

**. . . Fire Protection by Computer Design**

Residential Fire Protection  
64 Daggett Hill Rd.  
Greene, ME 04236  
946-3473

Job Name : 162 EASTERN PROMANADE APT  
Building : 3rd floor level  
Location : 162 Easter Promanade Portland, Maine  
System : 1 of 1  
Contract : C18006  
Data File : 162 EASTERN PROMENADE APT-3RD LEVEL LOFT.WXF

HYDRAULIC DESIGN INFORMATION SHEET

Name - 162 Eastern Prom Apartments Date - 3-2-18  
Location - 162 Easter Promanade Portland, Maine  
Building - 3rd floor level System No. - 1 of 1  
Contractor - Crandall Toothaker Contract No. - C18006  
Calculated By - TPP Drawing No. - 1 of 1  
Construction: (X) Combustible ( ) Non-Combustible Ceiling Height Varies  
OCCUPANCY - Residential

S Type of Calculation: ( )NFPA 13 Residential (X)NFPA 13R ( )NFPA 13D  
Y Number of Sprinklers Flowing: ( )1 ( )2 (X)4 ( )  
S ( )Other  
T ( )Specific Ruling Made by Date  
E  
M Listed Flow at Start Point - 13 Gpm System Type  
Listed Pres. at Start Point - 7 Psi (X) Wet ( ) Dry  
D MAXIMUM LISTED SPACING 16 x 16 ( ) Deluge ( ) PreAction  
E Domestic Flow Added - Gpm Sprinkler or Nozzle  
S Additional Flow Added - Gpm Make VIKING Model VK494  
I Elevation at Highest Outlet - 47.5 Feet Size 7/16 K-Factor 4.9  
G Note:SAFETY MARGIN: 12.30 PSI Temperature Rating 155  
N

Calculation Gpm Required 58.702 Psi Required 44.684 At Test  
Summary C-Factor Used: Overhead 150 Underground 150

W Water Flow Test: Pump Data: Tank or Reservoir:  
A Date of Test - 5-25-17 Rated Cap. Cap.  
T Time of Test - @ Psi Elev.  
E Static (Psi) - 57 Elev.  
R Residual (Psi) - 54 Other Well  
Flow (Gpm) - 1198 Proof Flow Gpm  
S Elevation - 28

P Location: MUNJOY STREET AT MOODY STREET

L Source of Information: PORTLAND WATER DISTRICT  
Y

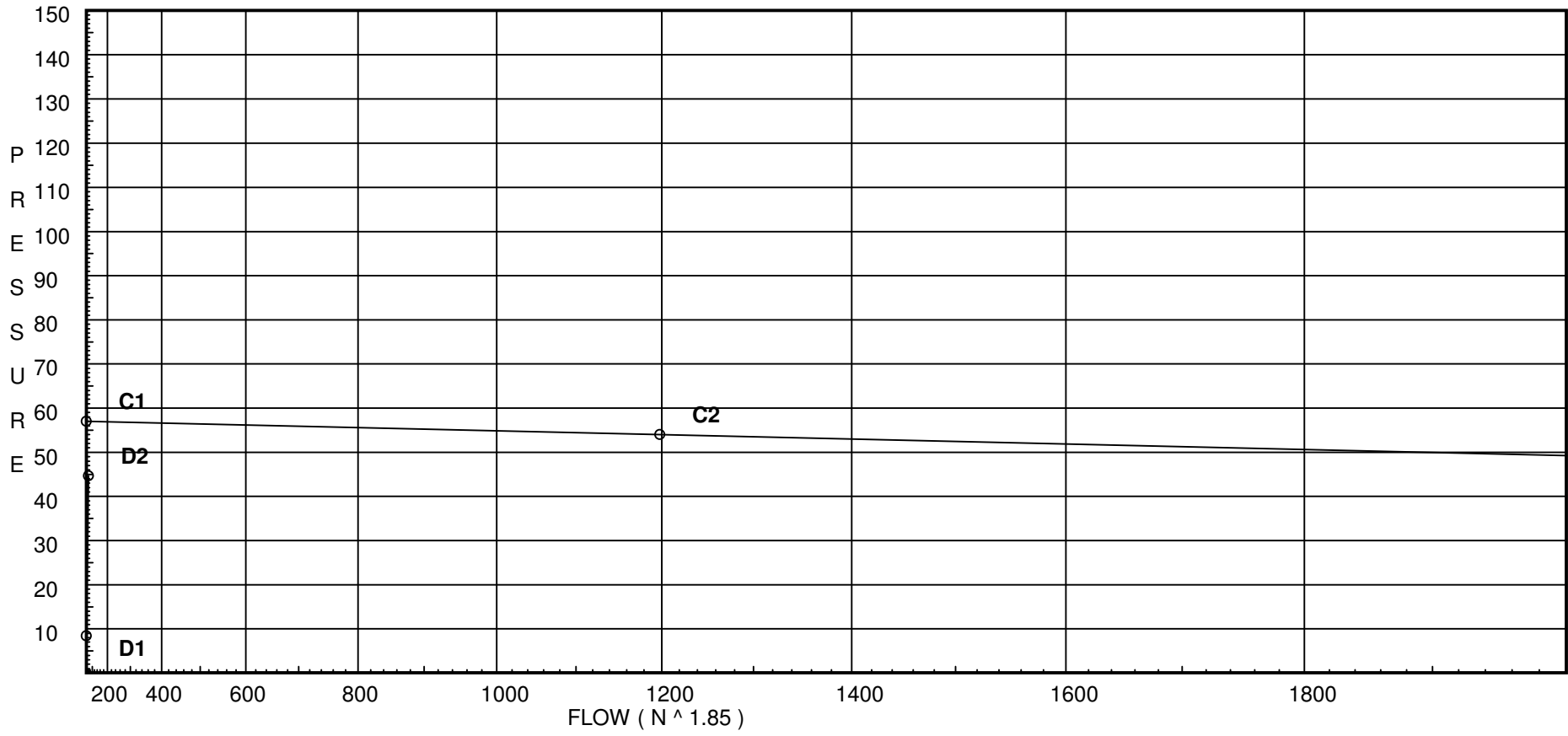
# Water Supply Curve (C)

