

# **Geotechnical Report**

### New Condominium Building 118 Congress Street Portland, Maine

Prepared for:

TLA, Inc. 118 Congress St Portland, Maine

Prepared by:

Summit Geoengineering Services 640 Main Street Lewiston, Maine

> Project #13193 December 2013



December 13, 2013 SGS #13193

118 Congress Street LLC c/o TLA, Inc. 118 Congress St Portland, Maine Attn: Ed Theriault

Reference: Geotechnical Engineering Investigation, Proposed Condominium Building

118 Congress St., Portland, Maine

Dear Ed:

We have completed the geotechnical investigation for the construction of a new condominium building on Congress Street in Portland, Maine. Our scope of services included performing six test borings at the site and preparing this report summarizing our findings and geotechnical recommendations.

Our scope of services for this project did not include an environmental site assessment or further investigation for the presence or absence of hazardous or toxic material on, below, or around the site. No hazardous materials were encountered in the test borings completed at the site.

### 1.0 Project Description

The project consists of the construction of a new 4 story apartment building. The first or ground floor level will consist of a fully enclosed parking lot and two retail areas. The upper levels will consist of living units. The ground floor will be at or near the existing ground surface. An elevator pit, anticipated to extend to a depth of 5 feet (including the foundation) is planned for the middle of the building adjacent to Congress Street.

### 2.0 Explorations and Laboratory Testing

Summit Geoengineering Services (SGS) drilled a total of six borings at the site on December 3, 2013. The boring explorations were located by Summit by taping from existing site features. The boring locations were cleared from underground utilities by Dig Smart of Maine under contract to SGS. The borings using completed using 2½-inch hollow stem augers. Borings were drilled to refusal, ranging from 4.2 to 17.5 feet. Standard penetration tests (SPT) with split

spoon samples were obtained at 5-foot intervals. The location of the borings is shown on the Test Boring Location Plan in Appendix A. Logs of the explorations are included in Appendix B.

A sample of the existing fill soil from B-2 at a depth of 5 feet was tested for grain size analysis in accordance with ASTM D422. A laboratory test report is included in Appendix C.

### 3.0 Subsurface Conditions

The soil at the site generally consists of the following materials and thicknesses.

- Pavement, 4 to 4-1/2 inches
- Fill, 4.5 to 9 feet
- Glacial Till, 8 to 9.5 feet
- Bedrock

The fill soil, encountered at all the boring locations, varies from brown to dark brown silty sand to brown gravelly sand to dark brown sandy silt. The fill did not contain organics or other unsuitable materials. SPT-N values in the fill ranged from 6 to 36 blows per foot (bpf) and averaged 8 bpf in the upper 2 feet. The SPT-N values in the fill at a depth of 5 feet ranged from 22 to 37 bpf and averaged 29 bpf. A SPT-N value = 4 bpf was encountered at a depth of 5 feet at the B-3 location. We believe that this fill is loosely placed soil used to backfill the excavation after removal of an underground tank. No petroleum odors were encountered in the fill soil.

The fill at a depth of 5 feet at the B-2 location, based on the grain size test, consisted of about 31% gravel, 64% sand, and 5% fines (primarily silt). This soil will be usable for the new construction at the site.

The glacial till soil is described as olive-brown sandy silt with a little gravel and trace of clay. SPT-N values in the till ranged from 40 to 73 and averaged 61 bpf. The glacial till soil was not encountered at the B-1, B-5 and B-6 boring locations where refusal was encountered at depths of 4.2, 7.7, and 6.5 feet, respectively.

Refusal, presumed to be bedrock, was encountered at the following depths

	DEPTH TO BEDROCK									
Boring Depth Below Existing Ground Surface (										
B-2	17.5									
B-3	17.5									
B-4	13.4									
B-5	7.7									
B-6	6.5									

Refusal at B-1 at a depth of 4.2 feet is likely on an underground obstruction, probably rubble from previous demolitions at the property.

Samples of the bedrock were not taken. Based on maps published by the Maine Geological Survey, the bedrock is part of the Spring Point Formation consisting of greenish-gray biotite-quartz schist and amphibolite.

Groundwater was not observed in the borings due to the sidewalls collapsing. Measurements taken in the drilling augers indicate that groundwater is not present at the site. This is consistent with the findings in the August 1998 Phase 2 ESA report prepared by EER.

### **4.0 Foundation Design Recommendations**

### A. Allowable Bearing Pressure

With proper site preparation, the proposed building can be supported using a conventional spread footing foundations. We recommend that the footings for the proposed building be designed using an allowable bearing pressure of 3,000 psf. Column locations and loads were not available for this report. Assuming typical loading conditions for this type of building, total settlement for this allowable bearing pressure is estimated to be less than 3/4 inch. Assuming proper subgrade preparation, differential settlement will be negligible. This bearing pressure and associated settlement are based on the following conditions:

- All pavement is removed from the building footprint prior to constructing the foundations.
- The exposed soil within the building footprint beneath the removed pavement is proofrolled by making a minimum of 6 passes in each of two perpendicular directions using a vibratory roller with a minimum operating weight of 10 tons. Proofrolling should be performed prior to excavating for the footings. The intent of proofrolling is to densify areas of looser existing fill (e.g., B-3) and thereby provide a more uniform subgrade density and bearing resistance.
- After excavation, footing trenches are proofrolled by making a minimum of 4 passes using a large walk-behind vibratory compactor.
- Rubble encountered at the base of the footing excavations, if encountered, is removed and replaced with Structural Fill or ¾ inch crushed stone.

