stonhard, Inc.
- J. Evaporation Control: Monomolecular film-forming compound applied to exposed concrete slab surfaces for temporary protection from rapid moisture loss.
  - 1. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Products: Subject to compliance with requirements, provide one of the following:
    - a. Aquafilm, Conspec Marketing and Mfg. Co.
    - b. Eucobar, Euclid Chemical Co.
    - c. E-Con, L&M Construction Chemicals, Inc.
    - d. Confilm, Master Builders, Inc.
    - e. Waterhold, Metalcrete Industries.
- K. Bonding Agent: Polyvinyl acetate or acrylic base.
  - 1. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Products: Subject to compliance with requirements, provide one of the following:
    - a. Polyvinyl Acetate (Interior Only):
      - 1) Superior Concrete Bonder, Dayton Superior Corp.
      - 2) Euco Weld, Euclid Chemical Co.
      - 3) Weld-Crete, Larsen Products Corp.

- 4) Everweld, L&M Construction Chemicals, Inc.
- 5) Herculox, Metalcrete Industries.
- 6) Ready Bond, Symons Corp.
- b. Acrylic or Styrene Butadiene:
  - 1) Acrylic Bondcrete, The Burke Co.
  - 2) Strongbond, Conspec Marketing and Mfg. Co.
  - 3) Day-Chem Ad Bond, Dayton Superior Corp.
  - 4) SBR Latex, Euclid Chemical Co.
  - 5) Daraweld C, W.R. Grace & Co.
  - 6) Hornweld, A.C. Horn, Inc.
  - 7) Everbond, L&M Construction Chemicals, Inc.
  - 8) Acryl-Set, Master Builders Inc.
  - 9) Intralok, W.R. Meadows, Inc.
  - 10) Acrylpave, Metalcrete Industries.
  - 11) Sonocrete, Sonneborn-Chemrex.
  - 12) Stonlock LB2, Stonhard, Inc.
  - 13) Strong Bond, Symons Corp.
- L. Epoxy Adhesive: ASTM C 881, two-component material suitable for use on dry or damp surfaces. Provide material type, grade, and class to suit Project requirements.
  - 1. Available Products: Subject to compliance with requirements, products that may be incorporated in the Work include, but are not limited to, the following:
  - 2. Products: Subject to compliance with requirements, provide one of the following:
    - a. Burke Epoxy M.V., The Burke Co.
    - b. Spec-Bond 100, Conspec Marketing and Mfg. Co.
    - c. Resi-Bond (J-58), Dayton Superior.
    - d. Euco Epoxy System #452 or #620, Euclid Chemical Co.
    - e. Epoxtite Binder 2390, A.C. Horn, Inc.
    - f. Epabond, L&M Construction Chemicals, Inc.

- g. Concresive Standard Liquid, Master Builders, Inc.
- h. Rezi-Weld 1000, W.R. Meadows, Inc.
- i. Metco Hi-Mod Epoxy, Metalcrete Industries.
- j. Sikadur 32 Hi-Mod, Sika Corp.
- k. Stonset LV5, Stonhard, Inc.
- 1. R-600 Series, Symons Corp.

#### 2.5 PROPORTIONING AND DESIGNING MIXES

- A. Prepare design mixes for each type and strength of concrete by either laboratory trial batch or field experience methods as specified in ACI 301. For the trial batch method, use an independent testing agency acceptable to Architect for preparing and reporting proposed mix designs.
  - 1. Do not use the same testing agency for field quality control testing.
  - 2. Limit use of fly ash and blast furnace slag to not exceed 35 percent of cement content by weight.
- B. Submit written reports to Architect of each proposed mix for each class of concrete at least 15 days prior to start of Work. Do not begin concrete production until proposed mix designs have been reviewed by Architect and Engineer of Record.
- C. Design mixes to provide normal weight concrete with the following properties as indicated on drawings and schedules:
  - 1. 3,000 psi, 28-day compressive strength; water-cement ratio, 0.60 maximum (non-airentrained)
  - 2. 4,000 psi, 28-day compressive strength; water-cement ratio, 0.5 maximum, (5% air-entrained)
  - 3. 4,000 psi, 28-day compressive strength; water-cement ratio, 0.45 maximum ( 6% airentrained), w/ Fibermesh
  - 3. 3,500 psi, 28-day compressive strength; water-cement ratio, 050 maximum ( 3% airentrained), w/ Fibermesh
- D. Water-Cement Ratio: Provide concrete for following conditions with maximum water-cement (W/C) ratios as follows:
  - 1. Subjected to freezing and thawing: W/C 0.45.
- E. Slump Limits: Proportion and design mixes to result in concrete slump at point of placement as follows:
  - 1. Ramps, slabs, and sloping surfaces: Not more than 3 inches (75 mm).
  - 2. Reinforced foundation systems: Not less than 2 inch and not more than 6 inches.