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City Water Supply:  
C1 - Static Pressure : 57  
C2 - Residual Pressure: 54  
C2 - Residual Flow : 1198

Demand:  
D1 - Elevation : 8.445  
D2 - System Flow : 58.7024  
D2 - System Pressure : 44.684  
Hose ( Adj City ) : \_\_\_\_\_  
Hose ( Demand ) : \_\_\_\_\_  
D3 - System Demand : 58.7024  
Safety Margin : 12.305



# Fittings Used Summary

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## Fitting Legend

| Abbrev. | Name                      | 1/2 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2  | 2 1/2 | 3  | 3 1/2 | 4  | 5  | 6  | 8  | 10 | 12 | 14 | 16 | 18 | 20  | 24  |
|---------|---------------------------|-----|-----|---|-------|-------|----|-------|----|-------|----|----|----|----|----|----|----|----|----|-----|-----|
| E       | 90' Standard Elbow        | 2   | 2   | 2 | 3     | 4     | 5  | 6     | 7  | 8     | 10 | 12 | 14 | 18 | 22 | 27 | 35 | 40 | 45 | 50  | 61  |
| G       | Generic Gate Valve        | 0   | 0   | 0 | 0     | 0     | 1  | 1     | 1  | 1     | 2  | 2  | 3  | 4  | 5  | 6  | 7  | 8  | 10 | 11  | 13  |
| N       | CPVC 90'ElI Harvel-Spears | 7   | 7   | 7 | 8     | 9     | 11 | 12    | 13 | 0     | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0   |
| O       | CPVC Tee - Branch         | 3   | 3   | 5 | 6     | 8     | 10 | 12    | 15 | 0     | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0   |
| R       | CPVC Coupling Tee - Run   | 1   | 1   | 1 | 1     | 1     | 1  | 2     | 2  | 0     | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0   | 0   |
| T       | 90' Flow thru Tee         | 3   | 4   | 5 | 6     | 8     | 10 | 12    | 15 | 17    | 20 | 25 | 30 | 35 | 50 | 60 | 71 | 81 | 91 | 101 | 121 |
| Z       | Generic Flow Switch       | 2   | 2   | 2 | 3     | 4     | 5  | 6     | 7  | 8     | 10 | 12 | 14 | 18 | 22 | 27 | 35 | 40 | 45 | 50  | 61  |