### B. Frost Protection

Based on the required frost protection depth, exterior footings should be constructed at a minimum depth of 4 feet below the exterior finished grade. This frost protection depth is based on a design air-freezing index of 1,250-degree days for the Portland area.

We recommend that the exterior of the foundation walls be backfilled with soil meeting the following gradation specification:

FOUNDATION BACKFILL								
Sieve Size	Percent finer							
3 inch	100							
½ inch	60 to 100							
No. 40	0 to 50							
No. 200	0 to 7							

Reference: MeDOT Specification 703.06, Type F

The maximum particle size should be limited to 6 inches. The Foundation Backfill should be compacted to a minimum of 95 percent of its maximum dry density, determined in accordance with ASTM D1557. Based on the grain size analysis, the fill in the area of B-2 will meet this gradation specification.

### C. Groundwater Control

Groundwater was not observed in the borings and perimeter underdrains are not strictly necessary at this site. In order to account for potential changes in local and regional hydrogeology and infiltration of regionally generated surface water runoff it may be desired to install exterior perimeter underdrains. If used, perimeter underdrains should consist of 4 inch rigid perforated PVC placed adjacent to the exterior footings and surrounded by a minimum of 6 inches of crushed stone wrapped in filter fabric to prevent clogging from the migration of the fine soil particles in the foundation backfill soils. The underdrain pipe should be outlet to a location where it will be free flowing.

### D. Seismic Design

The subgrade profile at the site is categorized as Site Class C, "Very Dense Soil and Soft Rock" in accordance with the 2009 International Building Code (IBC). The following seismic site coefficients should be used:

2009 IBC SEISMIC COEFFICIE	ENTS
Seismic Coefficient	Site Class C
Short period spectral response (S <sub>S</sub> )	0.314
1 second spectral response (S <sub>1</sub> )	0.077
Site coefficient (F <sub>a</sub> )	1.2
Site Coefficient (F <sub>v</sub> )	1.7
Design short period spectral response (S <sub>DS</sub> )	0.251
Design 1 second spectral response (S <sub>D1</sub> )	0.087

Soils susceptible to liquefaction were not encountered in the borings.

#### E. Slabs on Grade – Heated Areas

We recommend the slabs-on-grade in heated areas be constructed on a minimum 12-inch thick layer of Structural Fill (SF) or ¾ inch crushed stone.

STRUCTURAL FILL (SF)								
Sieve Size	Percent finer							
3 inch	100							
1/4 inch	25 to 70							
No. 40	0 to 30							
No. 200	0 to 7							

**Reference**: MDOT 703.06, Type D

The maximum particle size should be limited to 6 inches. We recommend that the existing subgrade soil beneath the SF be proofrolled as described in Section 4.0A. The SF can be placed in a single 12-inch lift, assuming that it can be compacted to 95 percent of its maximum dry density determined in accordance with ASTM D1557.

The slabs can be designed using a subgrade modulus value of 175 pci for the above subgrade conditions.

#### F. Slabs-on-Grade – Unheated Areas

We recommend that slabs on grade in unheated areas be placed on a minimum of 30 inches of SF in order to provide frost heave protection. Concrete for exterior slabs should be air-entrained and have a minimum 28 cay compressive strength of 4,000 psi. We recommend that concrete slabs at entrances be constructed on a frost wall foundation. This construction method will exclude potential slab movements from interfering with doors.

### **5.0** Pavement Section Design

The mean annual freezing index for the Portland area is approximately 900 degree F days. The mean annual frost penetration depth for this freezing index and the soil at the site is approximately 30 inches. The subgrade soil in the ground floor parking area is anticipated to consist of the existing proofrolled fill soil.

Based on the subgrade soil conditions and the anticipated traffic (cars and light trucks traveling at low speeds) we recommend a minimum total pavement section thickness of approximately 60% of the mean annual frost penetration depth, or 18 inches. We further recommend that the pavement section consist of the following materials.

PAVEMENT SECTION MATERIAL THICKNESSES								
Material	Specification							
Asphalt Surface Course	3/4	MeDOT 703.09 Grading D MeDOT Superpave 9.5 mm						
Asphalt Binder Course	2-1/4	MeDOT Superpave 19 mm						
Base Soil	3	MeDOT 703.06 Type A						
Subbase Soil	12	MeDOT 703.06 Type D						

The material specifications are referenced to the 1995 Maine Department of Transportation Standard Specifications for Highways and Bridges.

