

**... Fire Protection by Computer Design**

HIGH TECH FIRE PROTECTION  
84 HACKETT MILLS ROAD  
P.O. BOX 156  
POLAND, ME 04274  
207-998-2551

Job Name : Press Hotel 4th floor room 401 #4A  
Drawing : FP-03  
Location : 119 Exchange Street Portland  
Remote Area : 4A  
Contract : 110713-1  
Data File : Calc #4A 4th floor Unit 401 (new h2o).WXF

---

**HYDRAULIC CALCULATIONS**  
*for*

**Project name:** Press Hotel 4th floor room 401 #4A  
**Location:** 119 Exchange Street Portland  
**Drawing no:** FP-03  
**Date:** 3/20/14

**Design**

**Remote area number:** 4A  
**Remote area location:** 4th floor Unit 401  
**Occupancy classification:** Residential / light hazard  
**Density:** .1 - Gpm/SqFt  
**Area of application:** 233 - SqFt  
**Coverage per sprinkler:** 224 - SqFt  
**Type of sprinklers calculated:** Residential Pendants  
**No. of sprinklers calculated:** 4  
**In-rack demand:** n/a - GPM  
**Hose streams:** 100 - GPM  
**Total water required (including hose streams):** 193 - GPM @ 71 - Psi  
**Type of system:** Wet NFPA 13  
**Volume of dry or preaction system:** n/a - Gal

**Water supply information**

**Date:** 5-12-2014  
**Location:** Corner of Exchange Street and Federal St.  
**Source:** Portland Water District

**Name of contractor:** High Tech Fire Protection  
**Address:** 84 Hackett Mills Road Poland / P.O. Box 154 Minot, ME / Pola  
**Phone number:** 207-998-2551  
**Name of designer:** Ed Poulin  
**Authority having jurisdiction:** State of Maine / City of Portland  
**Notes: (Include peaking information or gridded systems here.)**

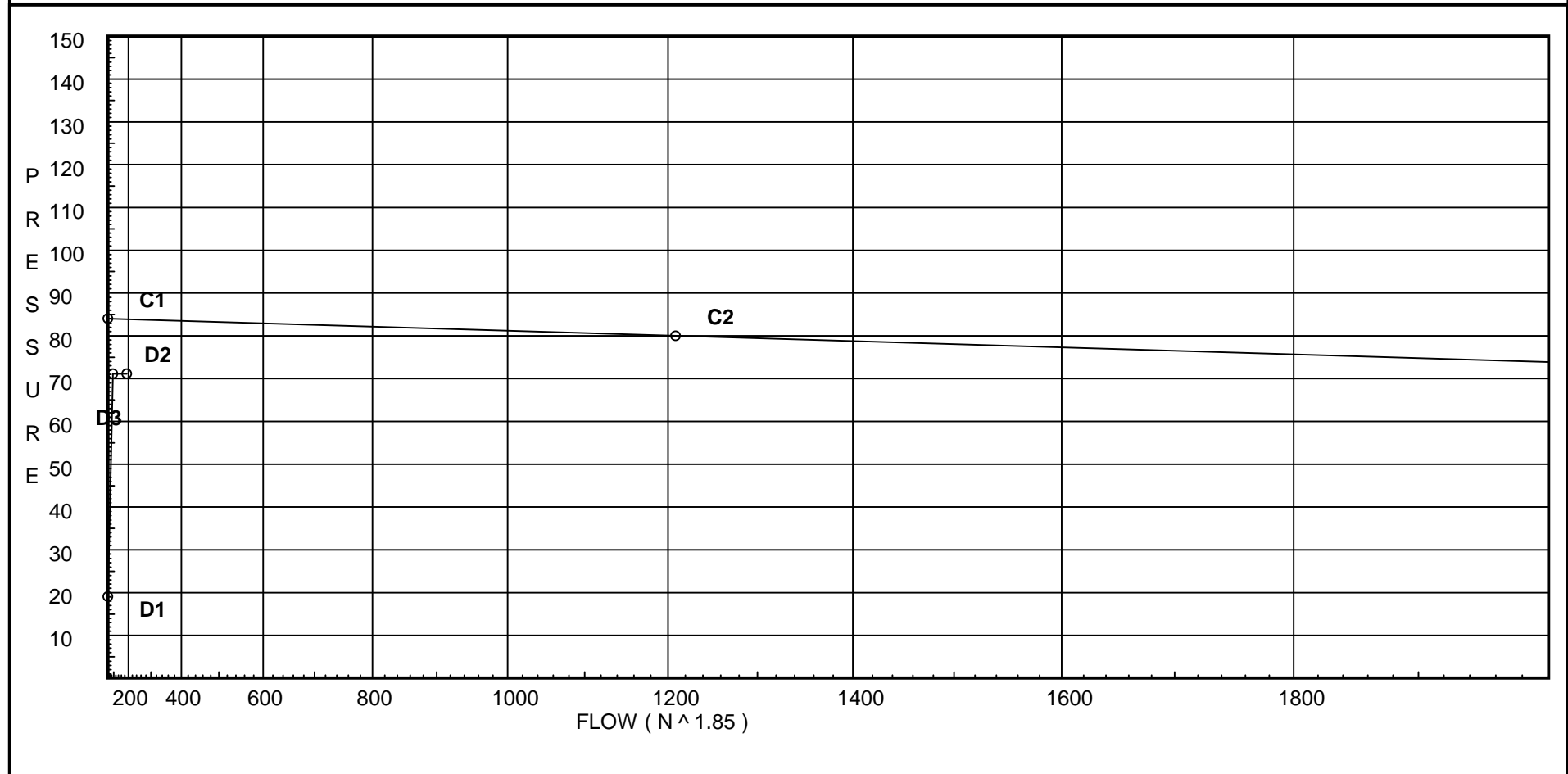
# Water Supply Curve (C)