- 3. Concrete containing high-range water-reducing admixture (superplasticizer): Not more than 8 inches (200 mm) after adding admixture to site-verified 2 3 inch (50 75 mm) slump concrete.
- 4. Other concrete: Not more than 4 inches (100 mm).
- F. Adjustment to Concrete Mixes: Mix design adjustments may be requested by Contractor when characteristics of materials, job conditions, weather, test results, or other circumstances warrant, as accepted by Architect. Laboratory test data for revised mix design and strength results must be submitted to and accepted by Architect before using in Work.
- G. Fiber Reinforcement: Add at manufacturer's recommended rate but not less than 1.5 lb/cu. yd. (0.9 kg/cu. m).

#### 2.6 ADMIXTURES

- A. Use water-reducing admixture or high-range water-reducing admixture (superplasticizer) in concrete, as required, for placement and workability.
- B. Use accelerating admixture in concrete slabs placed at ambient temperatures below 50 deg F (10 deg C).
- C. Use high-range water-reducing admixture in pumped concrete, concrete for heavy-use industrial slabs, architectural concrete, parking structure slabs, concrete required to be watertight, and concrete with water-cement ratios below 0.50.
- D. Use air-entraining admixture in exterior exposed concrete unless otherwise indicated. Add airentraining admixture at manufacturer's prescribed rate to result in concrete at point of placement having total air content with a tolerance of plus or minus 1-1/2 percent within the following limits:
  - 1. Concrete structures and slabs exposed to freezing and thawing, deicer chemicals, or hydraulic pressure:
    - a. 4.0 percent (moderate exposure); 6.0 percent (severe exposure) for 3/4 inch (19 mm) maximum aggregate.
  - 2. Other concrete not exposed to freezing, thawing, or hydraulic pressure, or to receive a surface hardener: 2 to 4 percent air.
- E. Use admixtures for water reduction and set accelerating or retarding in strict compliance with manufacturer's directions.

#### 2.7 CONCRETE MIXING

- A. Ready-Mixed Concrete: Comply with requirements of ASTM C 94, and as specified.
  - 1. When air temperature is between 85 deg F (29 deg C) and 90 deg F (32 deg C), reduce mixing and delivery time from 1-1/2 hours to 75 minutes, and when air temperature is above 90 deg F (32 deg C), reduce mixing and delivery time to 60 minutes.

## PART 3 - EXECUTION

### 3.1 GENERAL

A. Coordinate the installation of joint materials, vapor retarder/barrier, and other related materials with placement of forms and reinforcing steel and Insulated Concrete Forms

### 3.2 FORMS

A. General: Design, erect, support, brace, and maintain formwork to support vertical, lateral, static, and dynamic loads that might be applied until concrete structure can support such loads. Construct formwork so concrete members and structures are of correct size, shape, alignment, elevation, and position. Maintain formwork construction tolerances and surface irregularities complying with the following ACI 347 limits:

## 1. **Provide Class A tolerances for concrete surfaces exposed to view.**

- 2. Provide Class C tolerances for other concrete surfaces.
- B. Construct forms to sizes, shapes, lines, and dimensions shown and to obtain accurate alignment, location, grades, level, and plumb work in finished structures. Provide for openings, offsets, sinkages, keyways, recesses, moldings, rustications, reglets, chamfers, blocking, screeds, bulkheads, anchorages and inserts, and other features required in the Work. Use selected materials to obtain required finishes. Solidly butt joints and provide backup at joints to prevent cement paste from leaking.
- C. Fabricate forms for easy removal without hammering or prying against concrete surfaces. Provide crush plates or wrecking plates where stripping may damage cast concrete surfaces. Provide top forms for inclined surfaces where slope is too steep to place concrete with bottom forms only. Kerf wood inserts for forming keyways, reglets, recesses, and the like for easy removal.
- D. Provide temporary openings for clean-outs and inspections where interior area of formwork is inaccessible before and during concrete placement. Securely brace temporary openings and set tightly to forms to prevent losing concrete mortar. Locate temporary openings in forms at inconspicuous locations.
- E. Chamfer exposed corners and edges as indicated, using wood, metal, PVC, or rubber chamfer strips fabricated to produce uniform smooth lines and tight edge joints.
- F. Provisions for Other Trades: Provide openings in concrete formwork to accommodate work of other trades. Determine size and location of openings, recesses, and chases from trades providing such items. Accurately place and securely support items built into forms.
- G. Cleaning and Tightening: Thoroughly clean forms and adjacent surfaces to receive concrete. Remove chips, wood, sawdust, dirt, or other debris just before placing concrete. Retighten forms and bracing before placing concrete, as required, to prevent mortar leaks and maintain proper alignment.