We recommend that the subgrade soil in pavement areas be proofrolled as described in Section 4A above. Subbase and Base soil can each be placed in a single lift. These soils should be compacted to a minimum of 95 percent of their maximum dry density, determined in accordance with ASTM D1557, Modified Proctor Density.

Groundwater is not an issue for pavement areas at this site and pavement underdrains are not necessary.

### **6.0** Construction Considerations

The composition of the existing fill is primarily mineral. The fill at the B-2 location and possibly other locations will be suitable for reuse at the site. We recommend that soil which appears to clean and granular be stockpiled at the site and reused as appropriate, based on laboratory grain size tests performed on samples from the stockpile.

We recommend that the pavement be removed in its entirety from beneath the building footprint. The subgrade soil within the building footprint should be proofrolled by making a minimum of 5 passes in each of two perpendicular directions using a vibratory roller with a minimum operating weight of 10 tons. Proofrolling should be performed prior to excavating for the footings. This procedure is important to provide a uniform dense subgrade soil at this site, considering the presence of the loose fill soil at the B-3 location and possibly other locations not explored.

The existing fill soil is classified as OSHA Type C. Temporary Slopes in the existing fill soil should be sloped no steeper than 1.5H:1V.

### 7.0 Closure

Our recommendations are based on professional judgment and generally accepted principles of geotechnical engineering. Some changes in subsurface conditions from those presented in this report may occur. Should these conditions differ materially from those described in this report, Summit should be notified so that we can re-evaluate our recommendations.

Finished grades and foundation loads were not available for this report. We recommend that SGS be given an opportunity to review the grading and foundation plans to confirm that the assumptions used to generate the recommendations in this report are valid.

We appreciate the opportunity to provide geotechnical engineering services on this phase of the project. If there are any questions please do not hesitate to contact me.

Sincerely,

**Summit Geoengineering Services, Inc.** 

William M. Peterlein, P.E.

William Mater

Principal Geotechnical Engineer



# APPENDIX A TEST BORING LOCATION PLAN

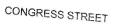
### LEGEND

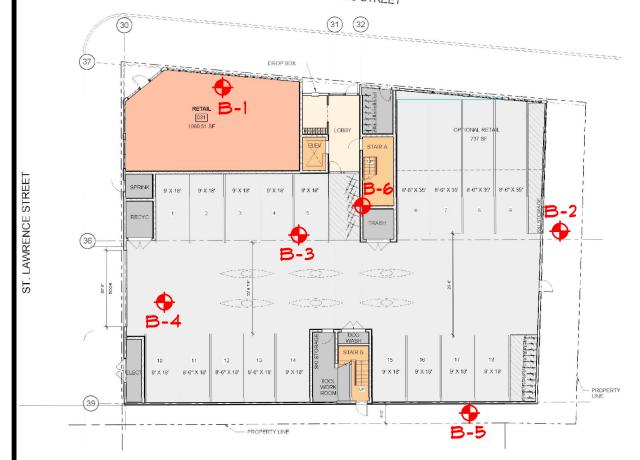
♣ B-1

SUMMIT TEST BORING (DECEMBER 3, 2013)

### PLAN REFERENCE

"118 CONDOMINIUMS, PARKING LEVEL", DATED NOVEMBER 1, 2013, PREPARED BY ARCHETYPE ARCHITECTS





# TEST BORING LOCATION PLAN 118 CONGRESS STREET

PORTLAND, MAINE PREPARED FOR TLA, INC.

DATE: DEC. 4, 2013 DRAWN BY: KRF CHECKED BY: WMP

JOB: 13193 SCALE: 1" = 25' FILE: 13193 BOR

145 LISBON ST. - SUITE 601 LEWISTON, ME 04240 Tel.: (207) 576-3313 2002 ATLANTIC HIGHWAY CAMDEN, ME 04843 Tel.: (201) 106-1999



# APPENDIX B BORINGS LOGS

### **EXPLORATION REPORT COVER SHEET**

The exploration report has been prepared by the geotechnical engineer from both field and laboratory data. Differences between field logs and exploration reports may exist.

It is common practice in the soil and foundation engineering profession that field logs and laboratory data sheets not be included in engineering reports, because they do no represent the engineer's final opinion as to appropriate descriptions for conditions encountered in the exploration and testing work. The field logs will be retained in our office for review. Results of laboratory tests are generally shown on the borings logs or are described in the text of the report as appropriate.

### **Drilling and Sampling Symbols:**

SS = Split Spoon Hyd = Hydraulic advance of probes

ST = Shelby Tube - 2" OD, disturbed WOH = Weight of Hammer UT = Shelby Tube - 3" OD, undisturbed WOR = Weight of Rod HSA = Hollow Stem Auger GS = Grain Size Data

CS = Casing size as noted PI = Plasticity Index

CS = Casing - size as noted PI = Plasticity Index Sv = Vane Shear LL = Liquid Limit

PP = Pocket Penetrometer w = Natural Water Content

RX = Rock Core – size as noted USCS = unified Soil Classification System

### Water Level Measurements:

Water levels indicated on the boring logs are the levels measured in the boring at the times indicated. In pervious soils, the indicated elevations are considered reliable groundwater levels. In impervious soils, the accurate determination of groundwater elevations may not be possible, even after several days of observations; additional evidence of groundwater elevations via observation or monitoring wells must be sought.