HIGH TECH FIRE PROTECTION  
Press Hotel 4th floor room 401 #4A

Page 2  
Date 3/20/14

City Water Supply:  
C1 - Static Pressure : 84  
C2 - Residual Pressure: 80  
C2 - Residual Flow : 1209

Demand:  
D1 - Elevation : 19.056  
D2 - System Flow : 92.302  
D2 - System Pressure : 71.119  
Hose ( Demand ) : 100  
D3 - System Demand : 192.302  
Safety Margin : 12.748



# Fittings Used Summary

HIGH TECH FIRE PROTECTION  
Press Hotel 4th floor room 401 #4A

Page 3  
Date 3/20/14

## Fitting Legend

| Abbrev. | Name                       | 1/2  | 3/4 | 1 | 1 1/4 | 1 1/2 | 2   | 2 1/2 | 3  | 3 1/2 | 4   | 5   | 6  | 8  | 10 | 12 | 14 | 16 | 18 | 20  | 24  |
|---------|----------------------------|--|-----|---|-------|-------|-----|-------|----|-------|-----|-----|----|----|----|----|----|----|----|-----|-----|
| B       | NFPA 13 Butterfly Valve    | 0  | 0   | 0 | 0     | 0     | 6   | 7     | 10 | 0     | 12  | 9   | 10 | 12 | 19 | 21 | 0  | 0  | 0  | 0   | 0   |
| E       | NFPA 13 90' Standard Elbow | 1  | 2   | 2 | 3     | 4     | 5   | 6     | 7  | 8     | 10  | 12  | 14 | 18 | 22 | 27 | 35 | 40 | 45 | 50  | 61  |
| F       | NFPA 13 45' Elbow          | 1  | 1   | 1 | 1     | 2     | 2   | 3     | 3  | 3     | 4   | 5   | 7  | 9  | 11 | 13 | 17 | 19 | 21 | 24  | 28  |
| Fsp     | Flow Switch Potter VSR     | Fitting generates a Fixed Loss Based on Flow |     |   |       |       |     |       |    |       |     |     |    |    |    |    |    |    |    |     |     |
| G       | NFPA 13 Gate Valve         | 0  | 0   | 0 | 0     | 1     | 1   | 1     | 1  | 1     | 2   | 2   | 3  | 4  | 5  | 6  | 7  | 8  | 10 | 11  | 13  |
| N *     | CPVC 90'EI Harvel-Spears   |  | 7   | 7 | 8     | 9     | 11  | 12    | 13 | 0     | 0   | 0   | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0   |
| O *     | CPVC Tee - Branch          | 3  | 3   | 5 | 6     | 8     | 10  | 12    | 15 | 0     | 0   | 0   | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0   |
| S       | NFPA 13 Swing Check        | 0  | 0   | 5 | 7     | 9     | 11  | 14    | 16 | 19    | 22  | 27  | 32 | 45 | 55 | 65 |    |    |    |     |     |
| T       | NFPA 13 90' Flow thru Tee  | 3  | 4   | 5 | 6     | 8     | 10  | 12    | 15 | 17    | 20  | 25  | 30 | 35 | 50 | 60 | 71 | 81 | 91 | 101 | 121 |
| V       | 90' EI Firelock #001       | 0  | 0   | 0 | 0     | 0     | 3.5 | 4.3   | 5  | 0     | 6.8 | 8.5 | 10 | 13 | 0  | 0  | 0  | 0  | 0  | 0   | 0   |
| X       | 90'Tee-BranchFirelock002   | 0  | 0   | 0 | 0     | 0     | 8.5 | 10.8  | 13 | 0     | 16  | 21  | 25 | 33 | 0  | 0  | 0  | 0  | 0  | 0   | 0   |
| Zia     | Wilkins 350                | Fitting generates a Fixed Loss Based on Flow |     |   |       |       |     |       |    |       |     |     |    |    |    |    |    |    |    |     |     |

## Units Summary

|                |                        |
|----------------|------------------------|
| Diameter Units | Inches                 |
| Length Units   | Feet                   |
| Flow Units     | US Gallons per Minute  |
| Pressure Units | Pounds per Square Inch |

Note: Fitting Legend provides equivalent pipe lengths for fittings types of various diameters. Equivalent lengths shown are standard for actual diameters of Sched 40 pipe and CFactors of 120 except as noted with \*. The fittings marked with a \* show equivalent lengths values supplied by manufacturers based on specific pipe diameters and CFactors and they require no adjustment. All values for fittings not marked with a \* will be adjusted in the calculation for CFactors of other than 120 and diameters other than Sched 40 per NFPA.

