

. . . Fire Protection by Computer Design

Eastern Fire Protection
170 Kitty Hawk Ave.
P.O. Box 1390
Auburn, Maine, 04211
207-784-1507

Job Name : MAINE EYE CENTER SECOND FLOOR PROOF CALCULATION
Drawing : 2 OF 2
Location : 161 MARGINAL WAY, PORTLAND, MAINE
Remote Area : TWO
Contract : 5501-16
Data File : MAINE EYE SECOND FLOOR PROOF SUBMITTAL .W XF

HYDRAULIC CALCULATIONS
for

Project name: MAINE EYE CENTER SECOND FLOOR PROOF CALCULATION
Location: 161 MARGINAL WAY, PORTLAND, MAINE
Drawing no: 2 OF 2
Date: 7/26/16

Design

Remote area number: TWO
Remote area location: SECOND FLOOR
Occupancy classification: LIGHT
Density: .10 - Gpm/SqFt
Area of application: 1112 - SqFt
Coverage per sprinkler: 148 - SqFt
Type of sprinklers calculated: 1/2" K=5.6 RELIABE F1FR CHROME PENDENT
No. of sprinklers calculated: 12
In-rack demand: - GPM
Hose streams: 100 - GPM
Total water required (including hose streams): 351.25 - GPM @ 102.87 - Psi
Type of system: WET
Volume of dry or preaction system: - Gal

Water supply information

Date: 5/31/2016
Location: HYDRANT LOCATED ON MARGINAL WAY
Source: PORTLAND WATER DISTRICT

Name of contractor: Eastern Fire Protection
Address: 170 Kitty Hawk Ave. / P.O. Box 1390 / Auburn, Maine, 04211
Phone number: 207-784-1507
Name of designer: WAF
Authority having jurisdiction: STATE FIRE MARSHAL, PORTLAND FIRE DEPARTMENT
Notes: (Include peaking information or gridded systems here.)
NOTE: REMOTE AREA MODIFIED PER NFPA 13 SECTION 11.2.3.2.3.1