### Gradation Description and Terminology:

Less than 5% Boulders: Over 8 inches Trace: 8 inches to 3 inches 5% to 15% Cobbles: Little: 3 inches to No.4 sieve 15% to 25% Gravel: Some: Sand: No.4 to No. 200 sieve Silty, Sandy, etc.: Greater than 25%

Silt: No. 200 sieve to 0.005 mm

Clay: less than 0.005 mm

#### Density of Granular Soils and Consistency of Cohesive Soils:

CONSISTENCY OF CO	OHESIVE SOILS	DENSITY OF GRANULAR SOILS				
SPT N-value blows/ft	Consistency	SPT N-value blows/ft	<b>Relative Density</b>			
0 to 2	Very Soft	0 to 3	Very Loose			
3 to 4	Soft	4 to 9	Loose			
5 to 8	Firm	10 to 29	Compact			
9 to 16	Stiff	30 to 49	Dense			
17 to 32	Very Stiff	50 to 80	Very Dense			
>32	Hard					

						S	OIL BORI	NG LOG	Boring #:	B-1			
		CALLA	AALT			Project:	Residential Bui		Project #:	13193			
		SUM	IVITA			Project: Location:	118 Congress		Project #: Sheet:	13193 1 of 1			
		GEOENGINEERI				City, State:	Portland, Main		Chkd by:	1 0. 1			
Drilling (	Co:	Summit Geoen	ngineering Ser	rvices		Boring Elevation:							
Drilling ( Driller:		C. Coolidge, P.				Reference:							
Summit	Staff:	B. Peterlein, P.				Date started:	12/3/2013	Date Completed:	12/3/2013				
DF	RILLING I	METHOD		AMPLER				ESTIMATED GROUND V					
Vehicle:	Tracked	d ver Probe	Length:	24" SS	15	Date	Depth	Elevation		ference			
	2-1/2		Diameter: Hammer:	2"OD/1.5" 140 lb	עו	12/3/2013			None observed - bor	enoie ary			
Hammer	Style: A	Auto	Method:	ASTM D15	86								
Depth	T						SAMPL	E	Geological/	Geological			
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	Ī	DESCRIP	TION	Test Data	Stratum			
						4" Pavement							
1_	S-1	24/20	0.5 to 2.5	4		Brown to dark br		), trace Gravel,		FILL			
2				3		damp, loose, SM							
۷_	+			5		1							
3				<del>                                     </del>		†							
-						<u> </u>							
4_						]							
_				<u> </u>		5		5.6					
5_	+			-		End of E	Boring at 4.2 tee	et - Auger Refusal					
6				+		†							
-				<u> </u>		<u>Note</u> : Ref	usal probably o	n bedrock - possible					
7_						]	boulder or i	rubble					
						1							
8_	+			-		1							
9	-			+		†							
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10						1							
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22						]							
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Granul	ar Soils	Cohesiv	o Soils	% Compo	osition	NOTES:	DD - Docket Don	etrometer, MC = Moisture C	ontont	Soil Moisture Condition			
	Density	Blows/ft.	Consistency	ASTM D		NOTES.		;, PI = Plastic Index	ontent	Dry: S = 0%			
0-4	V. Loose		V. soft	7.51111 5.	2107	Bedrock Joints	EE - Eiquia Eiriii	, II – Flastic Macx		Humid: $S = 1 \text{ to } 25\%$			
5-10	Loose	2-4	Soft	< 5% T	race	Shallow = 0 to 35	degrees			Damp: S = 26 to 50%			
11-30	Compact		Firm	5-15% l		Dipping = 35 to 55	-			Moist: S = 51 to 75%			
31-50	Dense	9-15	Stiff	15-30%		Steep = 55 to 90 d	legrees			Wet: S = 76 to 99%			
>50	V. Dense	16-30 >30	V. Stiff Hard	> 30% '	vvith	Boulders = diameter	er > 12 inches C	obbles = diameter < 12 inch	nes and > 3 inches	Saturated: S = 100%			
		/30	riaru					$I = \langle No 4 \text{ and } \rangle No 200$ , Sil					