## 3.3 PLACING REINFORCEMENT

- A. General: Comply with Concrete Reinforcing Steel Institute's recommended practice for "Placing Reinforcing Bars," for details and methods of reinforcement placement and supports and as specified.
  - 1. Avoiding cutting or puncturing vapor retarder/barrier during reinforcement placement and concreting operations. Repair damages before placing concrete.
- B. Clean reinforcement of loose rust and mill scale, earth, ice, and other materials that reduce or destroy bond with concrete.
- C. Accurately position, support, and secure reinforcement against displacement. Locate and support reinforcing by metal chairs, runners, bolsters, spacers, and hangers, as approved by Architect.
- D. Place reinforcement to maintain minimum coverages as indicated for concrete protection. Arrange, space, and securely tie bars and bar supports to hold reinforcement in position during concrete placement operations. Set wire ties so ends are directed into concrete, not toward exposed concrete surfaces.
- E. Install welded wire fabric in lengths as long as practicable. Lap adjoining pieces at least one full mesh and lace splices with wire. Offset laps of adjoining widths to prevent continuous laps in either direction.

# 3.4 JOINTS

- A. Construction Joints: Locate and install construction joints so they do not impair strength or appearance of the structure, as acceptable to Architect.
- B. Provide keyways at least 1-1/2 inches (38 mm) deep in construction joints in walls and slabs. Bulkheads designed and accepted for this purpose may be used for slabs.
- C. Place construction joints perpendicular to main reinforcement. Continue reinforcement across construction joints except as indicated otherwise. Do not continue reinforcement through sides of strip placements.
- D. Use bonding agent on existing concrete surfaces that will be joined with fresh concrete.
- E. Waterstops: Provide waterstops in construction joints as indicated. Install waterstops to form continuous diaphragm in each joint. Support and protect exposed waterstops during progress of Work. Field-fabricate joints in waterstops according to manufacturer's printed instructions.
- F. Isolation Joints in Slabs-on-Grade: Construct isolation joints in slabs-on-grade at points of contact between slabs-on-grade and vertical surfaces, such as column pedestals, foundation walls, grade beams, and other locations, as indicated.
  - 1. Joint fillers and sealants are specified in Division 7 Section "Joint Sealants."
- G. Contraction (Control) Joints in Slabs-on-Grade: Construct contraction joints in slabs-on-grade to form panels of patterns as shown. Use saw cuts 1/8 inch (3 mm) wide by one-fourth of slab depth or inserts 1/4 inch (6 mm) wide by one-fourth of slab depth, unless otherwise indicated.
  - 1. Form contraction joints by inserting premolded plastic, hardboard, or fiberboard strip into fresh concrete until top surface of strip is flush with slab surface. Tool slab edges round

on each side of insert. After concrete has cured, remove inserts and clean groove of loose debris.

- 2. Contraction joints in unexposed floor slabs may be formed by saw cuts as soon as possible after slab finishing as may be safely done without dislodging aggregate.
- 3. If joint pattern is not shown, provide joints not exceeding 12 ft. (4.5 m) in either direction and located to conform to bay spacing wherever possible (at column centerlines, half bays, third bays).
- 4. Joint fillers and sealants are specified in Division 7 Section "Joint Sealants."

## 3.5 INSTALLING EMBEDDED ITEMS

- A. General: Set and build into formwork anchorage devices and other embedded items required for other work that is attached to or supported by cast-in-place concrete. Use setting drawings, diagrams, instructions, and directions provided by suppliers of items to be attached.
- B. Install reglets to receive top edge of foundation sheet waterproofing and to receive through-wall flashings in outer face of concrete frame at exterior walls, where flashing is shown at lintels, relieving angles, and other conditions.
- C. Install dovetail anchor slots in concrete structures as indicated on drawings.
- D. Forms for Slabs: Set edge forms, bulkheads, and intermediate screed strips for slabs to achieve required elevations and contours in finished surfaces. Provide and secure units to support screed strips using strike-off templates or compacting-type screeds.