# Pressure / Flow Summary - STANDARD

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| Node No. | Elevation | K-Fact | Pt Actual | Pn | Flow Actual | Density | Area | Press Req. |
|----------|-----------|--------|-----------|----|-------------|---------|------|------------|
| 1        | 47.5      | 4.9    | 7.04      | na | 13.0        | 0.0508  | 256  | 7.0        |
| 2        | 47.5      | 4.9    | 7.68      | na | 13.58       | 0.0508  | 256  | 7.0        |
| 50       | 47.5      |        | 8.78      | na |             |         |      |            |
| 3        | 47.5      | 4.9    | 8.96      | na | 14.66       | 0.0508  | 256  | 7.0        |
| 12       | 36.92     |        | 17.85     | na |             |         |      |            |
| 13       | 36.92     |        | 17.85     | na |             |         |      |            |
| 10       | 36.92     | 4.9    | 12.69     | na | 17.45       | 0.0508  | 256  | 7.0        |
| 11       | 36.92     |        | 17.13     | na |             |         |      |            |
| 51       | 36.92     |        | 17.85     | na |             |         |      |            |
| 52       | 36.92     |        | 17.99     | na |             |         |      |            |
| 53       | 36.92     |        | 21.83     | na |             |         |      |            |
| 54       | 27.21     |        | 28.51     | na |             |         |      |            |
| 55       | 17.83     |        | 35.88     | na |             |         |      |            |
| 56       | 7.71      |        | 43.88     | na |             |         |      |            |
| 57       | 6.67      |        | 47.28     | na |             |         |      |            |
| TR       | 6.67      |        | 49.28     | na |             |         |      |            |
| BR       | 0.75      |        | 55.27     | na |             |         |      |            |
| 8UG      | 9.0       |        | 52.89     | na |             |         |      |            |
| TEST     | 28.0      |        | 44.68     | na |             |         |      |            |

The maximum velocity is 12.34 and it occurs in the pipe between nodes 52 and 53

# Final Calculations - Hazen-Williams

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| Hyd.<br>Ref.<br>Point | Qa<br>Qt       | Dia.<br>"C"<br>Pf/Ft   | Fitting<br>or<br>Eqv. | Ln.                | Pipe<br>Ftng's<br>Total    | Pt<br>Pe<br>Pf           | Pt<br>Pv<br>Pn | ***** | Notes           | ***** |
|-----------------------|----------------|------------------------|-----------------------|--------------------|----------------------------|--------------------------|----------------|-------|-----------------|-------|
| 1<br>to<br>50         | 13.00<br>13.0  | 0.874<br>150<br>0.0945 | 1O                    | 3.0<br>0.0<br>0.0  | 15.420<br>3.000<br>18.420  | 7.044<br>0.0<br>1.740    |                |       | K Factor = 4.90 |       |
|                       | 0.0<br>13.00   |                        |                       |                    |                            |                          | 8.784          |       | K Factor = 4.39 |       |
| 2<br>to<br>50         | 13.58<br>13.58 | 0.874<br>150<br>0.1023 | 1R                    | 1.0<br>0.0<br>0.0  | 9.790<br>1.000<br>10.790   | 7.680<br>0.0<br>1.104    |                |       | K Factor = 4.90 |       |
| 50<br>to<br>3         | 13.00<br>26.58 | 1.101<br>150<br>0.1153 | 1R                    | 1.0<br>0.0<br>0.0  | 0.500<br>1.000<br>1.500    | 8.784<br>0.0<br>0.173    |                |       | Vel = 8.96      |       |
| 3<br>to<br>52         | 14.67<br>41.25 | 1.394<br>150<br>0.0823 | 3N<br>1O              | 24.0<br>6.0<br>0.0 | 24.080<br>30.000<br>54.080 | 8.957<br>4.582<br>4.450  |                |       | K Factor = 4.90 |       |
|                       | 0.0<br>41.25   |                        |                       |                    |                            |                          | 17.989         |       | K Factor = 9.73 |       |
| 12<br>to<br>13        | 0.0<br>0.0     | 0.874<br>150<br>0.0    | 1R                    | 1.0<br>0.0<br>0.0  | 8.000<br>1.000<br>9.000    | 17.847<br>0.0<br>0.0     |                |       | Vel = 0         |       |
| 13<br>to<br>51        | 0.0<br>0.0     | 1.101<br>150<br>0.0    | 1N<br>1O              | 7.0<br>5.0<br>0.0  | 8.750<br>12.000<br>20.750  | 17.847<br>0.0<br>0.0     |                |       | Vel = 0         |       |
|                       | 0.0<br>0.0     |                        |                       |                    |                            |                          | 17.847         |       | K Factor = 0    |       |
| 10<br>to<br>11        | 17.45<br>17.45 | 0.874<br>150<br>0.1628 | 1N<br>1R              | 7.0<br>1.0<br>0.0  | 19.300<br>8.000<br>27.300  | 12.688<br>0.0<br>4.445   |                |       | K Factor = 4.90 |       |
| 11<br>to<br>51        | 0.0<br>17.45   | 1.101<br>150<br>0.0529 | 1O                    | 5.0<br>0.0<br>0.0  | 8.500<br>5.000<br>13.500   | 17.133<br>0.0<br>0.714   |                |       | Vel = 5.88      |       |
| 51<br>to<br>52        | 0.0<br>17.45   | 1.394<br>150<br>0.0167 | 2R                    | 2.0<br>0.0<br>0.0  | 6.500<br>2.000<br>8.500    | 17.847<br>0.0<br>0.142   |                |       | Vel = 3.67      |       |
| 52<br>to<br>53        | 41.25<br>58.7  | 1.394<br>150<br>0.1581 | 3R<br>1O              | 3.0<br>6.0<br>0.0  | 15.330<br>9.000<br>24.330  | 17.989<br>0.0<br>3.846   |                |       | Vel = 12.34     |       |
| 53<br>to<br>54        | 0.0<br>58.7    | 1.598<br>150<br>0.0813 | 1N<br>1O              | 9.0<br>8.0<br>0.0  | 13.420<br>17.000<br>30.420 | 21.835<br>4.205<br>2.472 |                |       | Vel = 9.39      |       |
| 54<br>to<br>55        | 0.0<br>58.7    | 1.598<br>150<br>0.0813 | 1N<br>2O<br>1R        | 9.0<br>16.0<br>1.0 | 14.670<br>26.000<br>40.670 | 28.512<br>4.062<br>3.306 |                |       | Vel = 9.39      |       |
| 55<br>to<br>56        | 0.0<br>58.7    | 1.598<br>150<br>0.0813 | 1N<br>1O<br>1R        | 9.0<br>8.0<br>1.0  | 26.500<br>18.000<br>44.500 | 35.880<br>4.383<br>3.617 |                |       | Vel = 9.39      |       |
| 56<br>to<br>57        | 0.0<br>58.7    | 1.61<br>120<br>0.1184  | 2E<br>1T              | 8.0<br>8.0<br>0.0  | 8.880<br>16.000<br>24.880  | 43.880<br>0.450<br>2.947 |                |       | Vel = 9.25      |       |