		$\wedge$	<u> </u>			9	OIL BORI	NG LOG	Boring #:	B-2
		CILL	TAALT			Project:	Residential Bui	Project #:	13193	
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		GEOENGINEER	ING SERVICES			City, State:	Chkd by:			
Drilling C	co:	Summit Geoer	naineerina Se	rvices		Boring Elevation	Portland, Main :			
Driller:		C. Coolidge, P				Reference:	-			
Summit	Staff:	B. Peterlein, P				Date started:	12/3/2013	Date Completed:	12/3/2013	
		METHOD	S	AMPLER				ESTIMATED GROUNI	D WATER DEPTH	
	ehicle: Tracked Length: 24" SS					Date	Depth	Elevation		ference
	odel: AMS Power Probe Diameter: 2"OD/1.5"ID ethod: 2-1/2" H.S.A. Hammer: 140 lb				ID	12/3/2013			Borehole caved at 1	0 ft - dry
Method: Hammer			Hammer: Method:	140 lb ASTM D15	0.4					
Depth	Style.	Auto	wethou.	ASTIVIDIO	100		SAMPI	F	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>		DESCRIP		Test Data	Stratum
<u> </u>	S-1	24/8	0 to 2	5		Dark brown Grav		e Silt, trace organics,		
1				4		loose, moist, SM	-	, ,		
1				2						FILL
2_				2						
3_	-					1				
4						_				
,						†				
5						_				
_	S-2	24/20	5 to 7	7		Brown Gravelly S	SAND, trace Silt	, dense, moist, SP	31.3% Gravel	
6_				11					63.7% Sand	
_				26					5% Fines	
7_	-	1	1	15		Cobbles and Bou	Idors at 7 ft			
8						Hard drilling	liders at 7 ft			
_						riara ariiirig				
9						1				
_										
10										GLACIAL TILL
	S-3	24/24	10 to 12	17		Olive-brown slig				
11_				22		Gravel and Clay,	very stiff, mois	t, ML		
12				20		_				
12 _				20		1				
13						_				
_										
14_										
15_	C 4	24/24	15 45 17	20		_				
16	S-4	24/24	15 to 17	20 48		Olive-gray SILT	little Sand trac	ce Gravel and Clay,		
10_				25		hard, damp, ML		o Graver and Glay,		
17				19						
- I						<u> </u>				
18						End of	Boring at 17.5	ft - Auger Refusal		BEDROCK
						1				
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21						Ī				
22 _						1				
				1		1				
Cro	r Call-	C-L	ro Soils	0/ 0	ocition	NOTES:	DD = Dook=+ D · ·	otromotor MC M-:-'	Contont	Soil Moisture Caraditi
Granula Blows/ft.		Cohesiv Blows/ft.	Consistency	% Comp		NOTES:		etrometer, MC = Moisture t, PI = Plastic Index	e Content	Soil Moisture Condition  Dry: S = 0%
0-4	V. Loose		V. soft	AS IIVI D	Z40/	Bedrock Joints	LL – LIQUIU LIMII	, i i – ridstic maex		Humid: S = 1 to 25%
5-10	Loose	2-4	Soft	< 5% 7	race	Shallow = 0 to 35	degrees			Damp: S = 26 to 50%
11-30	Compact		Firm	5-15%		Dipping = 35 to 55	-			Moist: S = 51 to 75%
31-50	Dense	9-15	Stiff	15-30%	Some	Steep = 55 to 90 c	degrees			Wet: S = 76 to 99%
>50	V. Dense		V. Stiff	> 30%	With					Saturated: S = 100%
		>30	Hard					obbles = diameter < 12 in		
						Gravel = < 3 inch	and > No 4, Sand	$d = \langle No 4 \text{ and } \rangle No 200,$	Silt/Clay = < No 200	

									Daring #.	D 2
	SUMMIT						OIL BORII		Boring #:	B-3
		SUM	MIN			Project:	Residential Bui	Project #:	13193	
		GEOENGINEERI				Location:	118 Congress S	Sheet:	1 of 1	
Daillia a C	) -	C				City, State:	Portland, Maine	2	Chkd by:	
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Summit S	Staff.	B. Peterlein, P.				Date started:	12/3/2013	Date Completed:	12/3/2013	
		METHOD		AMPLER		Date Starteu.	12/3/2013	ESTIMATED GROUND		
Vehicle:			Length:	24" SS		Date	Depth	Elevation		eference
	Model: AMS Power Probe Diameter: 2"OD/1.5"ID					12/3/2013	Ворин	Lievation	Borehole caved at 3	
Method:		" H.S.A.	Hammer:	140 lb	· <u> </u>					
Hammer			Method:	ASTM D15	86					
Depth							SAMPL	.E	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	DESCRIPTION			Test Data	Stratum
						4-1/2" Pavement				
1_										
	S-1	12/12	1 to 2	7		Brown SAND, litt	le Gravel and S	ilt, compact, dry, SM		FILL
2_	ļ			6		1				
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3_	<b> </b>			ļ		1				
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) -	S-2	24/18	5 to 7	1		Olive-brown SII	Emixed with Cr	avel Sand and Clay,		
6	J-Z	27/10	3107	2		loose, damp, ML		avoi Jana ana Glay,		
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4.4	S-3	24/24	10 to 12	16				little Gravel, trace		GLACIAL TILL
11_				24 36		Clay, hard, mois	, IVIL			
12				49		†				
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	S-4	24/24	15 to 17	30		Cobble at 15 to				
16_				40		†	•	ravel, trace Clay,		
	<u> </u>			40		dense, damp, MI	-			
17_	<b> </b>			43		1				
10						End of F	Poring at 17 F ft	- Auguer Refusal		BEDROCK
18_						Elia ol E	outing at 17.5 H	- Auguer Kerusar		DEDKOCK
19						†				
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Granula		Cohesiv		% Compo		NOTES:		etrometer, MC = Moisture	e Content	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	ASTM D	2487	Dadasala Istoto	LL = Liquid Limit	, PI = Plastic Index		Dry: S = 0%
0-4 5-10	V. Loose	<2	V. soft	, E0/ T	race	Bedrock Joints	dograce			Humid: S = 1 to 25%
5-10 11-30	Loose	2-4 5-8	Soft	< 5% T 5-15%		Shallow = 0 to 35 Dipping = 35 to 55	-			Damp: S = 26 to 50% Moist: S = 51 to 75%
11-30	Compact Dense	5-8 9-15	Firm Stiff	15-30%		Steep = 55 to 90 d	· ·			Wet: S = 76 to 99%
31.50		7-10	JIII	13-30 /6	JUITE	21cch - 22 10 40 0	cyrees			Wei. 3 - 70 to 99%
31-50 >50		16-30	V Stiff	> 30%	With					Saturated: S = 100%
	V. Dense	16-30 >30	V. Stiff Hard	> 30%	With	Boulders = diamete	er > 12 inches. Co	obbles = diameter < 12 ir	nches and > 3 inches	Saturated: S = 100%