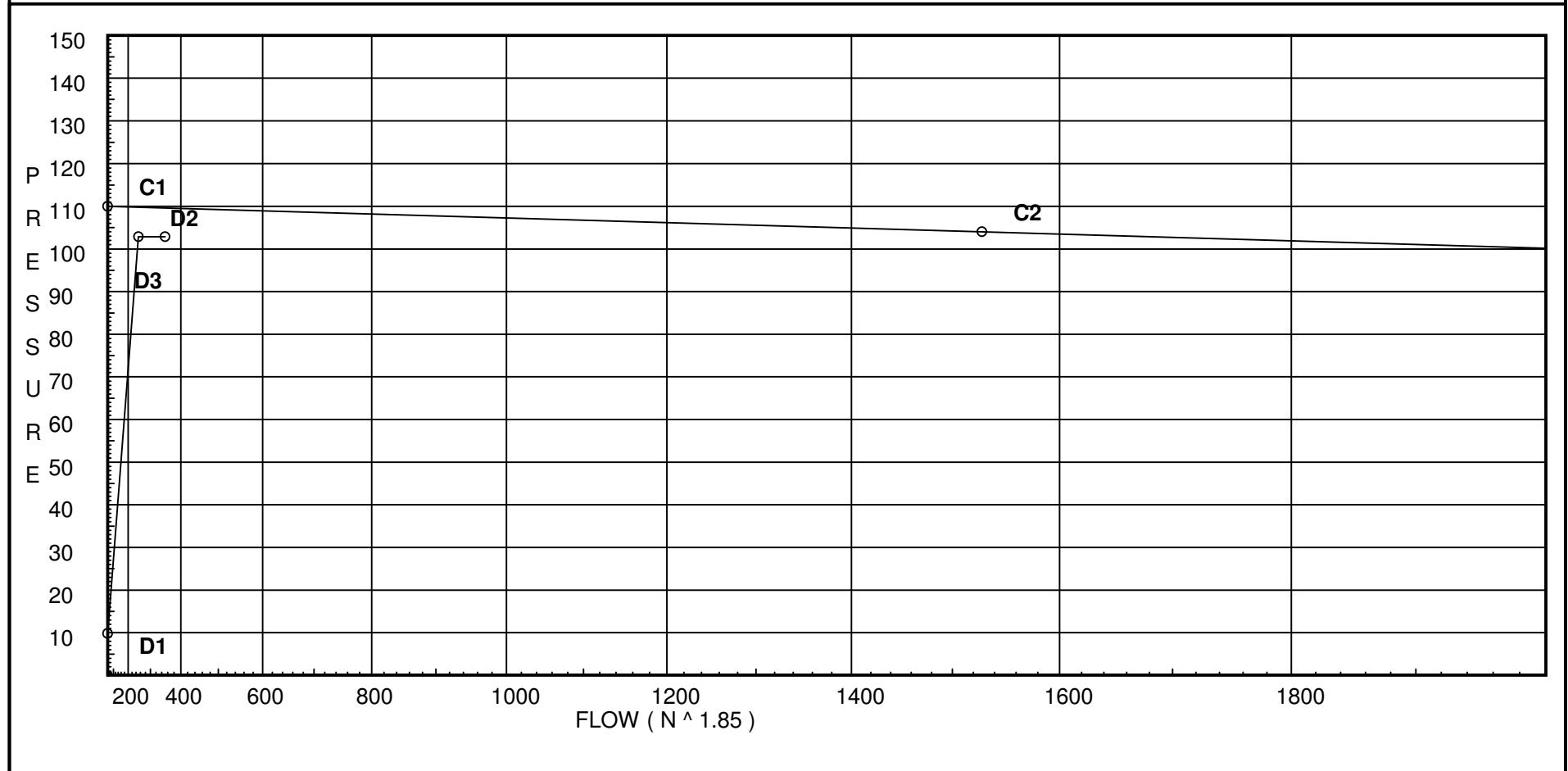
Water Supply Curve C

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City Water Supply:
C1 - Static Pressure : 110
C2 - Residual Pressure: 104
C2 - Residual Flow : 1528

Demand:
D1 - Elevation : 9.818
D2 - System Flow : 251.253
D2 - System Pressure : 102.874
Hose (Demand) : 100
D3 - System Demand : 351.253
Safety Margin : 6.731



Fittings Used Summary

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Fitting Legend		1/2	3/4	1	1 1/4	1 1/2	2	2 1/2	3	3 1/2	4	5	6	8	10	12	14	16	18	20	24
Abbrev.	Name																				
B	NFPA 13 Butterfly Valve	0	0	0	0	0	6	7	10	0	12	9	10	12	19	21	0	0	0	0	0
E	NFPA 13 90° Standard Elbow	1	2	2	3	4	5	6	7	8	10	12	14	18	22	27	35	40	45	50	61
G	NFPA 13 Gate Valve	0	0	0	0	0	1	1	1	1	2	2	3	4	5	6	7	8	10	11	13
I	90° Grvd-Vic Elbow #10	0	0	2	3	4	3.5	6	5	8	7	8.5	10	13	17	20	23	25	33	36	40
J	90° Tee-Branch Grv Vic #20	0	0	4.5	6	8	8.5	10.8	13	17	16	21	25	33	41	50	65	78	88	98	120
L	NFPA 13 Long Turn Elbow	0.5	1	2	2	2	3	4	5	5	6	8	9	13	16	18	24	27	30	34	40
S	NFPA 13 Swing Check	0	0	5	7	9	11	14	16	19	22	27	32	45	55	65					
T	NFPA 13 90° Flow thru Tee	3	4	5	6	8	10	12	15	17	20	25	30	35	50	60	71	81	91	101	121
Zcb	Colt C200 Vert Butt	Fitting generates a Fixed Loss Based on Flow																			

Units Summary

Diameter Units Inches
 Length Units Feet
 Flow Units US Gallons per Minute
 Pressure Units Pounds per Square Inch

Note: Fitting Legend provides equivalent pipe lengths for fittings types of various diameters. Equivalent lengths shown are standard for actual diameters of Sched 40 pipe and CFactors of 120 except as noted with *. The fittings marked with a * show equivalent lengths values supplied by manufacturers based on specific pipe diameters and CFactors and they require no adjustment. All values for fittings not marked with a * will be adjusted in the calculation for CFactors of other than 120 and diameters other than Sched 40 per NFPA.

SUPPLY ANALYSIS

Node at Source	Static Pressure	Residual Pressure	Flow	Available Pressure	Total Demand	Required Pressure
TEST	110.0	104	1528.0	109.605	351.25	102.874

NODE ANALYSIS

Node Tag	Elevation	Node Type	Pressure at Node	Discharge at Node	Notes
D1	0.0	5.6	7.0	14.82	
200	122.67	4.06	13.35	14.82	K=K @ L1
201	122.67	4.06	13.98	15.16	K=K @ L1
202	122.67	4.06	16.82	16.63	K=K @ L1
203	122.67	4.06	24.14	19.92	K=K @ L1
205	122.67	4.06	28.94	21.81	K=K @ L1
204	122.67	4.06	31.03	22.59	K=K @ L1
207	122.67	4.06	17.95	17.18	K=K @ L1
208	122.67	4.06	18.78	17.57	K=K @ L1
209	122.67	4.06	23.12	19.5	K=K @ L1
210	122.67	4.06	33.01	23.3	K=K @ L1
211	122.67		40.46		
213	122.67	4.06	58.04	30.89	K=K @ L1
214	122.67	4.06	61.78	31.87	K=K @ L1
215	122.67		63.01		
212	122.67		58.07		
216	122.67		64.74		
217	122.67		68.19		
114	109.0		79.01		
A	109.0		81.23		
TOR	109.0		83.62		
B1	109.0		93.69		
BASE	101.0		102.14		
TEST	100.0		102.87	100.0	

Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqv.	Ln.	Pipe Ftng's Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
D1 to L1	0 0	5.60	14.82	1	E T	2.0 5.0 0.0	78.000 7.000 85.000	120	7.000 0.0 6.350			Vel = 5.50
L1			0.0 14.82						13.350		K Factor = 4.06	
200 to 201	122.670 122.670	4.06	14.82	1		0.0 0.0 0.0	8.460 0.0 8.460	120	13.350 0.0 0.632		K = K @ L1	Vel = 5.50
201 to 202	122.670 122.670	4.06	15.16	1		0.0 0.0 0.0	10.330 0.0 10.330	120	13.982 0.0 2.842		K = K @ L1	Vel = 11.13
202 to 203	122.670 122.670	4.06	16.63	1	2E	4.0 0.0 0.0	7.750 4.000 11.750	120	16.824 0.0 7.316		K = K @ L1	Vel = 17.30
203 to 205	122.670 122.670	4.06	19.93	1.25	T	6.0 0.0 0.0	9.170 6.000 15.170	120	24.140 0.0 4.798		K = K @ L1	Vel = 14.27
205 to 204	122.670 122.670	4.06	21.81	1.25		0.0 0.0 0.0	3.920 0.0 3.920	120	28.938 0.0 2.095		K = K @ L1	Vel = 18.95
204 to 211	122.670 122.670	4.06	22.59	1.25	T	6.0 0.0 0.0	5.580 6.000 11.580	120	31.033 0.0 9.431		K = K @ L1	Vel = 23.80
211			0.0 110.94						40.464		K Factor = 17.44	
207 to 208	122.670 122.670	4.06	17.18	1		0.0 0.0 0.0	8.460 0.0 8.460	120	17.948 0.0 0.831		K = K @ L1	Vel = 6.38
208 to 209	122.670 122.670	4.06	17.57	1		0.0 0.0 0.0	12.000 0.0 12.000	120	18.779 0.0 4.339		K = K @ L1	Vel = 12.90
209 to 210	122.670 122.670	4.06	19.50	1		0.0 0.0 0.0	12.000 0.0 12.000	120	23.118 0.0 9.892		K = K @ L1	Vel = 20.14
210 to 211	122.670 122.670	4.06	23.30	1.25	2T	12.0 0.0 0.0	5.750 12.000 17.750	120	33.010 0.0 7.454		K = K @ L1	Vel = 16.63
211 to 212	122.670 122.670		110.94	2	E 2T	6.153 24.613 0.0	40.610 30.766 71.376	120	40.464 0.0 17.604			Vel = 16.55
212			0.0 188.49						58.068		K Factor = 24.74	
213 to 214	122.670 122.670	4.06	30.89	1	T	5.0 0.0 0.0	7.870 5.000 12.870	120	58.038 0.0 3.744		K = K @ L1	Vel = 11.47

Final Calculations - Hazen-Williams

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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqv.	Ln.	Pipe Ftng's Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
214 to 215	122.670 122.670	4.06	31.88 62.77	2 2.067	T	10.0 0.0	20.960 10.000	120	61.782 0.0	K = K @ L1		
215 to 216	122.670 122.670		0.0 62.77	2 2.067	T	10.0 0.0	33.580 10.000	120	63.011 0.0	Vel = 6.00		
216			0.0 62.77						64.741	K Factor = 7.80		
212 to 216	122.670 122.670		188.49	2.5	I T	8.237 16.474	47.000 24.711	120	58.068 0.0			
216 to 217	122.670 122.670		188.49 62.76	2.635 2.5	T	0.0 16.474	71.711 5.330	0.0931	6.673	Vel = 11.09		
217 to 114	122.670 109		251.25	2.635		0.0	21.804	0.1584	3.453	Vel = 14.78		
217 to 114	122.670 109		0.0	3	3I 2J	20.159 34.943	32.000 55.102	120	68.194 5.920			
114 to A	109 109		251.25	3.26		0.0	87.102	0.0562	4.893	Vel = 9.66		
114 to A	109 109		0.0	3	2I	13.44 0.0	26.170 13.440	120	79.007 0.0			
A to TOR	109 109		251.25	3.26		0.0	39.610	0.0562	2.225	Vel = 9.66		
A to TOR	109 109		0.0	3	2I J	13.44 17.471	11.580 30.911	120	81.232 0.0			
TOR to B1	109 109		251.25	3.26		0.0	42.491	0.0562	2.386	Vel = 9.66		
TOR to B1	109 109		0.0	3	B 6I	13.44 40.319	104.120 75.262	120	83.618 0.0			
B1 to BASE	109 101		251.25	3.26	S	21.503	179.382	0.0562	10.076	Vel = 9.66		
B1 to BASE	109 101		0.0	4	I Zcb	9.217 0.0	8.000 9.217	120	93.694 8.179	* * Fixed Loss = 4.714		
BASE to TEST	101 100		251.25	4.26		0.0	17.217	0.0153	0.263	Vel = 5.66		
BASE to TEST	101 100		0.0	6	L G	12.911 4.304	100.000 60.252	140	102.136 0.433			
TEST			251.25	6.16	T	43.037	160.252	0.0019	0.305	Vel = 2.70		
TEST			100.00 351.25						102.874	Qa = 100.00 K Factor = 34.63		