#### 3.6 PREPARING FORM SURFACES

- A. General: Coat contact surfaces of forms with an approved, nonresidual, low-VOC, form-coating compound before placing reinforcement.
- B. Do not allow excess form-coating material to accumulate in forms or come into contact with inplace concrete surfaces against which fresh concrete will be placed. Apply according to manufacturer's instructions.
  - 1. Coat steel forms with a nonstaining, rust-preventative material. Rust-stained steel form-work is not acceptable.

## 3.7 CONCRETE PLACEMENT

- A. Inspection: Before placing concrete, inspect and complete formwork installation, reinforcing steel, and items to be embedded or cast in. Notify other trades to permit installation of their work.
- B. General: Comply with ACI 304, "Guide for Measuring, Mixing, Transporting, and Placing Concrete," and as specified.
- C. Deposit concrete continuously or in layers of such thickness that no new concrete will be placed on concrete that has hardened sufficiently to cause seams or planes of weakness. If a section cannot be placed continuously, provide construction joints as specified. Deposit concrete to avoid segregation at its final location.

- D. Placing Concrete in Forms: Deposit concrete in forms in horizontal layers no deeper than 24 inches (600 mm) and in a manner to avoid inclined construction joints. Where placement consists of several layers, place each layer while preceding layer is still plastic to avoid cold joints.
  - 1. Consolidate placed concrete by mechanical vibrating equipment supplemented by handspading, rodding, or tamping. Use equipment and procedures for consolidation of concrete complying with ACI 309.
  - 2. Do not use vibrators to transport concrete inside forms. Insert and withdraw vibrators vertically at uniformly spaced locations no farther than the visible effectiveness of the machine. Place vibrators to rapidly penetrate placed layer and at least 6 inches (150 mm) into preceding layer. Do not insert vibrators into lower layers of concrete that have begun to set. At each insertion, limit duration of vibration to time necessary to consolidate concrete and complete embedment of reinforcement and other embedded items without causing mix to segregate.
- E. Placing Concrete Slabs: Deposit and consolidate concrete slabs in a continuous operation, within limits of construction joints, until completing placement of a panel or section.
  - 1. Consolidate concrete during placement operations so that concrete is thoroughly worked around reinforcement, other embedded items and into corners.
  - 2. Bring slab surfaces to correct level with a straightedge and strike off. Use bull floats or darbies to smooth surface free of humps or hollows. Do not disturb slab surfaces prior to beginning finishing operations.
  - 3. Maintain reinforcing in proper position on chairs during concrete placement.
- F. Cold-Weather Placement: Comply with provisions of ACI 306 and as follows. Protect concrete work from physical damage or reduced strength that could be caused by frost, freezing actions, or low temperatures.
- G. When air temperature has fallen to or is expected to fall below 40 deg F (4 deg C), uniformly heat water and aggregates before mixing to obtain a concrete mixture temperature of not less than 50 deg F (10 deg C) and not more than 80 deg F (27 deg C) at point of placement.
  - 1. Do not use frozen materials or materials containing ice or snow. Do not place concrete on frozen subgrade or on subgrade containing frozen materials.
  - 2. Do not use calcium chloride, salt, or other materials containing antifreeze agents or chemical accelerators unless otherwise accepted in mix designs.
- H. Hot-Weather Placement: When hot weather conditions exist that would impair quality and strength of concrete, place concrete complying with ACI 305 and as specified.
  - 1. Cool ingredients before mixing to maintain concrete temperature at time of placement to below 90 deg F (32 deg C). Mixing water may be chilled or chopped ice may be used to control temperature, provided water equivalent of ice is calculated to total amount of mixing water. Using liquid nitrogen to cool concrete is Contractor's option.
  - 2. Cover reinforcing steel with water-soaked burlap if it becomes too hot, so that steel temperature will not exceed the ambient air temperature immediately before embedding in concrete.

- 3. Fog spray forms, reinforcing steel, and subgrade just before placing concrete. Keep subgrade moisture uniform without puddles or dry areas.
- 4. Use water-reducing retarding admixture when required by high temperatures, low humidity, or other adverse placing conditions, as acceptable to Architect.