		$\wedge$				9	OIL BORII	NG LOG	Boring #:	B-4
		CALA	AALT			Project:	Residential Bui	Project #:	13193	
		SUM	IVIN			Location:	118 Congress S		Sheet:	13193 1 of 1
		GEOENGINEERI	NG SERVICES			City, State:	Portland, Main	Chkd by:	1011	
Drilling C	,u.	Summit Geoer	naineerina Sei	vices		Boring Elevation:			orina by.	
Driller:	,	C. Coolidge, P.		VICC3		Reference:	•			
Summit S	Staff:	B. Peterlein, P.				Date started:	12/3/2013	Date Completed:	12/3/2013	
DR	RILLING	METHOD	S	AMPLER				ESTIMATED GROUNI	) WATER DEPTH	
	/ehicle: Tracked Length: 24" SS					Date	Depth	Elevation		eference
		ver Probe	Diameter:	2"OD/1.5"	ID	12/3/2013			Borehole caved at !	5.4 ft - dry
Method:			Hammer:	140 lb	0/					
Hammer Depth	Style: I	Auto	Method:	ASTM D15	80		SAMPL	E	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	+	DESCRIP		Test Data	Stratum
()	S-1	12/8	0 to 1	12	00	2" Pavement	2200		. oot Bata	on aran
1		.270	0 10 1	24		4	dy SILT, little G	ravel, hard, dry, ML		FILL
_										
2_						1				
_						1				
3_	<u> </u>			1		1				
4						†				
+-	<u> </u>			1		†				
5						†				
_	S-2	24/24	5 to 7	19				ravel, hard, dry, ML		
6_				24				tle Gravel, trace Clay,		
_				16		hard, humid, ML				CLACIAL TUI
7_	-			20		+				GLACIAL TILL
8						Cobble at 7 to 8	ft			
Ŭ <u>-</u>						1002210 41 7 10 0				
9						Dense at 9 ft				
_						T			1	
10_										
11	S-3	24/24	10 to 12	13		Olive gray Sandy		vel, trace Clay,		
11_				29 41		hard, humid, ML				
12				30		†				
-						†				
13						]				
14_						End of	Boring at 13.4 f	t - Auger Refusal		BEDROCK
15						+				
13_						†				
16						†				
_						]				
17_						1				
4.0						1				
18_	-			1		+				
19						†				
.,_						†				
20_						]				
						1				
21_						1				
22						4				
22 _	<del>                                     </del>			<del> </del>		†				
				1		†				
Granula	ar Soils	Cohesiv	e Soils	% Comp	osition	NOTES:	PP = Pocket Pen	etrometer, MC = Moisture	e Content	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	ASTM D		]		, PI = Plastic Index		Dry: S = 0%
0-4	V. Loose	<2	V. soft			Bedrock Joints				Humid: S = 1 to 25%
5-10	Loose	2-4	Soft	< 5% T		Shallow = 0 to 35	-			Damp: S = 26 to 50%
11-30	Compact	5-8	Firm	5-15%		Dipping = 35 to 55	-			Moist: S = 51 to 75%
31-50	Dense	9-15	Stiff	15-30%		Steep = 55 to 90 d	iegrees			Wet: S = 76 to 99%
	V Da									
	V. Dense	16-30 >30	V. Stiff Hard	> 30%	vvitn	Boulders = diameter	er > 10 inches C	obbles = diameter < 12 ii	nches and > 3 inches	Saturated: S = 100%