# Pressure / Flow Summary - STANDARD

HIGH TECH FIRE PROTECTION  
 Press Hotel 4th floor room 401 #4A

Page 4  
 Date 3/20/14

| Node No. | Elevation | K-Fact       | Pt Actual | Pn | Flow Actual | Density | Area | Press Req. |
|----------|-----------|--------------|-----------|----|-------------|---------|------|------------|
| DP1      | -1.0      | 5.8          | 14.92     | na | 22.4        | 0.1     | 224  | 7.6        |
| 400      | 47.0      | K = K @ EQ01 | 17.06     | na | 23.9        |         |      |            |
| 401      | 47.0      | 5.8          | 16.54     | na | 23.59       | 0.1     | 224  | 13.2       |
| 402      | 47.0      |              | 17.11     | na |             |         |      |            |
| 403      | 47.0      | 5.8          | 14.92     | na | 22.4        | 0.1     | 224  | 13.2       |
| 404      | 47.0      | K = K @ EQ01 | 15.01     | na | 22.42       |         |      |            |
| 405      | 47.0      |              | 17.73     | na |             |         |      |            |
| 406      | 47.0      |              | 21.66     | na |             |         |      |            |
| 407      | 47.0      |              | 22.78     | na |             |         |      |            |
| 408      | 47.0      |              | 29.09     | na |             |         |      |            |
| 409      | 47.0      |              | 31.18     | na |             |         |      |            |
| 410      | 47.0      |              | 36.71     | na |             |         |      |            |
| SR4      | 47.0      |              | 42.38     | na |             |         |      |            |
| SR1      | 14.0      |              | 56.92     | na |             |         |      |            |
| SR11     | 14.0      |              | 57.06     | na |             |         |      |            |
| SR0      | 0.0       |              | 63.17     | na |             |         |      |            |
| SR01     | 0.0       |              | 63.53     | na |             |         |      |            |
| SR02     | 0.0       |              | 64.53     | na |             |         |      |            |
| SR03     | 0.0       |              | 64.59     | na |             |         |      |            |
| TOR      | -4.0      |              | 66.61     | na |             |         |      |            |
| BOR      | -6.0      |              | 70.49     | na |             |         |      |            |
| BASE     | -6.0      |              | 74.84     | na |             |         |      |            |
| HS1      | -4.0      |              | 74.0      | na |             |         |      |            |
| HS2      | -4.0      |              | 74.02     | na |             |         |      |            |
| HS3      | -4.0      |              | 74.1      | na | 100.0       |         |      |            |
| TEST     | 3.0       |              | 71.12     | na |             |         |      |            |