# Final Calculations - Standard

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| Hyd.<br>Ref.<br>Point | Qa<br><br>Qt | Dia.<br>"C"<br>Pf/Ft   | Fitting<br>or<br>Eqv. Ln.    | Pipe<br>Ftng's<br>Total    | Pt<br>Pe<br>Pf            | Pt<br>Pv<br>Pn | *****           | Notes | ***** |
|-----------------------|--------------|------------------------|------------------------------|----------------------------|---------------------------|----------------|-----------------|-------|-------|
| 57<br>to<br>TR        | 0.0<br>58.7  | 1.61<br>120<br>0.1184  | 2E<br>8.0<br>0.0<br>0.0      | 8.920<br>8.000<br>16.920   | 47.277<br>0.0<br>2.004    |                | Vel = 9.25      |       |       |
| TR<br>to<br>BR        | 0.0<br>58.7  | 1.61<br>120<br>0.1184  | 3E 12.0<br>1Z 4.0<br>1Eq 6.0 | 6.920<br>22.000<br>28.920  | 49.281<br>2.564<br>3.424  |                | Vel = 9.25      |       |       |
| BR<br>to<br>8UG       | 0.0<br>58.7  | 2.003<br>150<br>0.0271 | 1G 1.296<br>1T 12.965<br>0.0 | 30.000<br>14.261<br>44.261 | 55.269<br>-3.573<br>1.198 |                | Vel = 5.98      |       |       |
| 8UG<br>to<br>TEST     | 0.0<br>58.7  | 8.27<br>140<br>0.0     | 0.0<br>0.0<br>0.0            | 625.000<br>0.0<br>625.000  | 52.894<br>-8.229<br>0.019 |                | Vel = 0.35      |       |       |
|                       | 0.0<br>58.70 |                        |                              |                            | 44.684                    |                | K Factor = 8.78 |       |       |