## 3.8 FINISHING FORMED SURFACES

- A. Rough-Formed Finish: Provide a rough-formed finish on formed concrete surfaces not exposed to view in the finished Work or concealed by other construction. This is the concrete surface having texture imparted by form-facing material used, with the holes and defective areas repaired and patched, and fins and other projections exceeding 1/4 inch (6 mm) in height rubbed down or chipped off.
- B. Smooth-Formed Finish: Provide a smooth-formed finish on formed concrete surfaces exposed to view or to be covered with a coating material applied directly to concrete, or a covering material applied directly to concrete, such as waterproofing, dampproofing, veneer plaster, painting, or another similar system. This is an as-cast concrete surface obtained with selected form-facing material, arranged in an orderly and symmetrical manner with a minimum of seams. Repair and patch defective areas with fins and other projections completely removed and smoothed.
- C. Smooth-Rubbed Finish: Provide smooth-rubbed finish on scheduled concrete surfaces that have received smooth-formed finish treatment not later than 1 day after form removal.
  - 1. Moisten concrete surfaces and rub with carborundum brick or another abrasive until producing a uniform color and texture. Do not apply cement grout other than that created by the rubbing process.
- D. Grout-Cleaned Finish: Provide grout-cleaned finish on scheduled concrete surfaces that have received smooth-formed finish treatment.
  - 1. Combine one part portland cement to one and one-half parts fine sand by volume, and a 50:50 mixture of acrylic or styrene butadiene-based bonding admixture and water to form the consistency of thick paint. Blend standard portland cement and white portland cement in amounts determined by trial patches so that final color of dry grout will match adjacent surfaces.
  - 2. Thoroughly wet concrete surfaces, apply grout to coat surfaces, and fill small holes. Remove excess grout by scraping and rubbing with clean burlap. Keep damp by fog spray for at least 36 hours after rubbing.
- E. Related Unformed Surfaces: At tops of walls, horizontal offsets, and similar unformed surfaces adjacent to formed surfaces, strike-off smooth and finish with a texture matching adjacent formed surfaces. Continue final surface treatment of formed surfaces uniformly across adjacent unformed surfaces unless otherwise indicated.

# 3.9 MONOLITHIC SLAB FINISHES

A. Scratch Finish: Apply scratch finish to monolithic slab surfaces to receive concrete floor topping or mortar setting beds for tile, portland cement terrazzo, and other bonded applied cementitious finish flooring material, and where indicated.

- 1. After placing slabs, finish surface to tolerances of F(F) 15 (floor flatness) and F(L) 13 (floor levelness) measured according to ASTM E 1155 (ASTM E 1155M). Slope surfaces uniformly to drains where required. After leveling, roughen surface before final set with stiff brushes, brooms, or rakes.
- B. Float Finish: Apply float finish to monolithic slab surfaces to receive trowel finish and other finishes as specified; slab surfaces to be covered with membrane or elastic waterproofing, membrane or elastic roofing, or sand-bed terrazzo; and where indicated.
  - 1. After screeding, consolidating, and leveling concrete slabs, do not work surface until ready for floating. Begin floating, using float blades or float shoes only, when surface water has disappeared, or when concrete has stiffened sufficiently to permit operation of power-driven floats, or both. Consolidate surface with power-driven floats or by hand-floating if area is small or inaccessible to power units. Finish surfaces to tolerances of F(F) 18 (floor flatness) and F(L) 15 (floor levelness) measured according to ASTM E 1155 (ASTM E 1155M). Cut down high spots and fill low spots. Uniformly slope surfaces to drains. Immediately after leveling, refloat surface to a uniform, smooth, granular texture.
- C. Trowel Finish: Apply a trowel finish to monolithic slab surfaces exposed to view and slab surfaces to be covered with resilient flooring, carpet, ceramic or quarry tile, paint, or another thin film-finish coating system.
  - 1. After floating, begin first trowel-finish operation using a power-driven trowel. Begin final troweling when surface produces a ringing sound as trowel is moved over surface. Consolidate concrete surface by final hand-troweling operation, free of trowel marks, uniform in texture and appearance, and finish surfaces to tolerances of F(F) 20 (floor flatness) and F(L) 17 (floor levelness) measured according to ASTM E 1155 (ASTM E 1155M). Grind smooth any surface defects that would telegraph through applied floor covering system.
- D. Trowel and Fine Broom Finish: Where ceramic or quarry tile is to be installed with thin-set mortar, apply a trowel finish as specified, then immediately follow by slightly scarifying the surface with a fine broom.
- E. Nonslip Broom/Grooved Finish: Apply a nonslip broom/grooved finish to exterior concrete platforms, steps, and ramps, and elsewhere as indicated.
  - 1. Immediately after float finishing, slightly roughen concrete surface by brooming/grooveing with fiber-bristle broom perpendicular to main traffic route or groove trowel as specified by Architect. Coordinate required final finish with Architect before application.
- F. Nonslip Aggregate Finish: Apply nonslip aggregate finish to concrete stair treads, platforms, ramps, sloped walks, and where indicated.
  - 1. After completing float finishing and before starting trowel finish, uniformly spread dampened nonslip aggregate at a rate of 25 lb per 100 sq. ft. (12 kg/10 sq. m) of surface. Tamp aggregate flush with surface using a steel trowel, but do not force below surface. After broadcasting and tamping, apply trowel finishing as specified.
  - 2. After curing, lightly work surface with a steel wire brush or an abrasive stone, and water to expose nonslip aggregate.