The maximum velocity is 19.4 and it occurs in the pipe between nodes 405 and 406

# Final Calculations - Hazen-Williams

HIGH TECH FIRE PROTECTION  
Press Hotel 4th floor room 401 #4A

Page 5  
Date 3/20/14

| Hyd.<br>Ref.<br>Point | Qa<br><br>Qt       | Dia.<br>"C"<br>Pf/Ft     | Fitting<br>or<br>Eqv.        | Ln.                                       | Pipe<br>Ftng's<br>Total     | Pt<br>Pe<br>Pf            | Pt<br>Pv<br>Pn | ***** | Notes                                   | ***** |
|-----------------------|--------------------|--------------------------|------------------------------|---|-----------------------------|---------------------------|----------------|-------|---|-------|
| DP1<br>to<br>EQ01     | 22.40<br><br>22.4  | 1.101<br>150.0<br>0.0838 | 1O                           | 5.0<br>0.0<br>0.0                         | 1.000<br>5.000<br>6.000     | 14.916<br>-0.433<br>0.503 |                |       | K Factor = 5.80<br><br>Vel = 7.55       |       |
|                       | 0.0<br>22.40       |                          |                              |   |                             |                           | 14.986         |       | K Factor = 5.79                         |       |
| 400<br>to<br>402      | 23.90<br><br>23.9  | 1.101<br>150.0<br>0.0950 |                              | 0.0<br>0.0<br>0.0                         | 0.600<br>0.0<br>0.600       | 17.056<br>0.0<br>0.057    |                |       | K Factor @ node EQ01<br><br>Vel = 8.05  |       |
|                       | 0.0<br>23.90       |                          |                              |   |                             |                           | 17.113         |       | K Factor = 5.78                         |       |
| 401<br>to<br>402      | 23.59<br><br>23.59 | 1.101<br>150.0<br>0.0924 | 1O                           | 5.0<br>0.0<br>0.0                         | 1.200<br>5.000<br>6.200     | 16.540<br>0.0<br>0.573    |                |       | K Factor = 5.80<br><br>Vel = 7.95       |       |
| 402<br>to<br>405      | 23.90<br><br>47.49 | 1.394<br>150.0<br>0.1067 |                              | 0.0<br>0.0<br>0.0                         | 5.800<br>0.0<br>5.800       | 17.113<br>0.0<br>0.619    |                |       | <br><br>Vel = 9.98                      |       |
|                       | 0.0<br>47.49       |                          |                              |   |                             |                           | 17.732         |       | K Factor = 11.28                        |       |
