# - T. . - Mobile <br> 15 Commerce Way Suite B <br> Norton, MA 02766 

## StRUCTURAL ANALYSIS 4PB1259A



Address:
638 Congress Street
Portland, ME 04101 Date:

## J ULY 11, 2017



CHAPPELL
ENGINEERING
ASSOCIATES, LLC
Civil-Structural•Land Surveying

July 11, 2017
-T---Mobile
15 Commerce Way
Suite B
Norton, MA 02766

## Structural Analysis of Antenna Loads

RE:

| Site Number | 4PB1259A |
| :--- | :--- |
| Site Name | PB259 / Comfac - Lafayette |
| Site Address | 638 Congress Street, Portland, ME 04101 |

To whom it may concern:
Chappell Engineering Associates, LLC has reviewed the existing antenna installation at the above referenced location. Based upon the site visit completed on 06-05-2017, the alpha, beta and gamma sector antennas are located on the face of the existing rooftop penthouse. The existing antenna mounts consist of cantilevered antenna pipe masts secured to the face of the penthouse.

The existing T-Mobile sectors currently consist of two (2) existing panel antennas per sector. T-Mobile currently proposes to reconfigure the existing antenna configuration by removing and replacing one existing antenna in its place and installing a proposed antenna on the existing antenna mount. Additionally, three (3) Remote Radio Units and three (3) style 3CX TMA's will be located on the exiting antenna mounts. Also, two (2) hybrid DC/Fiber cables will be run to service the proposed antennas

The current antenna configuration consists of:

| Sectors | Status | Antenna/ Appurtenance | Dimensions (in) | Location |
| :--- | :--- | :--- | :--- | :--- |
| Alpha, Beta , Gamma | Existing | (1) RFS APX16DWV-S-E-A20 | $56 \mathrm{H} \times 13 \mathrm{~W} \times 3.2 \mathrm{D}$ | Face of Penthouse |
|  | Existing | (1) Andrew LNX-6515DS-A1M | $96.6 \mathrm{H} \times 11.9 \mathrm{~W} \times 7.1 \mathrm{D}$ | Face of Penthouse |
|  | Existing | (1) RFS Twin TMA's | $12 \mathrm{H} \times 10 \mathrm{~W} \times 4 \mathrm{D}$ | Face of Penthouse |
|  | Existing | (2) TMA's | $14 \mathrm{H} \times 6 \mathrm{~W} \times 4 \mathrm{D}$ | Face of Penthouse |

T-Mobile currently proposes to re-configure the existing antennas as shown (final total configuration):

| Sectors | Status | Antenna/ Appurtenance | Dimensions (in) | Location |
| :---: | :---: | :---: | :---: | :---: |
| Alpha, Beta , Gamma | Proposed | (1) Commscope FF-65C-R2 Panel | $96 \mathrm{H} \times 25.2 \mathrm{~W} \times 9.3 \mathrm{D}$ | Face of Penthouse |
|  | Proposed | (1) Ericsson 4478 B71 RRU | $15 \mathrm{H} \times 13.2 \mathrm{~W} \times 7.4 \mathrm{D}$ | Face of Penthouse |
|  | Existing | (1) RFS APX16DWV-S-E-A20 Panel | $56 \mathrm{H} \times 13 \mathrm{~W} \times 3.2 \mathrm{D}$ | Face of Penthouse |
|  | Proposed | (1) RFS Style 3CX TMA | $11.2 \mathrm{H} \times 8.0 \mathrm{~W} \times 4.9 \mathrm{D}$ | Face of Penthouse |
|  | Proposed | (2) RFS ACU-A20-S | $4 \mathrm{H} \times 1.6 \mathrm{~W} \times 3.5 \mathrm{D}$ | Face of Penthouse |

The proposed antennas will be installed on the existing pipe currently supporting the existing AIR antennas.
Based upon our review of the loads, our stability analysis of the existing antenna mounting pipes, Chappell Engineering Associates, LLC has determined that the existing antenna support structures have adequate capacity to support the proposed L600MHz modernization upgrade configuration as shown above. Photos of the existing antenna mounts are enclosed for your convenience. A copy of the proposed L600MHz antenna upgrade mounting plan being proposed by Chappell Engineering is also enclosed.

If you have any questions regarding this matter, please do not hesitate to call.