- G. Colored Wear-Resistant Finish: Apply a colored wear-resistant finish to monolithic slab surface indicated.
  - 1. Apply dry shake materials for the colored wear-resistant finish at a rate of 100 lb per 100 sq. ft. (49 kg/10 sq. m), unless a greater amount is recommended by material manufacturer.
  - 2. Cast a trial slab approximately 10 ft. (3 m) square to determine actual application rate, color, and finish, as acceptable to Architect.
  - 3. Immediately following the first floating operation, uniformly distribute with mechanical spreader approximately two-thirds of the required weight of the dry shake material over the concrete surface, and embed by power floating. Follow floating operation with second shake application, uniformly distributing remainder of dry shake material with overlapping applications to ensure uniform color, and embed by power floating.
  - 4. After broadcasting and floating, apply a trowel finish as specified. Cure slab surface with a curing compound recommended by the dry shake material manufacturer. Apply the curing compound immediately after the final finishing.

#### 3.10 MISCELLANEOUS CONCRETE ITEMS

- A. Filling In: Fill in holes and openings left in concrete structures for passage of work by other trades, unless otherwise shown or directed, after work of other trades is in place. Mix, place, and cure concrete as specified to blend with in-place construction. Provide other miscellaneous concrete filling shown or required to complete Work.
- B. Curbs: Provide monolithic finish to interior curbs by stripping forms while concrete is still green and by steel-troweling surfaces to a hard, dense finish with corners, intersections, and terminations slightly rounded.
- C. Equipment Bases and Foundations: Provide machine and equipment bases and foundations as shown on drawings. Set anchor bolts for machines and equipment to template at correct elevations, complying with diagrams or templates of manufacturer furnishing machines and equipment.
- D. Steel Pan Stairs: Provide concrete fill for steel pan stair treads, landings, and associated items. Cast-in safety inserts and accessories as shown on drawings. Screed, tamp, and trowel-finish concrete surfaces.

# 3.11 CONCRETE CURING AND PROTECTION

- A. General: Protect freshly placed concrete from premature drying and excessive cold or hot temperatures. In hot, dry, and windy weather protect concrete from rapid moisture loss before and during finishing operations with an evaporation-control material. Apply according to manufacturer's instructions after screeding and bull floating, but before power floating and troweling.
- B. Start initial curing as soon as free water has disappeared from concrete surface after placing and finishing. Weather permitting, keep continuously moist for not less than 7 days.
- C. Curing Methods: Cure concrete by curing compound, by moist curing, by moisture-retaining cover curing, or by combining these methods, as specified.