| 403<br>to<br>404      | 22.40<br><br>22.4  | 1.101<br>150.0<br>0.0836 |                              | 0.0<br>0.0<br>0.0                         | 1.100<br>0.0<br>1.100       | 14.916<br>0.0<br>0.092    |                |       | K Factor = 5.80<br><br>Vel = 7.55       |       |
| 404<br>to<br>405      | 22.42<br><br>44.82 | 1.101<br>150.0<br>0.3027 | 1O                           | 5.0<br>0.0<br>0.0                         | 4.000<br>5.000<br>9.000     | 15.008<br>0.0<br>2.724    |                |       | K Factor @ node EQ01<br><br>Vel = 15.10 |       |
| 405<br>to<br>406      | 47.48<br><br>92.3  | 1.394<br>150.0<br>0.3651 | 1N                           | 8.0<br>0.0<br>0.0                         | 2.750<br>8.000<br>10.750    | 17.732<br>0.0<br>3.925    |                |       | <br><br>Vel = 19.40                     |       |
| 406<br>to<br>407      | 0.0<br><br>92.3    | 2.003<br>150.0<br>0.0625 |                              | 0.0<br>0.0<br>0.0                         | 18.000<br>0.0<br>18.000     | 21.657<br>0.0<br>1.125    |                |       | <br><br>Vel = 9.40                      |       |
| 407<br>to<br>408      | 0.0<br><br>92.3    | 2.003<br>150.0<br>0.0625 | 1N<br>1O                     | 11.0<br>10.0<br>0.0                       | 80.000<br>21.000<br>101.000 | 22.782<br>0.0<br>6.312    |                |       | <br><br>Vel = 9.40                      |       |
| 408<br>to<br>409      | 0.0<br><br>92.3    | 2.067<br>120.0<br>0.0810 |                              | 0.0<br>0.0<br>0.0                         | 1.000<br>0.0<br>1.000       | 29.094<br>2.000<br>0.081  |                |       | * Fixed loss = 2<br>Vel = 8.82          |       |
| 409<br>to<br>410      | 0.0<br><br>92.3    | 2.003<br>150.0<br>0.0625 | 2N                           | 22.0<br>0.0<br>0.0                        | 66.500<br>22.000<br>88.500  | 31.175<br>0.0<br>5.531    |                |       | <br><br>Vel = 9.40                      |       |
| 410<br>to<br>SR4      | 0.0<br><br>92.3    | 2.157<br>120.0<br>0.0658 | 1B<br>1Fsp<br>1S<br>1X<br>1V | 7.384<br>0.0<br>13.537<br>10.461<br>4.307 | 5.000<br>35.689<br>40.689   | 36.706<br>3.000<br>2.678  |                |       | * Fixed loss = 3<br>Vel = 8.10          |       |
| SR4<br>to<br>SR1      | 0.0<br><br>92.3    | 4.26<br>120.0<br>0.0024  | 7V                           | 62.675<br>0.0<br>0.0                      | 40.000<br>62.675<br>102.675 | 42.384<br>14.292<br>0.246 |                |       | <br><br>Vel = 2.08                      |       |
| SR1<br>to<br>SR11     | 0.0<br><br>92.3    | 4.26<br>120.0<br>0.0024  | 3V                           | 26.861<br>0.0<br>0.0                      | 32.000<br>26.861<br>58.861  | 56.922<br>0.0<br>0.141    |                |       | <br><br>Vel = 2.08                      |       |