		<u> </u>				S	OIL BORII	NG LOG	Boring #:	B-5
		CLINA	AALT				Residential Bui		Project #:	13193
		SUM	IVITY				118 Congress S	3	Sheet:	1 of 1
		GEOENGINEERI	NG SERVICES				Portland, Main		Chkd by:	
Drilling (	()	Summit Geoen	naineering Ser	rvices		Boring Elevation:			···· ,	
Driller:		C. Coolidge, P.		V100C		Reference:	·			
Summit		B. Peterlein, P.				Date started:	12/3/2013	Date Completed:	12/3/2013	
DF	RILLING	METHOD	S/	AMPLER		<u></u> _		ESTIMATED GROUND V	VATER DEPTH	
	Tracked		Length:	24" SS		Date	Depth	Elevation	Re	ference
		ver Probe	Diameter:	2"OD/1.5"I	ID	12/3/2013			None observed in bo	rehole
Method:		" H.S.A.	Hammer:	140 lb		<u> </u>				
	Style: A	Auto	Method:	ASTM D15	86	<u> </u>	CANADI		Contaminal/	O I - min n l
Depth	No.	Dec /Dea (in)	D :th. (ft)	1.1	NI NI	4	SAMPL		Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	D. I. Ironovous Cilko	DESCRIPT		Test Data	Stratum
1	S-1	24/18	0 to 2	2	<del></del>	<del></del>	SAND, trace G	ravel, loose, humid		
1_	ļ		<del> </del>	3	<del></del>	SM				FILL
2			<del>                                     </del>	1		†				I ILL
				<del>'</del>		†				
3						†				
-					Í	†				
4						]				
					<u> </u>	]				
5_		3.404		<u> </u>	<del></del>	ļ				
,	S-2	24/24	5 to 7	6	<u> </u>	<del>-1</del>	SAND, trace to I	little Silt, dense, dry		
6_	<del>                                     </del>		<del></del>	12 16	<del></del>	SM				
7			<del></del>	25	<del></del>	+				
· -				2.5		†				
8						End of	Boring at 7.7 ff	t - Auger Refusal	+	BEDROCK
_	<u> </u>					†	J	Ü		
9						]				
						]				
10_				<u> </u>	ь					
.,			<del></del>		<del></del>	1				
11_	ļ		<del></del>	<del>                                     </del>	<del></del>	4				
12			<del></del>	+	<del></del>	+				
14_			<del></del>	+	<del></del>	+				
13				+ +		†				
-						†				
14						†				
						<u> </u>				
15			<u> </u>	<u> </u>	<u> </u>	]				
.,					<u> </u>	1				
16_	<u> </u>		<del></del>		<u> </u>	4				
17			<del></del>		<del></del>	4				
17 -			<del></del>	+	<del></del>	+				
18						†				
-						†				
19						†				
						]				
20					<u> </u>	]				
0.4			<b></b>		<del></del>	1				
21_	ļ		<del></del>	<del>                                     </del>	<del></del>	4				
22			<del></del>	+	<del></del>	4				
	+		<del> </del>	+		+				
			<b>—</b>			†				
Granula	ar Soils	Cohesiv	e Soils	% Compo	osition	NOTES:	PP = Pocket Pen	etrometer, MC = Moisture Co	ontent	Soil Moisture Condition
	Density	Blows/ft.	Consistency	ASTM D				t, PI = Plastic Index		Dry: S = 0%
0-4	V. Loose	<2	V. soft			Bedrock Joints	•			Humid: S = 1 to 25%
5-10	Loose	2-4	Soft	< 5% T	race	Shallow = 0 to 35 of	degrees			Damp: S = 26 to 50%
11-30	Compact	5-8	Firm	5-15% L		Dipping = 35 to 55	_			Moist: S = 51 to 75%
31-50	Dense	9-15	Stiff	15-30%		Steep = 55 to 90 d	legrees			Wet: S = 76 to 99%
>50	V. Dense		V. Stiff	> 30% \	With	Poulders "	or . 10 !==! · · · · · · · · · · · · · · · · ·	obbloo diamatan 40 '	soo and a 2 trade :	Saturated: S = 100%
		>30	Hard					obbles = diameter $< 12$ inch d = $< No 4$ and $>No 200$ , Silt		