- D. Provide moisture curing by the following methods:
  - 1. Keep concrete surface continuously wet by covering with water.
  - 2. Use continuous water-fog spray.
  - 3. Cover concrete surface with specified absorptive cover, thoroughly saturate cover with water, and keep continuously wet. Place absorptive cover to provide coverage of concrete surfaces and edges, with a 4 inch (100 mm) lap over adjacent absorptive covers.
- E. Provide moisture-retaining cover curing as follows:
  - 1. Cover concrete surfaces with moisture-retaining cover for curing concrete, placed in widest practicable width with sides and ends lapped at least 3 inches (75 mm) and sealed by waterproof tape or adhesive. Immediately repair any holes or tears during curing period using cover material and waterproof tape.
- F. Apply curing compound on exposed interior slabs and on exterior slabs, walks, and curbs as follows:
  - 1. Apply curing compound to concrete slabs as soon as final finishing operations are complete (within 2 hours and after surface water sheen has disappeared). Apply uniformly in continuous operation by power spray or roller according to manufacturer's directions. Recoat areas subjected to heavy rainfall within 3 hours after initial application. Maintain continuity of coating and repair damage during curing period.
  - 2. Use membrane curing compounds that will not affect surfaces to be covered with finish materials applied directly to concrete.
- G. Curing Formed Surfaces: Cure formed concrete surfaces, including underside of beams, supported slabs, and other similar surfaces, by moist curing with forms in place for the full curing period or until forms are removed. If forms are removed, continue curing by methods specified above, as applicable.
- H. Curing Unformed Surfaces: Cure unformed surfaces, including slabs, floor topping, and other flat surfaces, by applying the appropriate curing method.
  - 1. Final cure concrete surfaces to receive finish flooring with a moisture-retaining cover, unless otherwise directed.

## 3.12 REMOVING FORMS

- A. General: Formwork not supporting weight of concrete, such as sides of beams, walls, columns, and similar parts of the work, may be removed after cumulatively curing at not less than 50 deg F (10 deg C) for 24 hours after placing concrete, provided concrete is sufficiently hard to not be damaged by form-removal operations, and provided curing and protection operations are maintained.
- B. Formwork supporting weight of concrete, such as beam soffits, joists, slabs, and other structural elements, may not be removed in less than 14 days or until concrete has attained at least 75 percent of design minimum compressive strength at 28 days. Determine potential compressive strength of in-place concrete by testing field-cured specimens representative of concrete location or members.

C. Form-facing material may be removed 4 days after placement only if shores and other vertical supports have been arranged to permit removal of form-facing material without loosening or disturbing shores and supports.

### 3.13 REUSING FORMS

- A. Clean and repair surfaces of forms to be reused in the Work. Split, frayed, delaminated, or otherwise damaged form-facing material will not be acceptable for exposed surfaces. Apply new form-coating compound as specified for new formwork.
- B. When forms are extended for successive concrete placement, thoroughly clean surfaces, remove fins and laitance, and tighten forms to close joints. Align and secure joint to avoid offsets. Do not use patched forms for exposed concrete surfaces except as acceptable to Architect.

# 3.14 CONCRETE SURFACE REPAIRS

- A. Patching Defective Areas: Repair and patch defective areas with cement mortar immediately after removing forms, when acceptable to Architect.
- B. Mix dry-pack mortar, consisting of one part portland cement to 2-1/2 parts fine aggregate passing a No. 16 mesh (1.2 mm) sieve, using only enough water as required for handling and placing.
  - 1. Cut out honeycombs, rock pockets, voids over 1/4 inch (6 mm) in any dimension, and holes left by tie rods and bolts down to solid concrete but in no case to a depth less than 1 inch (25 mm). Make edges of cuts perpendicular to the concrete surface. Thoroughly clean, dampen with water, and brush-coat the area to be patched with bonding agent. Place patching mortar before bonding agent has dried.
  - 2. For surfaces exposed to view, blend white portland cement and standard portland cement so that, when dry, patching mortar will match surrounding color. Provide test areas at inconspicuous locations to verify mixture and color match before proceeding with patching. Compact mortar in place and strike-off slightly higher than surrounding surface.
- C. Repairing Formed Surfaces: Remove and replace concrete having defective surfaces if defects cannot be repaired to satisfaction of Architect. Surface defects include color and texture irregularities, cracks, spalls, air bubbles, honeycomb, rock pockets, fins and other projections on the surface, and stains and other discolorations that cannot be removed by cleaning. Flush out form tie holes and fill with dry-pack mortar or precast cement cone plugs secured in place with bonding agent.
  - 1. Repair concealed formed surfaces, where possible, containing defects that affect the concrete's durability. If defects cannot be repaired, remove and replace the concrete.
- D. Repairing Unformed Surfaces: Test unformed surfaces, such as monolithic slabs, for smoothness and verify surface tolerances specified for each surface and finish. Correct low and high areas as specified. Test unformed surfaces sloped to drain for trueness of slope and smoothness by using a template having the required slope.
  - 1. Repair finished unformed surfaces containing defects that affect the concrete's durability. Surface defects include crazing and cracks in excess of 0.01 inch (0.25 mm) wide or that penetrate to the reinforcement or completely through nonreinforced sections regardless of width, spalling, popouts, honeycombs, rock pockets, and other objectionable conditions.