Alpha Sector Antennas


Beta Sector Antennas


Gamma Sector Antennas


| SCALE $=1: 18$ | DATE: $7 / 11 / 17$ |
| :--- | :--- |


| Load no. 1: Selfweight (units - kips ft.) |
| :--- |
| I BEAM LOADS |
| SELF X3-1. B 1 TO 11 |
| I END |
| F O R C E S U M M A TI O N |
| FX1 $=0$. kip |
| FX2=0. kip |
| FX3 $=-0.0996$ kip |

## Load no. 2: Antenna X2 (units - kips ft.)

```
/ BEAM LOADS
DIST GL FX2 O. B }3
/ BEAM LOADS
DIST GL FX2 0.075 B 3 2
/ END
FORCE SUMMATION
FX1=0. kip
FX2=0.6 kip
FX3=0. kip
```


## Load no. 3: Antenna X1 (units - kips ft.)

```
/ BEAM LOADS
DIST GL FX1 0.03 B 3 2
/ END
FORCE SUMMATION
FX1=0.24 kip
FX2=0. kip
FX3=0. kip
```


## Load no. 4: Antenna Dead Load (units - kips ft.)

| Load no. 4: Antenna Dead Load (units - kips ft.) |
| :--- |
| F O R C E S U M M A T I O N |
| FX1 $=0$. kip |
| FX2=0. kip |
| FX3=-0.11 kip |


| 638 Congress St Portland T-Mobile |
| :--- |
| Load 1: Selfweight |
| SCALE $=1: 20$ |



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| :--- |
| Load 2: Antenna $\times 2$ |
| SCALE $=1: 20$ |



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Load 3: Antenna X1


| SCALE $=1: 20$ | UNITS: kip ft | DATE: $7 / 11 / 17$ |
| :--- | :--- | :--- |

638 Congress St Portland $T$-Mobile

Load 4: Antenna Dead Load

| SCALE $=1: 20$ | UNITS: kip ft | DATE: $7 / 11 / 17$ |
| :--- | :--- | :--- |




Detailed Results Table
Moments: kips*foot , Forces: kips , Stresses: ksi , Section prop.: inch


|  | Section: PIPE 2-1/2 |
| ---: | :--- |
| IX | $=1.53 \mathrm{Iy}=$ |
| $\mathrm{D}=$ | $1.53 \mathrm{in} 4 \mathrm{Sx}=1.06 \mathrm{Sy}=1.06 \mathrm{in} 3$ Area $=1.70$ |
| $\mathrm{~J}=$ | $3.87 \mathrm{t}=$ |
| 0.20 Cw | $=0.00 \mathrm{in} 6$ |



Max. AXIAL Force $=0.05$ (tens.), $\quad-0.09$ (compr.) Max. SHEAR Force $=0.47$

| DESIGN | EQUATION | FACTORS | VALUES | RESULT |
| :---: | :---: | :---: | :---: | :---: |
| V2 Shear (F4-1) | $\begin{aligned} & \mathrm{V} /\left(\mathrm{Av} \mathrm{v}^{\mathrm{F} v}\right)<1.00 \\ & \mathrm{Fv}=0.4^{*} \mathrm{Fy} \end{aligned}$ | $\mathrm{Av}=1.02$ | $\begin{aligned} & V=0.47 \\ & \mathrm{Fv}=14.00 \end{aligned}$ | 0.03 |
| M3 Moment (F3-1) | $\frac{\mathrm{M}}{\mathrm{~S}^{*} \mathrm{Fb}}<1.00$ | $\begin{aligned} & S=1.06 \\ & \mathrm{Fb}=0.660 * \mathrm{Fy} \end{aligned}$ | $\begin{gathered} \mathrm{M}=1.50 \\ \mathrm{~S}^{\star} \mathrm{Fb}=2.05 \end{gathered}$ | 0.73 |
| Deflection | $\frac{\text { defl. }}{\text { L / } 240}<1.00$ |  | $\begin{aligned} & \text { defl }= \\ & 0.51412 \end{aligned}$ | 0.89 |
| Combined Stresses (Local) (H1-2) (H2-1) | $\begin{array}{r} \frac{f a}{\begin{array}{l} 0.6 \mathrm{Fy} \\ (\mathrm{Ft}) \end{array}}+\frac{\mathrm{fbx}}{\mathrm{Fbx}}+\frac{\mathrm{fby}}{\mathrm{Fby}} \\ <1.00 \end{array}$ | fbx $=$ 0.00 <br> $F b x=$ 0.00 <br> fby $=$ 16.94 <br> Fby $=$ 23.10 | $\begin{aligned} \mathrm{P} & =0.09 \\ \mathrm{~A} & =1.70 \\ \mathrm{Fu} & =60.00 \\ \mathrm{fb} & =\mathrm{M} / \mathrm{S} \end{aligned}$ | 0.74 |
| Axial Force (E2-1/2) | $\frac{\mathrm{fa}}{\mathrm{Fa}}<1.00$ |  | $\begin{aligned} & \mathrm{P}=0.09 \\ & \mathrm{Ag}=1.70 \\ & \mathrm{Fa}=10.92 \end{aligned}$ | 0.00 |
| Combined Stresses (tension) (H2-1) | $\frac{\mathrm{fa}}{\mathrm{Ft}}+\frac{\mathrm{fbx}}{\mathrm{Fbx}}+\frac{\mathrm{fby}}{\mathrm{Fby}}$ | $\begin{aligned} & \text { Fbx }=23.10 \\ & F b y=23.10 \end{aligned}$ | $\begin{aligned} & \mathrm{fbx}=0.00 \\ & \mathrm{fby}=16.94 \end{aligned}$ | 0.73 |