		$\wedge$				S	OIL BORII	NG LOG	Boring #:	B-6
		SUM	TIM			Project:	Project #:	13193		
		GEOENGINEERI				Location:	Sheet:	1 of 1		
Daillin 1	\					City, State:	Portland, Maine	9	Chkd by:	
Drilling O Driller:		C. Coolidge, P.	3	vices		Boring Elevation Reference:	:			
Summit		B. Peterlein, P.				Date started:	12/3/2013	Date Completed:	12/3/2013	
		METHOD		AMPLER				ESTIMATED GROUND		
	/ehicle: Tracked Length: 24" SS					Date	Depth	Elevation		eference
	lodel: AMS Power ProbeDiameter:2"OD/1.5"IDlethod: 2-1/2" H.S.A.Hammer:140 lb				ID	12/3/2013			None observed in b	orehole
Method: Hammer			Hammer: Method:	ASTM D15	586	1				
Depth							SAMPL	E	Geological/	Geological
(ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	N <sub>60</sub>	<u> </u>	DESCRIPT	TION	Test Data	Stratum
	S-1	24/18	0 to 2	3		3-1/2" Pavemen				
1_	-			4		Brown Gravelly S	SAND, trace Silt,	loose, dry, SM		FILL
2	-			3 4		1				
<b>-</b>				7		1				
3_						]				
						Hard drilling at 3	to 5 ft			
4_	1			1		+				
5	<u> </u>					†				
-	S-2	10/10	5 to 5.3	11		Brown Gravelly S	SAND, trace Silt,	loose, dry, SM		
6_				50-4"		broken cobble in	spoon tip			
7				1		Fnd -f	Poring at 4 F ft	- Auger Refusal		
/_	<del>                                     </del>			1		Ena of	buring at 6.5 ft	- Auger Kerusal		
8_						1				
_						<u>Note</u> : Ref		n bedrock - possible		
9_				-		1	boulder or r	rubble		
10						+				
10_						†				
11_						1				
						1				
12_	-					+				
13	<b>-</b>					†				
.~_						1				
14_						Ţ				
45				-		1				
15_	<del>                                     </del>					†				
16						1				
						]				
17_				-		1				
18	-			1		1				
10_						1				
19						1				
						1				
20_	-			-		+				
21						†				
_						1				
22 _						1				
						+				
Granula	I ar Soils	Cohesiv	re Soils	% Comp	l osition	NOTES:	PP = Pocket Pen	etrometer, MC = Moisture	Content	Soil Moisture Condition
Blows/ft.		Blows/ft.	Consistency	ASTM D		1		, PI = Plastic Index		Dry: S = 0%
0-4	V. Loose	<2	V. soft			Bedrock Joints	•			Humid: S = 1 to 25%
5-10	Loose	2-4	Soft	< 5% 7		Shallow = 0 to 35	-			Damp: S = 26 to 50%
11-30 31-50	Compact Dense	5-8 9-15	Firm Stiff	5-15% 15-30%		Dipping = $35$ to $55$ Steep = $55$ to $90$ c	-			Moist: S = 51 to 75% Wet: S = 76 to 99%
>50	V. Dense		V. Stiff	> 30%		Sieeb = 33 t0 90 t	icgi ccs			Saturated: S = 100%
		>30	Hard		-	Boulders = diamet	er > 12 inches, Co	obbles = diameter < 12 in	ches and > 3 inches	
						Gravel = < 3 inch	and > No 4, Sand	= < No 4 and >No 200, S	Silt/Clay = < No 200	

# APPENDIX C LABORATORY TEST RESULTS



### **GRAIN SIZE ANALYSIS - ASTM D422**

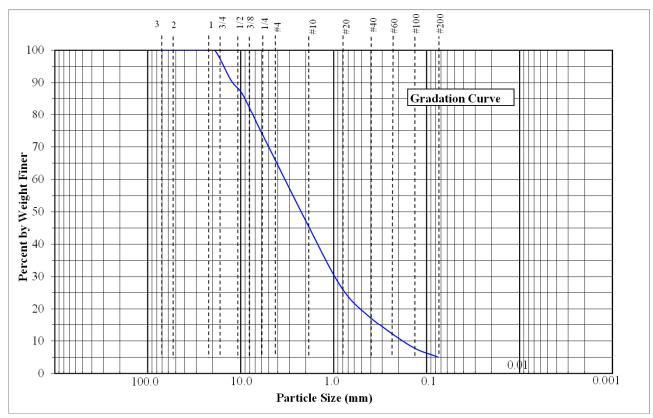
PROJECT NAME: 118 Congress Street Condos PROJECT NUMBER: 13193

CLIENT: TLA, Inc. SAMPLE NUMBER: B-2, S-2 SOURCE: B-2, 5' - 7' DESCRIPTION: Gravelly SAND, trace Silt, SW

DATE: 12/6/2013 TECHNICIAN: Erika Hawklsey, E.I.

## DATA

E SIZE mm	% BY WT FINER
(3 in)	100.0
(2 in)	100.0
(1-1/2 in)	100.0
(1 in)	100.0
(3/4 in)	100.0
(1/2 in)	90.7
(3/8 in)	86.3
(1/4 in)	75.9
(No. 4)	68.7
(No. 10)	47.3
(No. 20)	27.2
(No. 40)	17.9
(No. 100)	8.5
(No. 200)	5.0
	(3 in) (2 in) (1-1/2 in) (1 in) (3/4 in) (1/2 in) (3/8 in) (1/4 in) (No. 4) (No. 10) (No. 20) (No. 40) (No. 100)



REMARKS: Moisture Content = 5.6%