- 2. Correct high areas in unformed surfaces by grinding after concrete has cured at least 14 days.
- 3. Correct low areas in unformed surfaces during or immediately after completing surface finishing operations by cutting out low areas and replacing with patching mortar. Finish repaired areas to blend into adjacent concrete. Proprietary underlayment compounds may be used when acceptable to Architect.
- 4. Repair defective areas, except random cracks and single holes not exceeding 1 inch (25 mm) in diameter, by cutting out and replacing with fresh concrete. Remove defective areas with clean, square cuts and expose reinforcing steel with at least 3/4 inch (19 mm) clearance all around. Dampen concrete surfaces in contact with patching concrete and apply bonding agent. Mix patching concrete of same materials to provide concrete of same type or class as original concrete. Place, compact, and finish to blend with adjacent finished concrete. Cure in same manner as adjacent concrete.
- E. Repair isolated random cracks and single holes 1 inch (25 mm) or less in diameter by dry-pack method. Groove top of cracks and cut out holes to sound concrete and clean of dust, dirt, and loose particles. Dampen cleaned concrete surfaces and apply bonding compound. Place dry-pack before bonding agent has dried. Compact dry-pack mixture in place and finish to match adjacent concrete. Keep patched area continuously moist for at least 72 hours.
- F. Perform structural repairs with prior approval of Architect for method and procedure, using specified epoxy adhesive and mortar.
- G. Repair methods not specified above may be used, subject to acceptance of Architect.

#### 3.15 QUALITY CONTROL TESTING DURING CONSTRUCTION

- A. General: The Owner will employ a testing agency to perform tests and to submit test reports.
- B. Sampling and testing for quality control during concrete placement <u>may</u> include the following, as directed by Architect or Owners Representative.
  - 1. Sampling Fresh Concrete: ASTM C 172, except modified for slump to comply with ASTM C 94. Provide one set of tests for each 50 cu. yd. of each type of concrete for each day's pour; provide one set of tests of the following:
    - a. Slump: ASTM C 143; one test at point of discharge; additional tests when concrete consistency seems to have changed.
    - b. Air Content: ASTM C 173, volumetric method for lightweight or normal weight concrete; ASTM C 231, pressure method for normal weight concrete.
    - c. Concrete Temperature: ASTM C 1064; one test hourly when air temperature is 40 deg F (4 deg C) and below.
    - d. Compression Test Specimen: ASTM C 31; one set of four standard cylinders for each compressive-strength test, unless otherwise directed. Mold and store cylinders for laboratory-cured test specimens except when field-cured test specimens are required.

- e. Compressive-Strength Tests: ASTM C 39; one specimen tested at 7 days, two specimens tested at 28 days, and one specimen retained in reserve for later testing if required.
- 2. When frequency of testing will provide fewer than five strength tests for a given class of concrete, conduct testing from at least five randomly selected batches or from each batch if fewer than five are used.
- 3. When total quantity of a given class of concrete is less than 50 cu. yd. (38 cu. m), Architect may waive strength testing if adequate evidence of satisfactory strength is provided.
- 4. When strength of field-cured cylinders is less than 85 percent of companion laboratorycured cylinders, evaluate current operations and provide corrective procedures for protecting and curing the in-place concrete.
- 5. Strength level of concrete will be considered satisfactory if averages of sets of three consecutive strength test results equal or exceed specified compressive strength and no individual strength test result falls below specified compressive strength by more than 500 psi (3.4 MPa).
- C. Test results will be reported in writing to Architect, Structural Engineer, ready-mix producer, and Contractor within 24 hours after tests. Reports of compressive strength tests shall contain the Project identification name and number, date of concrete placement, name of concrete test-ing service, concrete type and class, location of concrete batch in structure, design compressive strength at 28 days, concrete mix proportions and materials, compressive breaking strength, and type of break for both 7-day tests and 28-day tests.
- D. Nondestructive Testing: Impact hammer, sonoscope, or other nondestructive device may be permitted but shall not be used as the sole basis for acceptance or rejection.
- E. Additional Tests: The testing agency will make additional tests of in-place concrete when test results indicate specified concrete strengths and other characteristics have not been attained in the structure, as directed by Architect. Testing agency may conduct tests to determine adequacy of concrete by cored cylinders complying with ASTM C 42, or by other methods as directed.

END OF SECTION 033000