# Final Calculations - Hazen-Williams

HIGH TECH FIRE PROTECTION  
 Press Hotel 4th floor room 401 #4A

Page 6  
 Date 3/20/14

| Hyd.<br>Ref.<br>Point | Qa<br>Qt       | Dia.<br>"C"<br>Pf/Ft    | Fitting<br>or<br>Eqv. Ln.                        | Pipe<br>Ftng's<br>Total      | Pt<br>Pe<br>Pf            | Pt<br>Pv<br>Pn | *****                              | Notes | ***** |
|-----------------------|----------------|-------------------------|--|------------------------------|---------------------------|----------------|------------------------------------|-------|-------|
| SR11<br>to<br>SR0     | 0.0<br>92.3    | 4.26<br>120.0<br>0.0024 | 1V<br>8.954<br>0.0<br>0.0                        | 10.000<br>8.954<br>18.954    | 57.063<br>6.063<br>0.046  |                | Vel = 2.08                         |       |       |
| SR0<br>to<br>SR01     | 0.0<br>92.3    | 4.26<br>120.0<br>0.0024 | 3V<br>26.861<br>1B 15.8<br>1X 21.067<br>1F 5.267 | 81.500<br>68.995<br>150.495  | 63.172<br>0.0<br>0.360    |                | Vel = 2.08                         |       |       |
| SR01<br>to<br>SR02    | 0.0<br>92.3    | 4.26<br>120.0<br>0.0030 | 0.0<br>0.0<br>0.0                                | 1.000<br>0.0<br>1.000        | 63.532<br>1.000<br>0.003  |                | * Fixed loss = 1<br>Vel = 2.08     |       |       |
| SR02<br>to<br>SR03    | 0.0<br>92.3    | 4.26<br>120.0<br>0.0024 | 1X 21.067<br>0.0<br>0.0                          | 2.000<br>21.067<br>23.067    | 64.535<br>0.0<br>0.055    |                | Vel = 2.08                         |       |       |
| SR03<br>to<br>TOR     | 0.0<br>92.3    | 4.26<br>120.0<br>0.0024 | 2V 17.907<br>1X 21.067<br>0.0                    | 81.000<br>38.974<br>119.974  | 64.590<br>1.732<br>0.288  |                | Vel = 2.08                         |       |       |
| TOR<br>to<br>BOR      | 0.0<br>92.3    | 4.26<br>120.0<br>0.0022 | 1Fsp 0.0<br>0.0<br>0.0                           | 4.000<br>0.0<br>4.000        | 66.610<br>3.866<br>0.009  |                | * Fixed loss = 3<br>Vel = 2.08     |       |       |
| BOR<br>to<br>BASE     | 0.0<br>92.3    | 4.26<br>120.0<br>0.0020 | 1Zia 0.0<br>0.0<br>0.0                           | 1.000<br>0.0<br>1.000        | 70.485<br>4.348<br>0.002  |                | * Fixed loss = 4.348<br>Vel = 2.08 |       |       |
| BASE<br>to<br>HS1     | 0.0<br>92.3    | 6.14<br>100.0<br>0.0006 | 1G 2.273<br>1E 10.608<br>1T 22.732               | 25.000<br>35.613<br>60.613   | 74.835<br>-0.866<br>0.035 |                | Vel = 1.00                         |       |       |
| HS1<br>to<br>HS2      | 0.0<br>92.3    | 8.23<br>100.0<br>0.0001 | 1T 29.011<br>0.0<br>0.0                          | 90.000<br>29.010<br>119.010  | 74.004<br>0.0<br>0.016    |                | Vel = 0.56                         |       |       |
| HS2<br>to<br>HS3      | 0.0<br>92.3    | 6.14<br>100.0<br>0.0006 | 1T 22.732<br>0.0<br>0.0                          | 120.000<br>22.732<br>142.732 | 74.020<br>0.0<br>0.080    |                | Vel = 1.00                         |       |       |
| HS3<br>to<br>TEST     | 100.0<br>192.3 | 6.14<br>100.0<br>0.0022 | 1G 2.273<br>1E 10.608<br>0.0                     | 10.000<br>12.881<br>22.881   | 74.100<br>-3.032<br>0.051 |                | Qa = 100<br>Vel = 2.08             |       |       |
|                       | 0.0<br>192.30  |                         |  |                              | 71.119                    |                | K Factor = 22.80                   |       |       |